



STRUCTURES ENGINEERING

BRIDGE BRANCH DESIGN INFORMATION

**BRIDGE BRANCH
DESIGN INFORMATION MANUAL**

This Manual is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise the issue and the use of this Manual.



A. LIM

SENIOR ENGINEER STRUCTURES

Date : 06/07/2022

Document No: 3912/02-1

This document is only controlled via the Main Roads website

BRIDGE BRANCH DESIGN INFORMATION

<u>SECTION</u>	<u>TITLE</u>
1.	Introduction, Scope and Purpose
2.	Design of New Structures
3.	Refurbishment and Strengthening Design
4.	Load Rating Bridges
5.	Design Vehicle Loadings
6.	Stress Limits in Structural Concrete
7.	Railings and Barriers
8.	Bearings and Joints
9.	Construction Forces and Effects
10.	Concrete Strengths and Finishes
11.	Bridge Widths
12.	Clearances and High Load Routes
13.	Bridge Waterways Investigation and Flood Estimation
14.	Structural Design and Analysis Software
15.	Inventory Information
16.	Historical Design and Load Rating Vehicles
17.	External Authorities
18.	Safety In Design

SECTION 1

CONTENTS

1	INTRODUCTION, SCOPE AND PURPOSE.....	4
1.1	Introduction	4
1.2	Scope	4
1.3	Purpose	5
1.4	Use of this Manual	5
1.5	Common Abbreviations	5

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
2	1	25/10/04	Index sheet amended. Section 15 re-titled and Section 16 incorporated into Section 15.
All	2	12/12/05	Complete review for introduction of AS 5100
2	3	22/01/08	Index sheet amended. New Section 16 added. Update clause 1.2.
2	4	18/06/09	Index sheet amended. New Section 18 added
All	5	03/04/18	Complete review for introduction of AS5100-2017
2	6	06/07/22	Index sheet amended. Section 4 re-titled

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 06/07/2022

1 INTRODUCTION, SCOPE AND PURPOSE

1.1 Introduction

The Bridge Branch Design Information Manual has been prepared to provide guidance and to set design criteria for the process of carrying out design and design related activities for bridges, culverts and other transport related structures. The Manual presents information and criteria for use in structural design to assist with the design process, clarify code ambiguities and to ensure uniformity, consistency and conformity of results.

The Manual has been prepared in good faith. However, Main Roads Western Australia (MRWA) does not guarantee or warrant the veracity of any information or referenced information contained within. The use of information and criteria contained within this Manual shall not relieve the user of their responsibilities for due diligence and checking of all results and outcomes.

1.2 Scope

The scope of the Manual includes, but is not limited to, the following:

- Design of new road and pedestrian bridges;
- Design of new culverts;
- Refurbishment design of existing bridges, including strengthening;
- Criteria for
 - Clearances
 - Bridge width
 - Bridge design loading
 - Serviceability stress limits
 - Construction forces and effects;
- Load rating of existing bridges, including historical design and load rating vehicles;
- Bearings and joints (including approach slabs);
- Railings and barriers; and
- Waterways investigation and flood estimation.

Unless specifically excluded by an authorised officer from Structures Engineering, all structural design undertaken within Main Roads Western Australia or by its authorised Agents shall incorporate the guidelines, methodologies, processes and criteria presented in this Manual.

1.3 Purpose

The principal purpose of this Manual is to:

- ensure uniformity of standards and details in the design of bridges, culverts and other transport related structures;
- record any variations from AS 5100 Bridge Design (CODE) approved for use in the design process;
- clarify any confusing or ambiguous areas of the CODE; and
- ensure that construction feedback receives widespread circulation.

Any person identifying a need for any of the above not already covered adequately elsewhere shall notify the Structures Design & Standards Engineer, who shall arrange the writing and issuing of any required revisions, if considered appropriate.

1.4 Use of this Manual

In using this Manual, references to other information Sections within the Manual are in the following format:

Design Information Manual / Document Number / Section Title

The above format is abbreviated to DIS 3912/02/xx “Section Title”, where DIS represents ‘Design Information Section’ and ‘xx’ represents the particular Section within the Manual.

1.5 Common Abbreviations

Common abbreviations used throughout this Manual are:

- DIS - Design Information Section
- BDC or CODE - Bridge Design Code, AS 5100
- MRWA - Main Roads Western Australia
- SES - Senior Engineer Structures
- SD&SE - Structures Design & Standards Engineer
- EBL - Engineer Bridge Loading

SECTION 2 – DESIGN OF NEW STRUCTURES

This information is Section 2 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As the head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.



A LIM
SENIOR ENGINEER STRUCTURES

Date: 04/09/2023

Document No: 3912/02-2

Controlled Copies shall be marked accordingly

SECTION 2

CONTENTS

2	DESIGN OF NEW STRUCTURES	3
2.1	Introduction	3
2.2	Preliminary Design	3
2.3	Prior to Detailed Design	4
2.4	Detailed Design.....	4
2.5	Design Criteria	4
2.6	Required Interfaces.....	6
2.7	Design Summary Sheets.....	7
2.8	Code Modifications	8
APPENDIX A	Preliminary Design Process.....	9
APPENDIX B	Modifications to AS 5100.....	9
APPENDIX C	Other Structural Design Requirements.....	9
APPENDIX D	Design Summary Sheet (Simply Supported).....	9
APPENDIX E	Design Summary Sheet (Continuous)	9

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	09/12/05	Complete review for introduction of AS 5100-2004
Appendix C	2	04/05/06	Amended Design Summary Sheet – Sample Only - Sheet No. 2 of 2
5, 6 and 8	3	11/12/06	Collision from railway traffic updated, RTEM guide renamed and use of Polymeric material for MSE walls
Appendix A	4	02/04/12	Amended Design Summary Sheets – Load Rating – Group 2 Vehicles 4 & 5 Non Supervision added
All	5	04/09/23	Full review and alignment with SWTC

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 04/09/2023

2 DESIGN OF NEW STRUCTURES

2.1 Introduction

The design of new structures shall be carried out in accordance with generally accepted engineering principles in conjunction with AS 5100 Bridge Design (Code). Additions and modifications to the Code are required as per Section 2.5.

General design guidance is provided in the Structures Engineering Design Manual, (Document No. 3912/03).

Main Roads staff may access the design process guidelines and report template provided in the Structures Engineering Management System manual (Document No. 3912/01).

Stakeholders should understand that Structures Engineering provides advice, not approval or direction. The Engineer is fully responsible for the design and the Project Manager is fully responsible for risk.

2.2 Preliminary Design

Great importance is attached to carrying out adequate Preliminary Design to ensure that all options and constraints are identified so that the most appropriate design can be selected. The potential for improvement by appropriate selection of structure type and construction method is much greater here than in final design, where only marginal refinements are possible.

This concept stage is vital and both experience and imagination are required. Sufficient time and effort must be put in before beginning the detailed design to ensure the best option is selected in terms of form, function, aesthetics, constraints such as site conditions, practicality and cost of both construction and maintenance.

During the preliminary design stage it is important to consider all constraints as these will have a considerable influence on the chosen structure type and components. More information on common constraints can be found in Section 2 of the Structures Engineering Design Manual (Document No. 3912/03), but amongst the more important constraints are:

- clear spanning requirements
- any staging requirements for future road or rail widening
- structure type, product selection and preventative treatments to minimise whole of life cost or improve value
- access for inspection (from parking to visibility of key components)
- environmental and/or ethnographical considerations
- need to maintain traffic, rail or navigation clearances during construction
- choice of construction method (difficult site conditions, restricted access etc)
- influence and importance to be placed on aesthetics

The preliminary design process is a simplification of final design. The aim is to obtain an approximate idea of member sizes, reinforcement, foundations etc so that a reasonably accurate cost estimate can be prepared. The amount of effort put in at this stage will obviously depend on the size, importance and cost of the particular structure.

It is normal to produce at least General Arrangement and Cross Section drawings of each bridge option or scheme investigated. Other drawings or sketches may be necessary so that an approximate Bill of Quantities can be prepared to enable an estimate to be calculated.

On completion of the preliminary design, the Design Engineer is required to produce a 15% design report and recommend an option to progress to detailed design. When recommending an option it is important that the Design Engineer not make assumptions about what price will be acceptable to Main Roads. It is up to Main Roads staff to obtain the funding required, or to select a different option if funding of the ideal option has not been achieved.

A simplified flow chart of the Preliminary Design process is presented in Appendix A.

2.3 Prior to Detailed Design

Prior to detailed design it is required that gaps in standards be identified and additional clauses/alternative standards to be used be submitted for review with comprehensive and unbiased research, optioneering and justification. Depending on scope and budget, this can be done as part of the 15% process or at the beginning of the detailed design.

2.4 Detailed Design

Detailed design is a natural progression of the preliminary design. All bridge and structure design shall be carried out in accordance with the Code, as modified by this Manual (refer section 2.8).

2.5 Design Criteria

The design criteria present the parameters used in the design. The design criteria is used to confirm accuracy of the design parameters prior to committing effort to detailed design. The design criteria may also be of use in future works if the asset is to be modified or load rated.

Main Roads has the following mandatory design criteria documents:

Bridge Design Criteria	Criteria form to present the conceptual design. Requires SES signature before detailed design can proceed.
Bridge Specific Design Criteria	Bridge specific design parameters that are submitted for review with the design report.
Standard Bridge Design Criteria	The Standard Bridge Design Criteria has standard design parameters and code references. It exists so that these are not re-produced in every design report. Do not include this document in report appendices. The Standard Bridge Design Criteria is not to be modified. Any authorised Deviation from standard shall be added to the Bridge Specific Design Criteria instead.

The design criteria forms need to be filled out to an extent that is appropriate to the stage of design. It is acknowledged that some items will be unknown at early stages of

design.

In cases where an item in the bridge specific design criteria is not applicable, “N/A” can be entered in place of a value. The need to offer an explanation is at discretion of the engineer but explanations do assist the reviewer/verifier. In example, for “Road Bridges – Vibration” the value for First mode flexural frequency could be entered as “N/A (compliant deflection)”.

This design criteria forms can be used for an Approval in Principle process where they are submitted early for review. Most designs will not require this process.

In an effort to not repeat the items from the Bridge Design Criteria Checklist in the Bridge Specific Design Criteria, it is intended to include both forms in the structural report.

It is expected that the design report will include a table as follows:

Type of Criteria	Description
Bridge Design Criteria	Refer Appendix X
Bridge Specific Design Criteria	Refer Appendix X
Standard Bridge Design Criteria	Main Roads Standard Bridge Design Criteria, dated dd/mm/yyyy
Relevant RFI	Include document number, subject and date. The author may decide whether they need to be included in an Appendix, generally this is not required unless an issue is contentious or not resolved.
Deviations from Standard	List here, eg: “Topic – Authorised” or “Topic – In progress”. Update the Bridge Specific Design Criteria to match. Include SES authorisation in an Appendix.

2.6 Required Interfaces

A summary of interfaces with Structures Engineering is presented below.

Item/Form	Responsible role & Contact address	Notes
Information requests	DO structengreviews@ mainroads.wa.gov.au	
New bridge number	DO structengreviews@ mainroads.wa.gov.au	
Vehicle loads	EBL structengreviews@ mainroads.wa.gov.au	
Bridge Design Criteria	SES structengreviews@ mainroads.wa.gov.au	Must be submitted prior to detailed design
Bridge Specific Design Criteria	Review Team structengreviews@ mainroads.wa.gov.au	This will generally be submitted as part of the design report, except for special cases where agreement in principle is considered necessary prior to design
Departure from Standards	SES structengreviews@ mainroads.wa.gov.au	Must be submitted prior to detailed design
Waterways	SWE eric.cheung@ mainroads.wa.gov.au	
OS&H Report (Safety in Design)	Project Specific (e.g.: Project Manager)	Typically submitted as part of the design report. Not reviewed by Structures Engineering
Bridge/Culvert Inventory form	DO structengreviews@ mainroads.wa.gov.au	
Submissions for review	Project Specific (e.g.: Project Manager)	The PM will provide to Structures Engineering if review is required. Drawings are not accepted without an associated design report and are not to be split into piecemeal packages. Structural, durability, waterways, TQ and RFI reviews only
Design Summary Sheets and model files	EBL structengreviews@ mainroads.wa.gov.au	The DSS incorporating load ratings for all design vehicles must be submitted and get reviewed at IFC Design Stage.
As Constructed information	Project Specific (e.g.: Project Manager)	The PM is responsible for sending to Structures Engineering. All X-refs to be bound.

It is important to only submit quality work. Work that is not of suitable standard will be returned unactioned. When this occurs there is a mandatory two week period where

the design and drawings are to be reviewed and updated before they may be sent again for review.

Do not include the email address of individual Structures Engineering staff in the email cc field when sending a request to structengreviews@mainroads.wa.gov.au. Doing so impacts internal document control processes and extends turnaround times.

2.7 Design Summary Sheets

Design Summary Sheets (DSS) shall be prepared by the Design Engineer for all new bridges, dual use path bridges with vehicle access and culverts/underpasses with clear spans over 3.0m. summarising the most important features of the design on completion of the design and independent design verification. The Design Summary Sheet is critical to load management as it contains a summary of all the major design components and is used to check heavy load movements and design future works. The actual contents will vary depending on the size and complexity of the structure. Typical Summary Sheet details for a simply supported structure and a continuous structure are attached at Appendix D and E respectively and should be adhered to as a minimum standard. The DSS incorporating load ratings for all design vehicles must be submitted and get reviewed at IFC Design Stage and finalised within two months.

The Design Engineer MUST report the load rating factor of each new bridge for each nominated rating vehicle in accordance with AS 5100.7 and Section 4.

The main items to include on the Design Summary Sheet are:

- Details of the span configuration
- The design cross-sections used in the analysis at critical positions, e.g., support and midspan
- The section properties of these design cross-sections
- Details of the reinforcement and/or prestress and the section capacities at the critical sections
- The serviceability design moments and resulting stresses at the critical sections
- Live Load Distribution Factors for different loadings
- The available live load capacity at the critical sections, for use in checking heavy load movements
- Foundation information, i.e., design bearing pressures for spread footings, design pile loads for piled foundations
- Design scour allowance
- Load rating information for all design and rating vehicles in accordance with Section 4 of BBDIM

2.8 Code Modifications

There are three main sources of modifications to the Code:

1. SES Circulars contain clarifications or mandatory Code modifications for Main Roads projects. The Design Engineer must check for currency of SES circulars as they may have been recalled or updated. SES Circulars are available on the Main Roads website.
2. This Manual contains mandatory Code modifications for Main Roads projects. The entire Manual is relevant, although the reader's attention is drawn to Appendix B & C in this section.
3. Deviations from the Code as requested by the Design Engineer. Any deviations from the Code require written approval from Senior Engineer Structures. Past practice is not an acceptable reason to deviate from the code on new projects. As such, it is noted that all approvals from SES are project specific.

APPENDICES

APPENDIX A	Preliminary Design Process
APPENDIX B	Modifications to AS 5100
APPENDIX C	Other Structural Design Requirements
APPENDIX D	Design Summary Sheet (Simply Supported)
APPENDIX E	Design Summary Sheet (Continuous)

APPENDIX A PRELIMINARY DESIGN PROCESS

Step 1: assess the site where the bridge is to be located. The site constraints will influence the bridge type, configuration and method of construction.

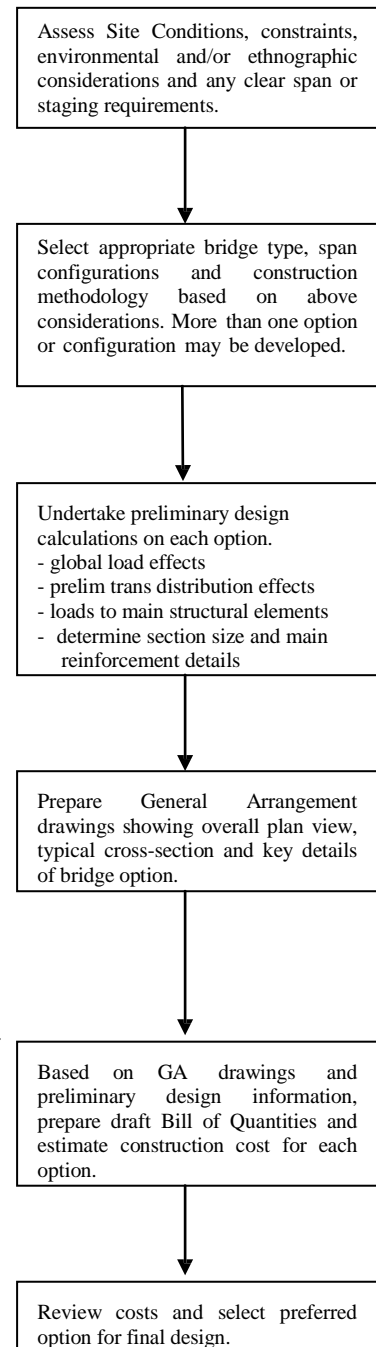
Step 2: an appropriate option for bridge type (reinforced or prestressed concrete, steel or composite), configuration (number and length of spans, bridge width), foundations (piled or spread footings) and construction methodology (in situ, precast, segmental, incremental launch).

Step 3: preliminary design can range from simple global models and simplified distribution analysis to use of grillage or FE models, depending on the complexity of the bridge.

Step 4: preliminary drawings showing general details of the overall bridge configuration, superstructure and substructure together with relevant sections and details will assist with estimating construction costs and visualising the bridge.

Step 5: construction costs are estimated (usually by a Quantity Surveyor) based on the details provided in the preliminary drawings, and are required to assess the economic attributes and cost-effectiveness of the various options.

Step 6: select the best option that meets all specified criteria to proceed to final design.



APPENDIX B MODIFICATIONS TO AS 5100

The clause numbers below refer to clause numbers as used in the Bridge Code. For example: BDC 1 - 13.1 refers to Bridge Code Part 1, Clause 13.1.

AS 5100.1 – SCOPE AND GENERAL PRINCIPLES

BDC 1 – 8.2 Design Life

Design life shall be in accordance with the Standard Bridge Design Criteria (D23#845709).
Art work and rebates must not compromise the design life of an asset.

BDC 1 - 13.6 Horizontal Clearance to Substructure Components of Bridges over Roadways

The face of any support, apart from columns located in the median, must be set back from the ultimate edge of the nearest traffic lane as per Figure 12.1 in Section 12.

BDC 1 - 13.7 Vertical Clearance of Structures

Refer to Section 12 for requirements.

Note that headroom requirements are presented in Appendix C.

BDC 1 - 14 Traffic Barriers

Main Roads' standard barriers that are deemed to comply with the respective Code Performance Levels should be used where possible.

Refer to Section 7 for additional requirements.

BDC 1 - 15.3 Collision from Road Traffic

For guidance on the protection of sign structures, see Austroads Guide to Road Design Part 6.

BDC 1 - 15.3 Collision from Rail Traffic

Whether deflection walls are required is dependent on assessment in accordance with the Code.

Where a sign structure has potential to fall and endanger life, the sign supports must be assessed in the same way as bridge supports.

BDC 1 - 16 Pedestrian and Bicycle-Path Barriers

Where a structure, such as a retaining wall, head wall or wingwall, presents a vertical or near vertical face 1.5 m or more in height and it would be likely that a person could gain access to the upper edge of the structure, an AS5100 compliant pedestrian restraint system shall be installed close to, or on top of the structure. Fences are not acceptable.

A risk assessment shall be carried out for the protection screen requirements for objects falling or being thrown from bridges in accordance with Main Roads' assessment procedure outlined in the "*Risk Assessment for Projectiles Thrown from Overpass Structures*" D22#878096. It is important to seek information from local police stations as there may be existing projectile rock throwing risk that would otherwise not be identified.

Protection screens (all types) must not be installed within the working distance of barriers.

BDC 1 - 18 Drainage

For bridges that are not on a crest, upstream road infrastructure shall be used to intercept water before it crosses a Deck joint.

Drainage pipes are not preferred due to the difficulty of maintenance. They should only be installed where required for Environmental reasons such as discharging water away from protected water sources.

All bridge drainage pipes whether external or internal must be of durable material, must be corrosion and fire resistant, and must be concealed from public view where possible.

All drainage structures must be vandal proof and accessible for cleaning (eg: pressure blasting and rodding), operation and maintenance purposes.

BDC 1 - 19 Access for Inspection, Maintenance and Component Replacement

Access shall be provided such that each component can be inspected and maintained (or replaced if applicable).

Where steps are used in areas subject to flood loading it is preferred to install them on the downstream side as they collect debris.

BDC 1 - 20 Utilities (Services)

When a service is installed within the bridge structure, it shall be installed where it is safest and maintainable.

It is expected that:

- (i) Services are installed in a footpath slab where possible. This includes having all spare conduits in one side of the bridge and crossing the road using off-bridge junction pits.
- (ii) Services cast into the beams shall generally be avoided.

It is required that

- (i) Water (including sewerage), gas and oil services shall not be located within a void unless agreed by the service authority.
- (ii) Service types shall only be mixed where approved by the service owners. For example, water/gas/oil and electricity may require separation.
- (iii) Services shall be concealed from view if possible.
- (iv) Adequate provision must be made for future inspection, maintenance and possible replacement.

Spare ducts comprising two 100 mm (internal diameter) conduits and draw wire must be provided on each side of the bridge terminating with capped ends beyond the deck and approach slab.

Where a bridge is subject to flooding and the bridge type provides limited space to have cast-in conduits, it should be considered whether service protection against flooding is more important than the number of spare ducts. If there are no services crossing the bridge, then installing only one spare duct per kerb is generally preferred to hanging spare conduits. Allowance shall still be made to install the additional ducts in the future if necessary, eg: by providing penetrations for future conduits in abutment walls.

Services must not require access (including inspection and maintenance) via traffic lanes. Locations of pits and conduits must not conflict with traffic barriers.

AS 5100.2 – DESIGN LOADS

BDC 2 – 7 Road Traffic

For additional requirements refer to Section 5, Design Vehicle Loadings.

BDC 2 - 6.3 Superimposed Dead Load

Traffic barriers, surfacing, parapets and any non-structural components must be treated as superimposed dead load.

Road bridge structures with an open graded asphalt wearing surface must be designed for the load from a total asphalt thickness of 100 mm. All other road bridges must be designed for the load from asphalt surfacing of 75 mm thick. Main Roads bridges on a highway or main road (ie. M or H class road) may take the surfacing super imposed dead load as “controlled”.

Bridge geometry such as deck levels and the depth of concrete upstands shall depend on the seal type. Refer to 3912/02/08 “Bearings and Joints” for general guidance.

BDC 2 – 7.3 Heavy load platform

For additional requirements refer to Section 5, Design Vehicle Loadings.

BDC 2 – 7.5 Standard design lanes

Use b = width (in metres) between external barriers. Where the barrier has an adjacent kerb this width may be subtracted during calculation of b .

If it can be demonstrated that there will be no future need to replace a median skylight with trafficable surface, then the design lanes may be placed to avoid the skylight. Doing so requires Structures Engineering and Road and Traffic Engineering approval.

All other traffic barriers, balustrade, medians, footpaths, must be treated as usable carriageway and their width included in the calculation of b .

Where there is no traffic barrier separating the carriageway and paths or raised verges, the Deck must be designed for SM1600 loading between traffic barriers with path concrete in place.

For additional requirements regarding vehicle positioning refer to Section 4, Load Rating of Bridges.

BDC 2 – 14 Earth Pressures for Integral and Semi-integral Bridges

Earth pressures that develop behind integral abutments and end screen walls may be calculated as per PD 6694-1:2011. In this case the load factor for passive earth pressure must be as per Table 6.4 of AS5100.2.

BDC 2 - 22 Construction Forces and Effects

In addition to Code requirements, the following criteria shall apply during the construction stage:

- (a) Construction Live Load of 1.0 kPa minimum on entire surface
- (b) The design differential settlement shall allow a component for settlement during construction (permanent effects and construction live load) of no more than 25mm.

For launched bridges, a note is required in the construction specification that launching is not to be carried out during strong winds.

AS 5100.3 – FOUNDATIONS AND SOIL-SUPPORTING STRUCTURES

BDC 3 - 5.3.1 Shallow Footings

The use of sill beams (beam-like shallow foundations) is not permitted on road bridges. Sill beams are permitted on footbridges provided there is a minimum footing embedment of 1.5m.

BDC 3 - 6 Piled Foundations

Continuous Flight Auger (CFA) piles will not be permitted:

- (A) in cohesive soils, silts or soil profiles with layers of coarse gravels or larger particles, except where excavation of an uncased hole near vibration sensitive Services is not possible;
- (B) where the concrete exposure classification is more severe than B1 in accordance with Section 5 of the Bridge Code;
- (C) where a socket in rock of a better quality than highly weathered is required;
- (D) where a rock socket longer than 300 mm is required;
- (E) where raked piles are required;
- (F) where the soil profile is complex with hard layers over soft layers; or
- (G) for end bearing piles, where the bearing stratum is on a slope steeper than one vertical to four horizontal.

AS 5100.4 – BEARINGS AND DECK JOINTS

Design shall be in accordance with Section 8, “Bearings and Joints” and as follows:

BDC 4 - 5 Functions of Bearings and Deck Joints

The bridge deck slab shall be continuous between abutments.

BDC 4 - 12.1 Elastomeric Bearings - General

Where the use of elastomeric bearings is proposed bearings must be selected from Appendix A of the Code.

BDC 4 - 12.6.7 Fixing of Bearings

Bearings must be restrained in position by recessed pockets in concrete Substructures or by mechanical devices.

BDC 4 - 19 Deck Joints

Joints that are primarily rubber that incorporate embedded steel plates shall not be used.

Joints must not inhibit the proper placement of concrete.

For new bridges, where the deck joint is attached by bolts cast into a concrete substrate, fully tensioned high tensile bolts must be used. Where the deck joint is attached by bars cast into concrete, flat bars must be used. Alternatively, proprietary joints with documented

evidence of long term performance may be submitted for to SEB for authorisation. The evidence submitted shall not be reliant on manufacturer brochures.

BDC 4 - 19.5 Drainage for Road Bridges

Deck joints must be designed to ensure the joint will contain run-off over the full width of the Deck, including at paths. A maintainable backup drainage solution should be provided if possible.

Prefabricated extrusion joints must be turned up directly behind the carriageway kerbs to maintain the same installation depth from the Deck or Superstructure surface, and extended for the full height of the kerb to contain runoff. Deck joints in shared path bridges or across raised parts of the Deck or Superstructure including paths, medians and parapets must be concealed and protected using a recessed steel cover plate. Deck or Superstructure crossfall must be designed to prevent water leakage or spilling from the Deck or Superstructure at the joints.

AS 5100.5 – CONCRETE

The following requirements are applicable to both superstructure and substructure design.

BDC 5 – 1.2 Application [Reinforcement]

Ductility Class L and/or LP reinforcement shall not be used for strength, except in culvert base slabs, apron slabs, and walls up to 2 m height.

BDC 5 – 4.14.3 Cover for Corrosion Protection

(A) The Designer must identify whether standard formwork and compaction or rigid formwork and intense compaction applies. It is noted that not all faces of precast elements receive intense vibration, particularly beam top and bottom flanges. Where rigid formwork and intense compaction is used, unless specifically allowed by Main Roads Specification 820, the engineer will note on the drawings that self-compacting concrete is not permitted.

(B) Where curing compounds are used, the cover shall be increased by 5 mm for classifications A and B1, and 10mm for other classifications.

BDC 5 - 4.3 Exposure Classification

Protective surface coatings must not be taken into account in durability design or assessment.

BDC 5 - 4.4.2 Curing

Accelerated curing by methods other than steam curing will not be permitted.

BDC 5 – 8.1.7 Stress in bonded tendons at ultimate strength

The maximum stress reached in bonded tendons at ultimate strength (σ_{pu}) shall be calculated based on the stress-strain relationships shown in Figure 2.1.

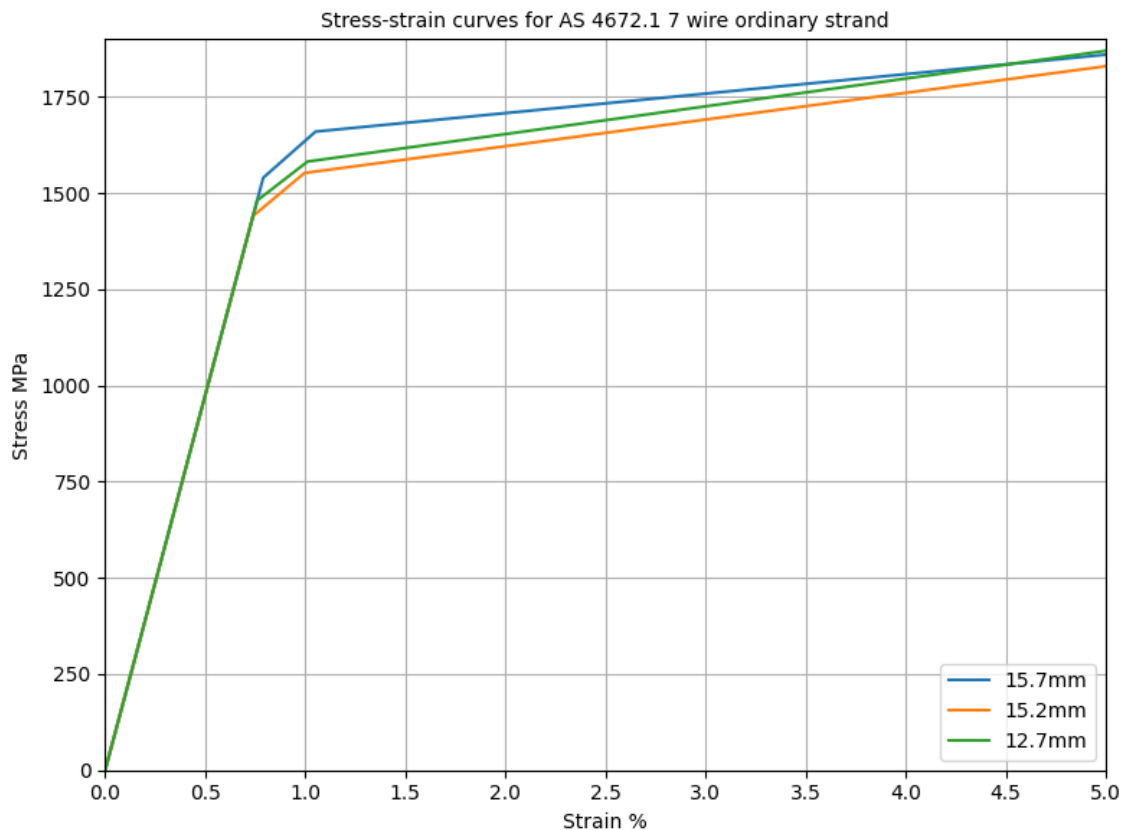


Figure 2.1 Idealized Stress-Strain Curve for 12.7, 15.2 and 15.7mm strand

The idealised trilinear stress-strain curves (Figure 2.1) are based on tensile properties of strand as per AS 4672.1 with a design breaking strain of 5%.

BDC 5 – 8.2 Strength of beams in shear and torsion

Section 4 provides a detailed example for using an iterative MCFT method to calculate the capacity of prestressed concrete members. Note the values of capacity reduction factor, ϕ , differs depending on the failure mode.

Please note, the approach presented in Section 4 to use of z as the internal moment lever arm as an approximate method should NOT be used in design or load rating for the Design Vehicles. Rather, the Design Engineers should use the known actual additional longitudinal reinforcement used for shear and torsional demand. Also, for the purpose of independent design verification and future calculation, the additional reinforcement shall be clearly demarcated in the relevant design drawings.

For determining if torsional strength should be considered or not as per Cl. 8.2.1.2 AS 5100.5, T^* shall be calculated from both cracked and uncracked sectional analysis as explained in Section 4.

BDC 5 – 10.7.4.2 Restraint of longitudinal reinforcement

The detailing in item (a)(iv) is only acceptable as restraint of longitudinal column reinforcement. Fitments can only be used for strength if complying to the requirements of AS 5100.5 Clause 8.3.2.4

BDC 5 – 13.2 / 13.2.5 Splicing of reinforcement

Bundled bars must be accounted for in determining lap length. Bundling caused by splicing of reinforcement must be included.

APPENDIX C OTHER STRUCTURAL DESIGN REQUIREMENTS

Structural design requirements that do not relate to a specific clause in AS 5100 are listed below.

1. Minimum Headroom

To assist in safe future inspection and maintenance, bridge clear headroom shall not be less than 1.0m.

2. General Reinforced/Prestressed Concrete Requirements

The use of half joints requires SES approval.

3. Precast Prestressed Concrete Beams

If precast prestressed concrete trough beams are used for the Superstructure, then the following detailing requirements must apply in the design and manufacture of beams:

- (A) Only open trough type beams will be permitted
- (B) Internal diaphragms must be provided at each end of each beam
- (C) Intermediate internal diaphragms must be provided at a maximum spacing of third points along the beam
- (D) Unless alternative measures are implemented to cater for torsional effects, cross girders / external diaphragms must be provided at the ends of each span between beams and must comply with clause 3.6(b)(xiii)
- (E) Web thickness must be a minimum of 125 mm to assist placement and compaction of the bottom flange concrete
- (F) The maximum bridge skew must be 30 degrees
- (G) Cover to the top face of the top flange must be a minimum of 20 mm
- (H) In order to prevent the development of intersecting horizontal cracks between the strands, not more than 50% of the prestressing strands must be debonded at any section, including beam ends. Debonding of adjacent strands is only permitted where there is at least 100 mm of concrete between the strands.

4. Reinforced Soil Walls

Refer to specification 802 for other design requirements.

MSE Abutments will not be permitted on structures over a water course.

The MSE panels must extend to the underside of the superstructure with minimum clearance sufficient to enable the maintenance and replacement of the bearings.

MSE wall panels are to be full height except segmental panels are acceptable for bridges over rail.

The top of all MSE walls and the area adjacent to the Abutment, including associated wingwalls, must be stone pitched for 1.0 m width to prevent ingress of water into the reinforced soil block. Bituthene, or equivalent membrane, must be used to prevent loss

of MSE wall backfill through facing panel joints.

5. Abutments and Piers

Abutments must be constructed so that any spill through embankment, backfill, or Abutment footings can be removed in the future down to 200 mm below the nearest road shoulder level without reducing structural adequacy.

Abutments and Piers must be of concrete construction. Steel piers are acceptable for Shared path bridges. Facing panels will not be permitted.

Minimum requirements for footings and pilecap soffit levels:

- On bridges over permanent water, 300 mm below design scour level and lowest astronomical tide
- On bridges not over permanent water, 300 mm below finished ground level. Note that AS5100.1 clause 15 requires this minimum be increased to 1.2m where a pier is functioning as a collision wall, however this shall be taken to apply to spread footings only.

6. Approach Slabs

Bridges longer than 30m shall have approach slabs. For bridges between 20 and 30m an allowance shall be made to install future approach slabs by incorporating a suitable corbel into the skirt beam or abutment curtain wall.

Approach slabs must be of uniform length and must be at least 5.0 m long measured normal to the expansion joint.

7. Waterproofing

The waterproofing design must be in accordance with Main Roads' Specification 875, *Waterproof Membrane*.

8. Shared Path Underpasses

(i) All underpasses must be single span concrete structures. Cladding will not be permitted. The Deck cross-section of shared path underpasses must have a continuous flat or curved Soffit, that is, Discrete Beams will not be permitted. Steel structures will not be permitted.

(ii) Underpass Skylights shall be designed for W80 wheel load at any location. The structure that supports the skylight may be subject to traffic loads as per Main Roads amendments to BDC 2 – 7.5.

9. Culverts

Culvert barrels must follow the natural waterway alignment.

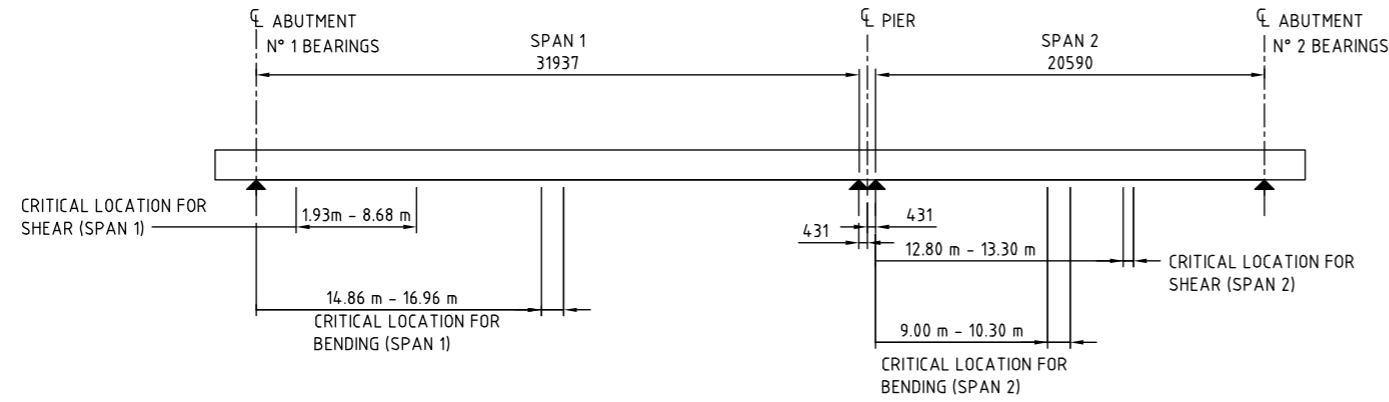
10. Future Modifications

All structures must be designed such that elements, other than barriers, that are constructed initially do not require modification or strengthening for the ultimate configuration.

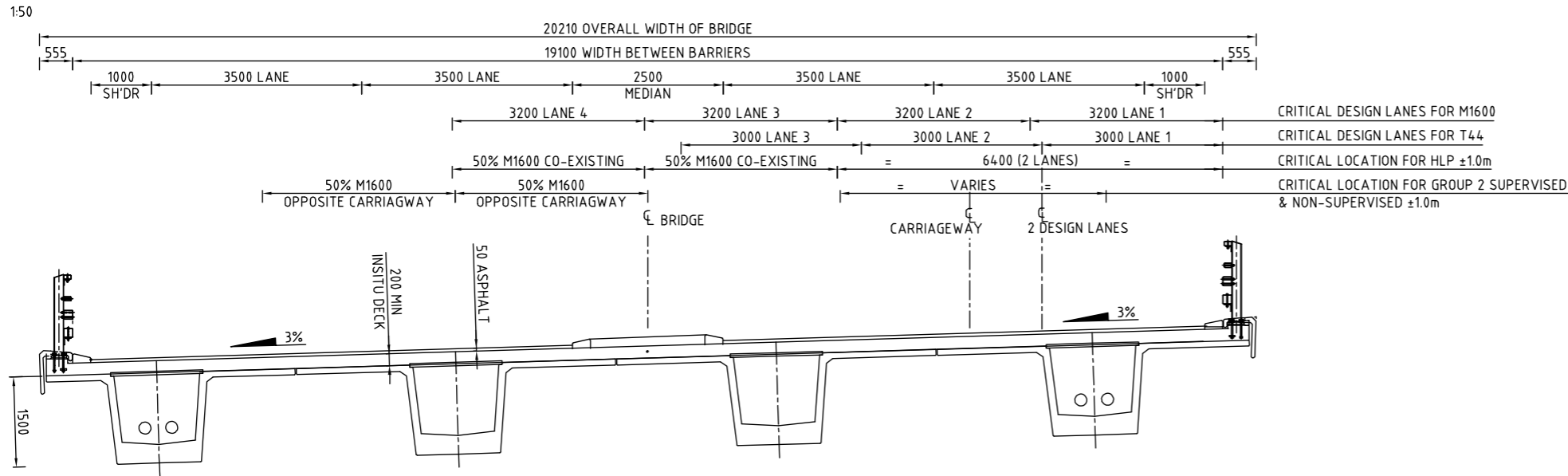
Design shall ensure any planned bridge widenings will be economic and practical.

1 - SPAN CONFIGURATION

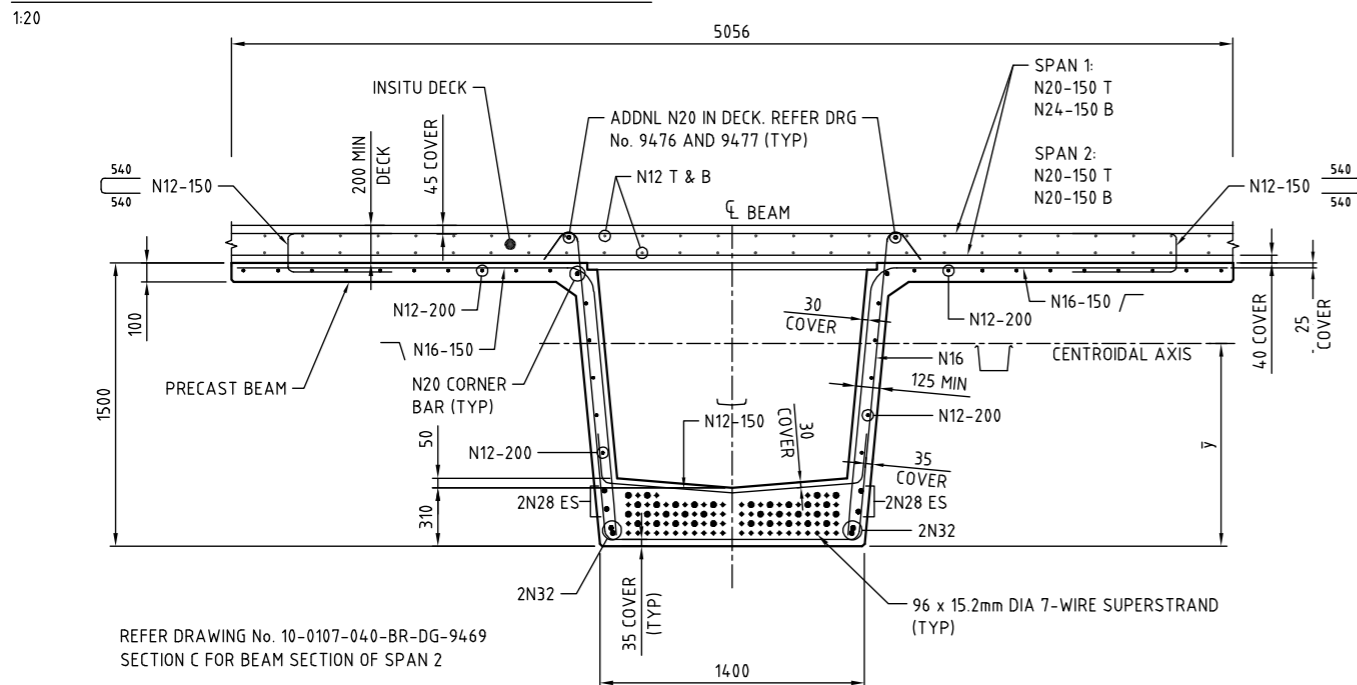
1:200
(SIMPLY SUPPORTED SPANS WITH LINK SLABS OVER PIER)



2 - TYPICAL DESIGN CROSS SECTION



3 - TYPICAL COMPOSITE BEAM SECTION AND PROPERTIES



MATERIAL PROPERTIES

PRESTRESSING:

$f_{pb} = 1830 \text{ MPa}$
 $f_{py} = 1501 \text{ MPa}$
 $E_p = 195,000 \text{ MPa}$
 $A_{pt} = 143 \text{ mm}^2 \text{ PER TENDON}$
 JACKING STRESS = 1208 MPa

CONCRETE:

$f'_c = 50 \text{ MPa}$ (PRECAST BEAM)
 $f'_c = 40 \text{ MPa}$ (INSITU SLAB)
 $E_c = 34,800 \text{ MPa}$ (PRECAST BEAM)
 $E_c = 32,800 \text{ MPa}$ (INSITU SLAB)

REINFORCEMENT:

$f_{sy} = 500 \text{ MPa}$
 $E_s = 200,000 \text{ MPa}$

TABLE 1 - CHARACTERISTICS OF THE COMPOSITE SECTION

CRITICAL SPAN & BEAM	BENDING		SHEAR	
	SPAN 1 BEAM 4	SPAN 2 BEAM 8	SPAN 1 BEAM 4	SPAN 2 BEAM 8
DISTANCE FROM A1 END SUPPORT (m)	14.86 TO 16.96	9.00 TO 10.30	1.93	12.80 TO 13.30
No. OF TENDONS	96	40	62	40
A_{cp} (m ²)	2.656	2.656	2.656	2.656
A_{ct} (m ²)	0.609	0.520	0.687	0.520
A_g (m ²)	2.102 MIN	1.907 MIN	2.102 MIN	1.907 MIN
A_o (m ²)	2.084	2.112	1.976	2.112
A_{oh} (m ²)	2.363	2.363	2.354	2.363
A_{pt} (mm ²) [1/2 DEPTH]	13728	5720	8306*	5720
A_{sc} (mm ²) [ABOVE d_h]	6341	3125	6341	3125
A_{st} (mm ²) [1/2 DEPTH]	6132	3164	6584	3164
A_{sv} (mm ²)	402	226	628	402
b_{ef} (m)	5.056	5.056	5.056	5.056
b_v (mm)	250	300	400	300
d (m)	1.543	1.592	1.547	1.592
d_h (mm) at ϕM_U (FROM TOP)	203.6	116.6	152.1	116.6
d_b (m)	1.630	1.630	1.630	1.630
d_p (m)	1.545	1.605	1.559	1.605
d_{sc} (m)	0.098	0.072	0.098	0.072
d_v (m)	1.439	1.433	1.392	1.433
I_g (m ⁴)	0.7944 MIN	0.6842 MIN	0.7944 MIN	0.6842 MIN
M_s (kNm)	24172	11078	N/A	N/A
P_v (kN)	0	0	0	0
s (mm)	150	150	150	150
t_w (mm)	125	150	200	150
u_c (m)	6.540	6.540	6.540	6.540
u_h (m)	6.169	6.169	6.157	6.169
z (m)	1.439	1.356	1.331	1.356
α_v (°)	90	90	90	90
\bar{y} (m)	1.159	1.165	N/A	N/A
σ_{cp} (MPa)	6.2	3.0	3.7	3.0
σ_{pu} (MPa)	1652	1652	1652	1652
ϕM_U (kNm)	30492	14094	20927	14094
0.25 ϕT_{cr} (kNm)	406	391	517	391

DSS NOTES:

- ALL LONGITUDINAL REINFORCEMENT AND PRESTRESSING ARE INCLUDED IN THE DETERMINATION OF ϕM_U . ACTUAL BENDING CAPACITY FOR EACH VEHICLE SHALL BE ADJUSTED BY THE RATIO OF THE LONGITUDINAL TENSILE FORCE DEMAND FROM BENDING ACTION OVER TOTAL TENSILE FORCE DEMAND INCLUDING SHEAR AND TORSION (SEE TABLES 2 AND 3).
- M_s BASED ON LIMITING THE INCREMENT IN STEEL STRESS NEAR THE TENSION FACE TO 200MPa.
- EXTERNAL BEAMS VARY IN FLANGE WIDTH. THE CAPACITY GIVEN IS FOR THE CROSS SECTION WITH THE MINIMUM FLANGE WIDTH.
- ϕM_U AND σ_{pu} HAS BEEN CALCULATED BASED ON AS 5100.5:2017 CLAUSE 8.1.7.
- A_{sv} AT THE CRITICAL SECTION FOR SHEAR HAS IGNORED THE D-SHIFT OF SHEAR REINFORCEMENT IN ACCORDANCE WITH AS 5100.5:2017 CLAUSE 8.3.2.3.
- DEVELOPMENT ZONES OF DE-BONDED STRANDS WERE CHECKED FOR ANY CONCRETE TENSION FROM SLS LOADING ($2L_d$ CHECK) IN ACCORDANCE WITH AS 5100.5:2017 CLAUSE 13.3.2.2.
- * DENOTES EFFECTIVE A_{pt} DERIVED THROUGH LINEAR INTERPOLATION WITHIN A PRESTRESS DEVELOPMENT ZONE.

PROJECT TITLE		DRAWING TITLE	
SIMPLY SUPPORTED BRIDGE		SIMPLY SUPPORTED BRIDGE	
DESIGN SUMMARY - SHEET N° 1 OF 3		DESIGN SUMMARY - SHEET N° 1 OF 3	
SAMPLE ONLY		SAMPLE ONLY	
MRWA DRAWING No.		LOCAL AUTHORITY	
STATUS		DRAWING NUMBER	
REV		REV	

Rev.	DATE	DESCRIPTION	APPROVED	HEIGHT DATUM:

METADATA

GROUND SURVEY STANDARD:

DATE OF CAPTURE:

MAPPING SURVEY STANDARD:

DATE OF CAPTURE:

MAIN ROADS PROJECT ZONE:

HEIGHT DATUM:

DESIGNED	VERIFIER
DRAWN	DESIGN MANAGER APPROVED
CHECKED	ALLIANCE PROJECT MANAGER APPROVED
DRAWING PURPOSE	

SCALE: 1:50 0 0.5m 1 1.5 2 2.5 3 3.5 4 4.5 5
1:200 0 200mm 400 600 800 1000 1200 1400 1600 1800 2000
1:2000 0 2m 4 6 8 10 12 14 16 18 20

TABLE 2 - DESIGN ACTIONS FOR ULS MOMENT AT CRITICAL LOCATIONS - LONGITUDINAL EFFECTS

VEHICLE LOAD CASE	CRITICAL SPAN & BEAM	CRITICAL LOCATION FROM A1 END SUPPORT (m)	PERMANENT ACTIONS			ACCOMPANYING ACTIONS			LIVE LOAD ACTIONS			% LONG REINF. DEMAND FROM BENDING (REFER NOTE 9)	CONTROLLING DESIGN CASE	LOAD FACTORS FOR RATING VEHICLE
			M _{PE,ULS} (kNm)	V _{PE} (kN)	T _{PE} (kNm)	M _{CE,ULS} (kNm)	V _{CE} (kN)	T _{CE} (kNm)	M _{LL,ULS} (kNm)	V _{LL} (kN)	T _{LL} (kNm)			
M1600 (4 LANES)	SPAN 1 BEAM 4	16.96	11659	92	239	0	0	0	18320	9	319	97%	M2	Y ₀ =1.8, DLA=0.3
T44 (2 LANES)	SPAN 2 BEAM 8	10.30	5223	22	51	0	0	0	5656	135	-51	100%	M1	Y ₀ =2.0, DLA=0.4
HLP 320 (1 LANE 50% M1600)	SPAN 1 BEAM 4	14.96	11677	93	334	1685	0	-29	15285	156	378	96%	M2	Y ₀ =1.5, DLA=0.1
HLP 400 (1 LANE 50% M1600)	SPAN 1 BEAM 4	16.16	11717	105	379	1650	-38	-62	18085	133	347	96%	M2	Y ₀ =1.5, DLA=0.1
GROUP 1, VEHICLE 1 (2 LANES)	SPAN 2 BEAM 8	9.10	5165	107	47	0	0	0	3130	-116	-49	100%	M1	Y ₀ =2.0, DLA=0.4
GROUP 1, VEHICLE 2 (3 LANES)	SPAN 1 BEAM 4	14.96	11677	93	334	0	0	0	8464	103	172	96%	M2	Y ₀ =2.0, DLA=0.4
GROUP 1, VEHICLE 3 (3 LANES)	SPAN 1 BEAM 4	14.96	11677	93	334	0	0	0	9357	108	190	96%	M2	Y ₀ =2.0, DLA=0.4
GROUP 1, VEHICLE 4 (3 LANES)	SPAN 1 BEAM 4	14.96	11677	93	334	0	0	0	9086	-100	186	96%	M2	Y ₀ =2.0, DLA=0.4
GROUP 2, VEHICLE 1 - 3.01*	SPAN 2 BEAM 8	9.00	5155	116	47	0	0	0	3286	-86	-110	100%	M1	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 1 - 3.70*	SPAN 2 BEAM 8	9.00	5155	116	47	0	0	0	3290	-91	-87	100%	M1	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 2 - 3.01*	SPAN 2 BEAM 8	9.10	5165	107	47	0	0	0	3720	111	-65	100%	M1	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 2 - 3.70*	SPAN 2 BEAM 8	9.10	5165	107	47	0	0	0	3575	103	-56	100%	M1	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 4*	SPAN 2 BEAM 8	10.30	5223	22	51	0	0	0	5096	69	-73	100%	M1	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 4 - NS*	SPAN 2 BEAM 8	10.30	5223	22	51	0	0	0	6022	82	-86	100%	M1	Y ₀ =1.5, DLA=0.3
GROUP 2, VEHICLE 5*	SPAN 2 BEAM 8	10.30	5223	22	51	0	0	0	6686	80	-138	100%	M1	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 5 - NS*	SPAN 2 BEAM 8	10.30	5223	22	51	0	0	0	7901	94	-163	100%	M1	Y ₀ =1.5, DLA=0.3
GROUP 2, VEHICLE 7 (1 LANE 50% M1600)	SPAN 1 BEAM 4	16.16	11717	105	379	199	-7	-15	19749	109	370	96%	M2	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 8 (1 LANE 50% M1600)	SPAN 1 BEAM 4	16.16	11717	105	379	199	-7	-15	24834	147	455	96%	M2	Y ₀ =1.5, DLA=0.1

TABLE 2 NOTES:

- * DENOTES NO ADVERSE ACTIONS FROM CO-EXISTING LOADS IN THE OPPOSITE CARRIAGEWAY. ACTIONS FROM ACCOMPANYING LOADS ARE CONSIDERED SEPARATELY FOR BENDING, SHEAR AND TORSION.
- * DENOTES CRITICAL LOCATIONS AT 2L_D DEVELOPMENT LENGTH OF DE-BONDED STRANDS IN ACCORDANCE WITH AS 5100.5:2017 CL.13.3.2.2. (NOT APPLICABLE FOR THIS EXAMPLE).
- CRITICAL LOCATION IS FROM THE CENTRELINE OF BEARING AT LOWEST CHAINAGE OF THE RESPECTIVE SPAN.
- DESIGN ACTIONS HAVE BEEN FACTORED BY ACCOMPANYING LANE FACTOR / MULTIPLE LANE MODIFICATION FACTOR, LOAD FACTOR AND DYNAMIC LOAD ALLOWANCE AS APPROPRIATE.
- TORSION IS CONSIDERED WHEN TOTAL FACTORED TORSION EXCEEDS THE TORSION LIMIT AS PER AS 5100.5:2017 CL.8.2.1.2.
- NEGATIVE T_{CE} OR T_{LL} INDICATE OPPOSITE DIRECTION TO T_{PE}.
- ACCOMPANYING DESIGN ACTIONS ARE THE MOST ADVERSE CONTRIBUTIONS FROM 50% M1600 LOADING IN THE OPPOSITE CARRIAGEWAY. THESE LOADS ARE DEDUCTED FROM THE AVAILABLE CAPACITY, TOGETHER WITH PERMANENT DESIGN ACTIONS.
- THE LONGITUDINAL BENDING LOAD RATING HAS BEEN CARRIED OUT AT VARIOUS SECTIONS ALONG THE SPAN AND AT EACH SECTION THE CASE WITH MAXIMUM TOTAL MOMENT (M_{MAX}), CORRESPONDING SHEAR AND TORSION HAS BEEN EXAMINED.
- % LONG. REINF. DEMAND FROM BENDING REPRESENTS THE LONGITUDINAL TENSILE FORCE DEMAND ASSOCIATED WITH THE DESIGN BENDING MOMENT AS A PROPORTION OF THE TOTAL TENSILE FORCE DEMAND ON THE CROSS-SECTION ACCOUNTING FOR THE EFFECTS OF AXIAL FORCE, BENDING MOMENT, SHEAR FORCE AND TORSIONAL MOMENT.
- FOR DEFINITION OF CONTROLLING DESIGN CASE REFER TO MRWA BBDIM (DOC 3912/02/04) SECTION 4.


TABLE 3 - DESIGN ACTIONS FOR COMBINED SHEAR AND TORSION AT CRITICAL LOCATIONS - LONGITUDINAL EFFECTS

VEHICLE LOAD CASE	CRITICAL SPAN & BEAM	CRITICAL LOCATION FROM A1 END SUPPORT (m)	PERMANENT ACTIONS			ACCOMPANYING ACTIONS			LIVE LOAD ACTIONS			CAPACITY			CONTROLLING DESIGN CASE	LOAD FACTORS FOR RATING VEHICLE	
			M _{PE,ULS} (kNm)	V _{PE} (kN)	T _{PE} (kNm)	M _{CE,ULS} (kNm)	V _{CE} (kN)	T _{CE} (kNm)	M _{LL,ULS} (kNm)	V _{LL} (kN)	T _{LL} (kNm)	φ _{VUS,VT} (kN)	% TRANS REINF. DEMAND FROM SHEAR (REFER NOTE 2)	φ _{VUC} (kN)			φ _{VUMAX} (kN)
M1600 (4 LANES)	SPAN 1 BEAM 4	1.93	1933	1370	378	0	0	0	3318	2331	480	N/A	N/A	1184	6447	V2	Y ₀ =1.8, DLA=0.3
T44 (2 LANES)	SPAN 2 BEAM 8	12.80	4896	246	71	0	0	0	4705	615	-68	N/A	N/A	398	5505	V3	Y ₀ =2.0, DLA=0.4
HLP 320 (1 LANE 50% M1600)	SPAN 2 BEAM 8	1.93	1422	904	178	58	36	-71	2074	1321	84	N/A	N/A	938	3476	V1	Y ₀ =1.5, DLA=0.1
HLP 400 (2 LANES 50% M1600)	SPAN 1 BEAM 4	2.19	2757	1318	383	787	138	0	3701	2089	1005	N/A	N/A	1146	6468	V2	Y ₀ =1.5, DLA=0.1
GROUP 1, VEHICLE 1 (2 LANES)	SPAN 2 BEAM 8	12.80	4896	246	71	0	0	0	2514	326	-49	N/A	N/A	397	5506	V3	Y ₀ =2.0, DLA=0.4
GROUP 1, VEHICLE 2 (2 LANES)	SPAN 1 BEAM 4	8.68	9241	683	348	0	0	0	5915	726	251	N/A	N/A	623	4256	V2	Y ₀ =2.0, DLA=0.4
GROUP 1, VEHICLE 3 (2 LANES)	SPAN 1 BEAM 4	8.68	9241	683	348	0	0	0	6791	847	325	1707	71%	630	4251	V5	Y ₀ =2.0, DLA=0.4
GROUP 1, VEHICLE 4 (2 LANES)	SPAN 1 BEAM 4	8.68	9241	683	348	0	0	0	6368	784	310	N/A	N/A	668	4224	V2	Y ₀ =2.0, DLA=0.4
GROUP 2, VEHICLE 1 - 3.01*	SPAN 2 BEAM 8	13.30	4748	293	-76	0	0	0	2409	356	190	847	73%	446	5420	V5	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 1 - 3.70 (1 LANE 50% M1600)	SPAN 1 BEAM 4	8.68	9241	683	348	200	6	0	4536	572	133	1830	78%	589	4283	V5	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 2 - 3.01*	SPAN 2 BEAM 8	13.30	4748	293	-76	0	0	0	2848	420	216	855	74%	443	5425	V5	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 2 - 3.70*	SPAN 2 BEAM 8	13.30	4748	293	-76	0	0	0	2753	402	194	867	75%	436	5437	V5	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 4*	SPAN 2 BEAM 8	13.30	4748	293	-76	0	0	0	3424	494	-200	N/A	N/A	404	5494	V3	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 4 - NS*	SPAN 2 BEAM 8	13.30	4748	293	-76	0	0	0	4046	583	-236	N/A	N/A	404	5494	V3	Y ₀ =1.5, DLA=0.3
GROUP 2, VEHICLE 5*	SPAN 2 BEAM 8	13.30	4748	293	-76	0	0	0	4106	602	333	837	72%	447	5419	V5	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 5 - NS*	SPAN 2 BEAM 8	13.30	4748	293	-76	0	0	0	4853	711	394	837	72%	447	5419	V5	Y ₀ =1.5, DLA=0.3
GROUP 2, VEHICLE 7 (1 LANE 50% M1600)	SPAN 1 BEAM 4	1.93	1933	1370	378	151	11	59	3119	2357	497	N/A	N/A	1185	6447	V2	Y ₀ =1.5, DLA=0.1
GROUP 2, VEHICLE 8 (1 LANE 50% M1600)	SPAN 1 BEAM 4	1.93	1933	1370	378	151	11	59	4030	2930	559	N/A	N/A	1184	6447	V2	Y ₀ =1.5, DLA=0.1

TABLE 3 NOTES:

IN ADDITION TO TABLE 2 NOTES:

- THE LOAD RATING HAS BEEN CARRIED OUT ALONG THE SPAN AND AT EACH SECTION THE FOLLOWING THREE CASES WERE EXAMINED:
 - MAXIMUM TOTAL MOMENT (M_{MAX}), CORRESPONDING SHEAR AND TORSION.
 - MAXIMUM TOTAL SHEAR (V_{MAX}), CORRESPONDING MOMENT AND TORSION.
 - MAXIMUM TOTAL TORSION (T_{MAX}), CORRESPONDING MOMENT AND SHEAR.
- % TRANSVERSE REINFORCEMENT DEMAND FROM SHEAR REPRESENTS THE TRANSVERSE SHEAR REINFORCEMENT DEMAND ASSOCIATED WITH THE SHEAR, V* AS A PROPORTION OF THE TOTAL DEMAND ASSOCIATED WITH COMBINED SHEAR, V* AND TORSION, T* (SCENARIO V5 ONLY).
- FOR DEFINITION OF CONTROLLING DESIGN CASE REFER TO MRWA BBDIM (DOC 3912/02/04) SECTION 4.

Rev.		DATE	DESCRIPTION	APPROVED	METADATA GROUND SURVEY STANDARD: DATE OF CAPTURE: MAPPING SURVEY STANDARD: DATE OF CAPTURE: MAIN ROADS PROJECT ZONE: HEIGHT DATUM:				DESIGNED	VERIFIER	PROJECT TITLE DRAWING TITLE MRWA DRAWING No. LOCAL AUTHORITY MAIN ROADS RESPONSIBILITY AREA STATUS DRAWING NUMBER REV		SHEET
											SIMPLY SUPPORTED BRIDGE DESIGN SUMMARY - SHEET N° 2 OF 3 SAMPLE ONLY		

SCALE

TABLE 4 - SLS DESIGN MOMENTS AT CRITICAL LOCATIONS - LONGITUDINAL EFFECTS

VEHICLE LOAD CASE	CRITICAL SPAN & BEAM	CRITICAL LOCATION FROM A1 END SUPPORT (m)	M _{PE,SLS} (kNm)	M _{CE,SLS} (kNm)	M _{LL,SLS} (kNm)	LOAD FACTORS FOR RATING VEHICLE
M1600 (3 LANES)	SPAN 2 BEAM 8	10.30	4190	0	4780	Y ₀ =1.0, DLA=0.3
T44 (2 LANES)	SPAN 2 BEAM 8	10.30	4190	0	2828	Y ₀ =1.0, DLA=0.4
HLP 320 (1 LANE 50% M1600)	SPAN 1 BEAM 4	16.26	9424	915	10282	Y ₀ =1.0, DLA=0.1
HLP 400 (1 LANE 50% M1600)	SPAN 1 BEAM 4	16.26	9424	915	12060	Y ₀ =1.0, DLA=0.1
GROUP 1, VEHICLE 1 (2 LANES)	SPAN 2 BEAM 8	9.10	4143	0	1565	Y ₀ =1.0, DLA=0.4
GROUP 1, VEHICLE 2 (2 LANES)	SPAN 2 BEAM 8	9.00	4135	0	2098	Y ₀ =1.0, DLA=0.4
GROUP 1, VEHICLE 3 (2 LANES)	SPAN 2 BEAM 8	9.00	4135	0	2344	Y ₀ =1.0, DLA=0.4
GROUP 1, VEHICLE 4 (2 LANES)	SPAN 2 BEAM 8	9.00	4135	0	2186	Y ₀ =1.0, DLA=0.4
GROUP 2, VEHICLE 1 - 3.01*	SPAN 2 BEAM 8	9.00	4135	0	2191	Y ₀ =1.0, DLA=0.1
GROUP 2, VEHICLE 1 - 3.70*	SPAN 2 BEAM 8	9.00	4135	0	2194	Y ₀ =1.0, DLA=0.1
GROUP 2, VEHICLE 2 - 3.01*	SPAN 2 BEAM 8	9.10	4143	0	2480	Y ₀ =1.0, DLA=0.1
GROUP 2, VEHICLE 2 - 3.70*	SPAN 2 BEAM 8	9.10	4143	0	2383	Y ₀ =1.0, DLA=0.1
GROUP 2, VEHICLE 4*	SPAN 2 BEAM 8	10.30	4190	0	3397	Y ₀ =1.0, DLA=0.1
GROUP 2, VEHICLE 4 - NS*	SPAN 2 BEAM 8	10.30	4190	0	4015	Y ₀ =1.0, DLA=0.3
GROUP 2, VEHICLE 5*	SPAN 2 BEAM 8	10.30	4190	0	4457	Y ₀ =1.0, DLA=0.1
GROUP 2, VEHICLE 5 - NS*	SPAN 2 BEAM 8	10.30	4190	0	5267	Y ₀ =1.0, DLA=0.3
GROUP 2, VEHICLE 7*	SPAN 2 BEAM 8	10.30	4190	0	6344	Y ₀ =1.0, DLA=0.1
GROUP 2, VEHICLE 8*	SPAN 2 BEAM 8	10.30	4190	0	7802	Y ₀ =1.0, DLA=0.1

TABLE 4 NOTES:

- DESIGN MOMENT HAS BEEN FACTORED BY MULTIPLE LANE MODIFICATION FACTOR / ACCOMPANYING LANE FACTOR, LOAD FACTOR AND DYNAMIC LOAD ALLOWANCE AS APPROPRIATE.
- *DENOTES NO ADVERSE ACTIONS FROM ACCOMPANYING LOADS IN THE OPPOSITE CARRIAGEWAY
- CRITICAL LOCATION IS FROM THE CENTRELINE OF BEARING AT LOWEST CHAINAGE OF THE SPAN.
- THE LONGITUDINAL BENDING RATING IS FOR THE CRITICAL LOCATION WHICH HAS BEEN IDENTIFIED THROUGH CHECKING AT VARIOUS SECTIONS ALONG THE SPAN.

TABLE 5 - LOAD RATINGS AT CRITICAL LOCATIONS

VEHICLE LOAD CASE	VEHICLE WIDTH (m)	SAG MOMENT LOAD RATING (%)		SHEAR LOAD RATING (%)	CONTROLLING DESIGN CASE
		SERVICEABILITY LIMIT STATE	ULTIMATE LIMIT STATE	ULTIMATE LIMIT STATE	
M1600	2.4	144%	98%	108%	M2
T44	2.2	244%	157%	162%	M1
HLP 320	3.6	135%	104%	105%	M2
HLP 400	4.5	115%	89%	101%	M2
GROUP 1, VEHICLE 1	2.4	443%	285%	304%	M1
GROUP 1, VEHICLE 2	2.4	331%	208%	226%	M2
GROUP 1, VEHICLE 3	2.4	296%	188%	194%	M2
GROUP 1, VEHICLE 4	2.4	318%	194%	201%	M2
GROUP 2, VEHICLE 1 - 3.01	3.01	317%	272%	280%	M1
GROUP 2, VEHICLE 1 - 3.70	3.70	317%	272%	302%	M1
GROUP 2, VEHICLE 2 - 3.01	3.01	280%	240%	239%	V5
GROUP 2, VEHICLE 2 - 3.70	3.70	291%	250%	251%	M1
GROUP 2, VEHICLE 4	3.70	203%	174%	219%	M1
GROUP 2, VEHICLE 4 - NS	3.70	172%	147%	185%	M1
GROUP 2, VEHICLE 5	3.01	155%	133%	164%	M1
GROUP 2, VEHICLE 5 - NS	3.01	131%	112%	139%	M1
GROUP 2, VEHICLE 7	4.81	109%	88%	105%	M2
GROUP 2, VEHICLE 8	6.22	88%	70%	85%	M2

TABLE 5 NOTES:

- TRANSVERSE DESIGN ACTIONS HAVE BEEN EXAMINED AND ARE GREATER THAN THE RATINGS FOR LONGITUDINAL BENDING AND SHEAR.
- SUBSTRUCTURE RATINGS HAVE BEEN EXAMINED AND ARE GREATER THAN THE RATINGS FOR LONGITUDINAL BENDING AND SHEAR.

GENERAL NOTES:

- PERMANENT EFFECTS COMPRISE OF SELF WEIGHT AND SUPERIMPOSED DEAD LOADS.
- NOMINAL ALLOWANCES FOR THE BRIDGE PER METRE RUN OF DECK ARE:
 100mm ASPHALT BETWEEN KERBS - 2.2kPa
 BARRIER - 1kN/m
 SELF WEIGHT BEAMS - 26kN/m³
 SELF WEIGHT INSITU DECK, MINIMUM THICKNESS - 5.1 kPa
 (PLUS ADDITIONAL SDL ALLOWANCES FOR THICKNESS OF UP TO 50mm AT ABUTMENT ENDS DUE TO ROAD PROFILE AND BEAM HOG)
- DESIGN VEHICLE IS SM1600 AS PER AS 5100.2:2017.
- LOAD EFFECTS HAVE BEEN BASED ON AN ELASTIC ANALYSIS OF THE STRUCTURE. THE STRUCTURE IS SIMPLY SUPPORTED.
- DYNAMIC LOAD ALLOWANCE (DLA) IS 0.3 FOR SM1600 IN ACCORDANCE WITH AS 5100.2-2017. DLA IS 0.4 FOR T44 AND GROUP 1 VEHICLES, AND 0.1 FOR HLP AND GROUP 2 VEHICLES IN ACCORDANCE WITH AS 5100.7:2017 AND MRWA BBDIM (DOC 3912/02/04).
- DLA IS 0.3 FOR UNSUPERVISED GROUP 2 VEHICLES. FOR DETAILS OF UNSUPERVISED MOVEMENT, REFER TO SECTION 4.3.4 OF MRWA BBDIM (DOC 3912/02/04).
- HLP VEHICLE POSITIONING IS IN ACCORDANCE WITH AS 5100.7:2017 CL.11.3.
- GROUP 2 VEHICLE POSITIONING IS IN ACCORDANCE WITH MRWA BBDIM (DOC 3912/02/04).
- SHEAR LOAD RATINGS INCLUDE AN ALLOWANCE FOR COMBINED SHEAR AND TORSION. COMBINED SHEAR AND TORSION IS CALCULATED IN ACCORDANCE WITH AS 5100.5-2017 SECTION 8.2 AND MAIN ROADS WA SES CIRCULAR 01/20.
- DISTRIBUTION FACTORS ARE THE RATIO BETWEEN MAXIMUM DESIGN ACTION FOR A BEAM AND TOTAL DESIGN ACTION FOR ALL BEAMS, FOR PURE BENDING AND SHEAR (WITHOUT THE EFFECTS TORSION). DISTRIBUTION FACTORS ARE FOR THE CRITICAL LOCATION FOR EACH VEHICLE, DISTRIBUTED PERPENDICULAR TO THE BEAM. CO-EXISTING EFFECTS ARE NOT INCLUDED.

NOTATION:

- A_{cp} = TOTAL AREA ENCLOSED BY OUTSIDE PERIMETER OF CONCRETE SECTION ENCASING TORSION REINFORCEMENT
- A_{ct} = AREA OF CONCRETE ON FLEXURAL TENSION SIDE OF MEMBER
- A_{st} = CROSS-SECTIONAL AREA OF LONGITUDINAL TENSILE REINFORCEMENT IN THE TENSILE HALF-DEPTH OF THE SECTION
- b_v = TOTAL WIDTH OF WEB(S) FOR SHEAR; OR EFFECTIVE WIDTH OF THE CRITICAL WEB IN AS 5100.5:2017 CL.8.2.1.2 ONLY.
- CE = CO-EXISTING EFFECTS
- DF = DISTRIBUTION FACTOR
- DL = DEAD LOADS ARE PERMANENT LOADS UNLIKELY TO VARY DURING THE USE OF THE STRUCTURE
- DLA = DYNAMIC LOAD ALLOWANCE
- d_n = DEPTH OF NEUTRAL AXIS FROM EXTREME COMPRESSION FIBRE
- I_g = SECOND MOMENT OF AREA OF THE GROSS CROSS-SECTION
- LL = LIVE LOAD
- M_{CE,SLS} = SERVICEABILITY DESIGN MOMENT DUE TO ACCOMPANYING LIVE LOAD
- M_{CE,ULS} = ULTIMATE DESIGN MOMENT DUE TO ACCOMPANYING LIVE LOAD
- M_{LL,SLS} = SERVICEABILITY DESIGN MOMENT DUE TO LIVE LOAD
- M_{LL,ULS} = ULTIMATE DESIGN MOMENT DUE TO LIVE LOAD
- M_{PE,SLS} = SERVICEABILITY DESIGN MOMENT DUE TO ALL PERMANENT EFFECTS
- M_{PE,ULS} = ULTIMATE DESIGN MOMENT DUE TO ALL PERMANENT EFFECTS
- M_s = SERVICEABILITY CAPACITY IN BENDING (PER BEAM)
- NS = NON-SUPERVISED VEHICLE MOVEMENT. REFER MRWA BBDIM (DOC 3912/02/04).
- PE = ALL PERMANENT EFFECTS (DL + SDL)
- s = CENTRE-TO-CENTRE SPACING OF SHEAR/TORSIONAL REINFORCEMENT
- SDL = SUPERIMPOSED DEAD LOADS ARE PERMANENT LOADS WHICH MAY VARY DURING THE USE OF THE STRUCTURE (IE. TEMPORARY KERBS, BARRIERS, FOOTPATHS, ASPHALT THICKNESS)
- SLS = SERVICEABILITY LIMIT STATE
- T_{CE} = ULTIMATE DESIGN TORSION DUE TO CO-EXISTING LIVE LOAD
- T_{LL} = ULTIMATE DESIGN TORSION DUE TO LIVE LOAD
- T_{PE} = ULTIMATE DESIGN TORSION DUE TO ALL PERMANENT EFFECTS
- u_c = LENGTH OF OUTSIDE PERIMETER OF CONCRETE CROSS-SECTION ENCASING TORSION REINFORCEMENT
- ULS = ULTIMATE LIMIT STATE
- V_{CE} = ULTIMATE DESIGN SHEAR DUE TO ACCOMPANYING LIVE LOAD
- V_{LL} = ULTIMATE DESIGN SHEAR DUE TO LIVE LOAD
- V_{PE} = ULTIMATE DESIGN SHEAR DUE TO ALL PERMANENT EFFECTS
- z = INTERNAL MOMENT LEVER ARM OF THE SECTION
- ȳ = DISTANCE TO NEUTRAL AXIS FROM BOTTOM OF SECTION
- Y_{DL} = DEAD LOAD FACTOR. REFER AS 5100.2:2017 T.6.2.
- Y_Q = TRAFFIC LOAD FACTOR. REFER AS 5100.2:2017 T.7.10(A) & MRWA BBDIM (DOC 3912/02/04).
- Y_{SDL} = SUPERIMPOSED DEAD LOAD FACTOR. REFER AS 5100.2:2017 T.6.3.
- σ_{cp} = AVERAGE INTENSITY OF EFFECTIVE PRESTRESS IN CONCRETE AT THE CENTROID, OR AT THE JUNCTION OF THE WEB AND FLANGE WHEN THE CENTROID LIES INSIDE THE FLANGE. REFER AS 5100.5:2017 CL.8.2.1.2..
- φ = CAPACITY REDUCTION FACTOR (0.8 FOR BENDING AND 0.7 FOR SHEAR/TORSION)
- φM_U = ULTIMATE CAPACITY IN BENDING (PER BEAM)
- φV_{us,vt} = CONTRIBUTION OF SHEAR REINFORCEMENT TO THE ULTIMATE SHEAR STRENGTH (PER BEAM) ADJUSTED BY TRANSVERSE SHEAR REINFORCEMENT DEMAND ASSOCIATED WITH THE SHEAR AS A PROPORTION OF THE TOTAL DEMAND FROM COMBINED SHEAR AND TORSION, ONLY WHEN SCENARIO V5 IS CONTROLLING.

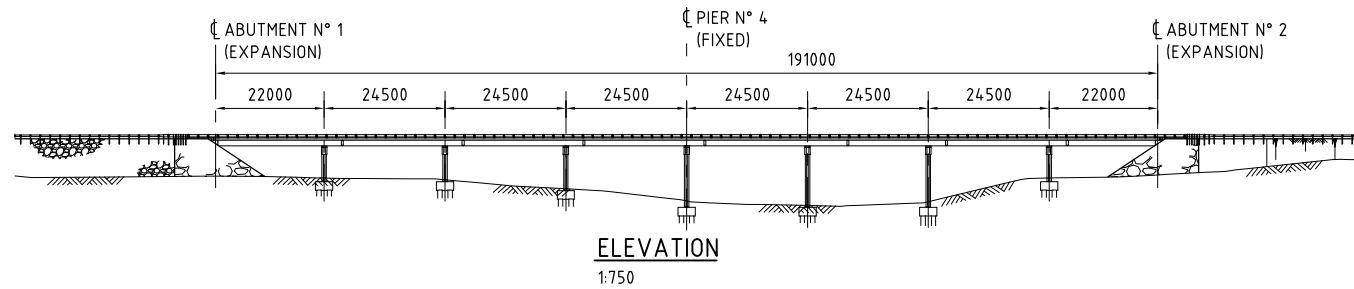
FOR ALL OTHER DEFINITIONS REFER TO AS 5100.5:2017.

TABLE 6 - DISTRIBUTION FACTORS

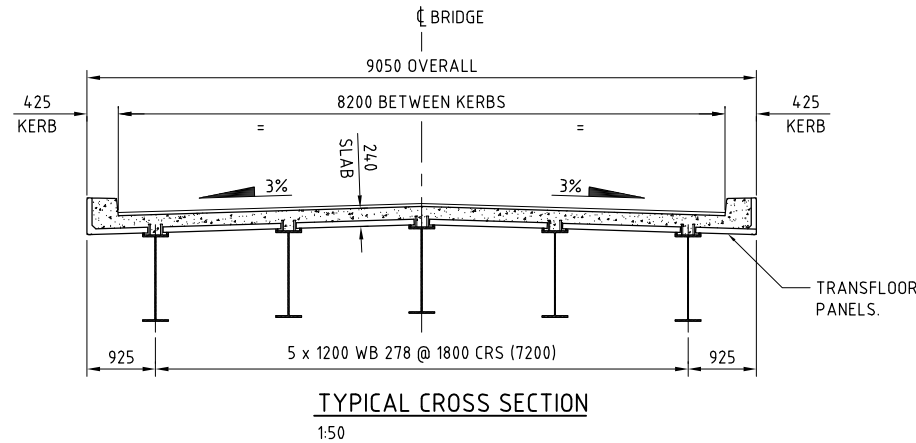
VEHICLE LOAD CASE	SAG MOMENT AT CRITICAL LOCATION		SHEAR AT CRITICAL LOCATION	
	CRITICAL SPAN & BEAM	DF	CRITICAL SPAN & BEAM	DF
M1600	SPAN 1 BEAM 4	0.467	SPAN 1 BEAM 4	0.524
T44	SPAN 2 BEAM 8	0.674	SPAN 2 BEAM 8	0.597
HLP 320	SPAN 1 BEAM 4	0.603	SPAN 2 BEAM 8	0.546
HLP 400	SPAN 1 BEAM 4	0.605	SPAN 1 BEAM 4	0.633
GROUP 1, VEHICLE 1	SPAN 2 BEAM 8	0.686	SPAN 2 BEAM 8	0.565
GROUP 1, VEHICLE 2	SPAN 1 BEAM 4	0.464	SPAN 1 BEAM 4	0.694
GROUP 1, VEHICLE 3	SPAN 1 BEAM 4	0.472	SPAN 1 BEAM 4	0.734
GROUP 1, VEHICLE 4	SPAN 1 BEAM 4	0.472	SPAN 1 BEAM 4	0.674
GROUP 2, VEHICLE 1 - 3.01	SPAN 2 BEAM 8	0.673	SPAN 2 BEAM 8	0.630
GROUP 2, VEHICLE 1 - 3.70	SPAN 2 BEAM 8	0.672	SPAN 1 BEAM 4	0.697
GROUP 2, VEHICLE 2 - 3.01	SPAN 2 BEAM 8	0.676	SPAN 2 BEAM 8	0.539
GROUP 2, VEHICLE 2 - 3.70	SPAN 2 BEAM 8	0.651	SPAN 2 BEAM 8	0.503
GROUP 2, VEHICLE 4	SPAN 2 BEAM 8	0.669	SPAN 2 BEAM 8	0.565
GROUP 2, VEHICLE 4 - NS	SPAN 2 BEAM 8	0.669	SPAN 2 BEAM 8	0.565
GROUP 2, VEHICLE 5	SPAN 2 BEAM 8	0.663	SPAN 2 BEAM 8	0.576
GROUP 2, VEHICLE 5 - NS	SPAN 2 BEAM 8	0.663	SPAN 2 BEAM 8	0.576
GROUP 2, VEHICLE 7	SPAN 1 BEAM 4	0.596	SPAN 1 BEAM 4	0.629
GROUP 2, VEHICLE 8	SPAN 1 BEAM 4	0.582	SPAN 1 BEAM 4	0.615

Rev.	DATE	DESCRIPTION	APPROVED	METADATA		 INFRASTRUCTURE DELIVERY DIRECTORATE	DESIGNED	DRAWN	CHECKED	DRAWING PURPOSE	VERIFIER	DESIGN MANAGER APPROVED	ALLIANCE PROJECT MANAGER APPROVED	PROJECT TITLE			SHEET A1
				GROUND SURVEY STANDARD:										DRAWING TITLE			
				DATE OF CAPTURE:						MRWA DRAWING No.			LOCAL AUTHORITY		MAIN ROADS RESPONSIBILITY AREA		
				MAPPING SURVEY STANDARD:						STATUS			DRAWING NUMBER		REV		
				DATE OF CAPTURE:													
				MAIN ROADS PROJECT ZONE:													
				HEIGHT DATUM:													

1 SPAN CONFIGURATION



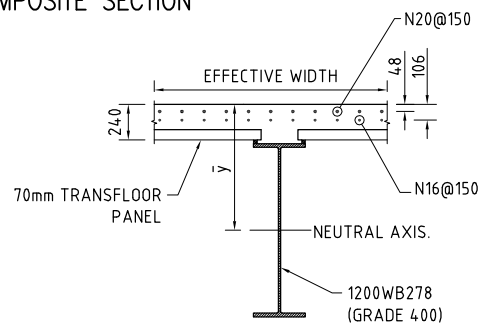
2 DESIGN CRITICAL SECTION



3 PROPERTIES OF TRANSFORMED COMPOSITE SECTION

TABLE 3.1

LOCATION	ABUTMENTS & PIERS	MID SPAN
EFFECTIVE WIDTH (m)	1.8	1.8
A (m ²)	0.04152	0.08895
I comp. (m ⁴)	0.01058	0.01941
\bar{y} (m)	0.714	0.380



$f_{sy} = 500\text{MPa}$
 $f'_c = 40\text{MPa}$
 $E_c = 35000\text{MPa}$
 $E_s = 200000\text{MPa}$

NOTES (TABLE 3.1)

1. I comp. IS BASED ON AN EQUIVALENT STEEL SECTION.

4 TRANSVERSE DISTRIBUTION FACTORS FOR LIVE LOADS

TABLE 4.1

VEHICLE	SAG	HOG	SHEAR
M1600 (2 VEH.)	0.271	0.263	0.267
T44 & GROUP 1 VEHICLES (2 VEH.)	0.288	0.281	0.290
L44 (2 LANES)	-	0.251	-
GROUP 2 VEHICLE 4 (3.7m O/A WIDTH)	0.267	0.292	0.301
GROUP 2 VEHICLE 5 (3.01m O/A WIDTH)	0.269	0.298	0.315
GROUP 2 VEHICLE 7 (4.81m O/A WIDTH)	0.275	0.278	0.279
GROUP 2 VEHICLE 8 (6.22m O/A WIDTH)	0.232	0.243	0.242

NOTES (TABLE 4.1)

1. M1600 AND T44/L44 DISTRIBUTION FACTORS ARE FOR THE MOST CRITICAL LANE LOADING, INCLUDING THE APPROPRIATE ACCOMPANYING LANE FACTORS OR LANE MODIFICATION FACTORS.
2. DISTRIBUTION FACTORS DO NOT INCLUDE DYNAMIC LOAD ALLOWANCE.
3. GROUP 2 VEHICLE DISTRIBUTION FACTORS ARE GIVEN FOR A SINGLE VEHICLE TRAVELLING DOWN THE CENTRE LINE OF THE BRIDGE ± 1 METRE.

5 TYPICAL DESIGN MOMENTS AND SHEARS AT CRITICAL LOCATIONS

TABLE 5.1 ULTIMATE LIMIT STATE

LOAD CASE	SAG (kNm)	HOG (kNm)	SHEAR (kN)	NOTES
PE	295	1223	104	1.4SDL+1.2S+1.5DS
M1600 (2 VEH.)	3212	2647	900	$\gamma_L=1.8, DLA=0.3$
T44 (2 VEH.)	2245	-	552	$\gamma_L=2.0, DLA=0.4$
L44 (2 LANES)	-	1453	-	$\gamma_L=2.0, DLA=0.4$
GROUP 2 VEHICLE 4	1922	1352	560	$\gamma_L=1.5, DLA=0.1$
GROUP 2 VEHICLE 5	2587	1537	759	$\gamma_L=1.5, DLA=0.1$
GROUP 2 VEHICLE 7	3844	2576	1027	$\gamma_L=1.5, DLA=0.1$
GROUP 2 VEHICLE 8	4323	2968	1186	$\gamma_L=1.5, DLA=0.1$

TABLE 5.2 SERVICEABILITY LIMIT STATE

LOAD CASE	HOG (kNm)	NOTES
PE	967	1.0SDL+1.0S+1.0DS
M1600 (2 VEH.)	1471	$\gamma_L=1.0, DLA=0.3$

NOTES (TABLE 5.1 & 5.2)

1. LOAD EFFECTS HAVE BEEN CALCULATED BASED ON AN ELASTIC ANALYSIS OF THE STRUCTURE. CRACKED SECTION PROPERTIES ARE ADOPTED OVER 15% OF SPAN LENGTH BOTH SIDES OF PIERS.

6 AVAILABLE LIVE LOAD CAPACITY

TABLE 6.1 MOMENT CAPACITY

ULTIMATE LIMIT STATE	SAG (kNm)	HOG (kNm)
$\phi M_u - M_{ULT,PE} - 1.0 M_{DT}$	6686	2673
SERVICEABILITY LIMIT STATE	HOG (kNm)	
$M_s (f_s = 280\text{MPa}) - M_{SERV,PE} - 0.5 M_{DT} - 0.5 M_{VW}$	3416	

TABLE 6.2 SHEAR CAPACITY

ULTIMATE LIMIT STATE	SHEAR (kN)
$\phi V_u - V_{ULT,PE} - 1.0 V_{DT}$	2921

NOTES (TABLE 6.1 & 6.2)

1. DEAD LOAD EFFECTS PRODUCED FROM CONSTRUCTION STAGING HAVE BEEN INCORPORATED IN A REDUCED STEEL BEAM f_y USED TO CALCULATE ULTIMATE MOMENT CAPACITY ABOVE.
2. SERVICEABILITY CAPACITY IN BENDING IS BASED ON A MAX STRESS OF 280MPa IN THE DECK STEEL REINFORCEMENT.

SYMBOLS USED

- A - EFFECTIVE AREA OF SECTION
- DLA - DYNAMIC LOAD ALLOWANCE
- DS - DIFFERENTIAL SETTLEMENT
- E_c - MODULUS OF ELASTICITY OF CONCRETE AT 28 DAYS
- E_s - MODULUS OF ELASTICITY OF STEEL
- f'_c - CHARACTERISTIC COMPRESSIVE CYLINDER STRENGTH OF CONCRETE AT 28 DAYS
- f_s - ALLOWABLE STRESS IN ORDINARY REINFORCEMENT
- f_{sy} - YIELD STRESS OF ORDINARY REINFORCEMENT
- I comp. - EFFECTIVE SECOND MOMENT OF AREA OF COMPOSITE SECTION
- M_{DT} - SERVICEABILITY MOMENT DUE TO DIFFERENTIAL TEMPERATURE
- M_s - SERVICEABILITY CAPACITY IN BENDING
- $M_{SERV,PE}$ - SERVICEABILITY MOMENT DUE TO ALL PERMANENT EFFECTS
- M_u - ULTIMATE CAPACITY IN BENDING
- $M_{ULT,PE}$ - ULTIMATE MOMENT DUE TO ALL PERMANENT EFFECTS
- M_{VW} - SERVICEABILITY MOMENT DUE TO VERTICAL WIND
- PE - PERMANENT EFFECTS
- S - SHRINKAGE
- SDL - SUPERIMPOSED DEAD LOAD
- V_{DT} - SERVICEABILITY SHEAR DUE TO DIFFERENTIAL TEMPERATURE
- $V_{ULT,PE}$ - ULTIMATE SHEAR DUE TO ALL PERMANENT EFFECTS
- V_v - ULTIMATE CAPACITY IN SHEAR
- \bar{y} - DISTANCE TO NEUTRAL AXIS, AS PER SECTION 3
- γ_L - LOAD FACTOR FOR LIVE LOAD
- ϕ - CAPACITY REDUCTION FACTOR

NOTES:

1. FOR GENERAL NOTES REFER TO SHEET 2

THIS DRAWING IS AN AMENDMENT OF THE APPROVED DRAWING.

No.	DATE	DESCRIPTION	AUTHORISED
AMENDMENTS			
CLIENT			
CONSULTANT			
PLANNING AND TECHNICAL SERVICES DIRECTORATE STRUCTURES ENGINEERING			
Telephone (08) 9323 4111		Fax (08) 9323 4136	
FILE No.	JOB No.		
DRAWN	DESIGNED		
CHECKED	VERIFIED		
APPROVED			



GUIDE DRAWING
CONTINUOUS COMPOSITE BRIDGE
DESIGN SUMMARY - SHEET N° 1 OF 2
SAMPLE ONLY

LOCAL AUTHORITY () DRAWING NUMBER AMEND.

1

SCALE 1:50 MICROFILM DATE A 1

SECTION 3 – REFURBISHMENT AND STRENGTHENING DESIGN

This information is Section 3 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As the head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information



A LIM

SENIOR ENGINEER STRUCTURES

Date: 04/09/2023

Document No: 3912/02-3

Controlled Copies shall be marked accordingly

SECTION 3

CONTENTS

3	REFURBISHMENT AND STRENGTHENING DESIGN	3
3.1	Introduction	3
3.2	Non-Timber Bridges	3
3.3	Timber Bridges.....	3
3.4	Construction Considerations	4

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	24/01/06	Complete review for introduction of AS 5100-2004 and 6706-02-2227.
3	2	30/07/10	Addition of new section 3.4
All	3	30/08/18	Complete review for introduction of AS5100-2017
All	4	04/09/23	Amended 3.1 Stage 2

Custodian Endorsement

M RAJAKARUNA

Structures Design & Standards Engineer

Date: 04/09/2023

3 REFURBISHMENT AND STRENGTHENING DESIGN

3.1 Introduction

This Section of the Design Information Manual shall be used for the design of refurbishment and strengthening of existing bridges.

The refurbishment and strengthening design process is essentially split into two basic stages as follows:

Stage 1 – Load Rating

This stage analyses the load capacity of the existing structure in its current condition to determine structural deficiencies. It involves modelling the bridge in its current form utilising all available information on actual geometric, material and condition parameters. The load rating stage shall be carried out in accordance with Section 4 “Load Rating Existing Bridges” for non-timber bridges, or Document No. 6706-02-2227 “Load Rating and Refurbishment Design Manual for Existing Timber Bridges” for timber bridges.

The designer is required to confirm the analysis vehicles with EBL.

Stage 2 – Refurbishment and/or Strengthening Design

This stage follows logically from stage 1, which has identified areas of structural deficiency or zones requiring strengthening to accommodate the required refurbishment (widening, raising, strengthening, additional traffic lanes etc). The refurbishment and/or strengthening design stage shall be carried out in accordance with the requirements detailed below.

Design shall be in accordance with the Code and Section 2 of this Manual except that design life may be modified as appropriate to the remaining service life of the existing bridge.

The designer is required to confirm the design vehicles with EBL.

3.2 Non-Timber Bridges

Refurbishment and strengthening designs shall be to the Code except where varied by the Bridge Branch Design Information Manual. If it has been demonstrated that Code standards cannot be achieved then a lower level of service may be accepted.

3.3 Timber Bridges

Refurbishment and strengthening designs for existing timber bridges shall be carried out in accordance with the “Load Rating and Refurbishment Design Manual for Existing Timber Bridges”, Document No. 6706-02-2227.

The design shall, as far as practical, include the appropriate standard repair details contained within the Pavements & Structures Engineering Practice Notes, Document Nos. 6702/02/221, 222, 223. Such details are provided for general information only. Although structural sizes are given, reference must be made to approved drawings for each specific job, and all standard details must be assessed and confirmed as suitable by an engineering analysis.

South-West Region and Structures Engineering are developing Project Standard Drawings. These are akin to Standard Drawings for timber maintenance/refurbishment. Until such time as these are authorised by SES, all Project Standard Drawings are to be treated as project specific drawings. That is, given a project specific drawing number and submitted for review alongside other project specific drawings.

3.4 Construction Considerations

During construction of a refurbishment or strengthening design it is common for the road to remain at least partially open to traffic. The Designer must provide for this in the design by either propping various elements as required or designating traffic restrictions that are required.

The bridge must be analysed for each stage during construction (for example, a two stage RCO construction), giving allowable traffic loads for at least the three modes of tri-axle group vehicles if applicable, outlined in Document No. 6706-02-2227 "Load Rating and Refurbishment Design Manual for Existing Timber Bridges" for timber bridges and the Group 1 Vehicle 2 and Group 2 Vehicle 1 at both spreads in as per Appendix D in Section 4 "Load Rating Existing Bridges" for non-timber bridges. This information is required for heavy load assessments during construction and shall be forwarded to EBL prior to construction.

Construction staging and associated load restrictions should also be specified on the Drawings in line with staged load assessments as above.

SECTION 4 – LOAD RATING OF BRIDGES

This information is Part 4 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

Engineer Bridge Loading is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As the head of Structures Engineering of Main Roads Western Australia,
I authorise this issue and the use of this Information.



A LIM
SENIOR ENGINEER STRUCTURES

Date: 04/09/2023

Document No: 3912/02-4

Controlled Copies shall be marked accordingly

SECTION 4

CONTENTS

4.	LOAD RATING OF BRIDGES	4
4.1	Introduction	4
4.2	Flowchart For Non-Timber Bridge Load Rating	4
4.3	Identify Bridge Properties And Condition Assessment	5
4.4	Identify Rating Vehicles.....	7
4.5	Calculate Projected Future Traffic Load Demand	14
4.6	Prepare Bridge Model And Calculate Action Effects	15
4.7	Capacity And Load Rating.....	16
	Appendix A - Typical Steel Section Properties (Old Imperial Beams).....	20
	Appendix B - Example Load Rating Calculation of a Prestressed Concrete Tee-Roff Beam.....	23
B.1	Determine section and material properties.....	25
B.2	ΦMu Calculation.....	26
B.3	Calculate effective shear depth dv	27
B.4	$0.25 \Phi Tcr$ Calculation	28
B.5	Calculate Load Rating Factor $kM1$ for Scenario M1	30
B.6	Calculate Load Rating Factor $kM2$ for Scenario M2.....	31
B.7	Calculate Load Rating Factor $kM3$ for Scenario M3	35
B.8	Calculate Load Rating Factor $kM4$ for Scenario M4.....	39
B.9	Calculate Load Rating Factor $kV1$ for Scenario V1.....	40
B.10	Calculate Load Rating Factor $kV2$ for Scenario V2.....	44
B.11	Calculate Load Rating Factor $kV3$ for Scenario V3 and $kV4$ for Scenarios V4..	47
B.12	Calculate Load Rating Factor $kV5$ for Scenario V5.....	48
	Appendix C - Example of Load Rating Memo and Report	53
C.1	Memorandum	53
C.2	Load Rating Report	56

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	24/01/06	Complete review for introduction of AS 5100 (2004) and 6706-02-2227
6	2	10/01/07	Section 4.3.4 - Paragraph 1 amended to include “..all design vehicles”
21	3	14/3/07	Note diagram amended
8-10	4	04/03/11	Differential temperature amended
All	5	13/1/12	Updated load rating vehicles and added Appendix F.
All	6	06/07/22	Complete review against AS 5100 (2017).
All	7	04/09/23	Minor update and corrections

Custodian Endorsement

R Hossain
Engineer Bridge Loading (EBL)
Date: 04/09/2023

4. LOAD RATING OF BRIDGES

4.1 INTRODUCTION

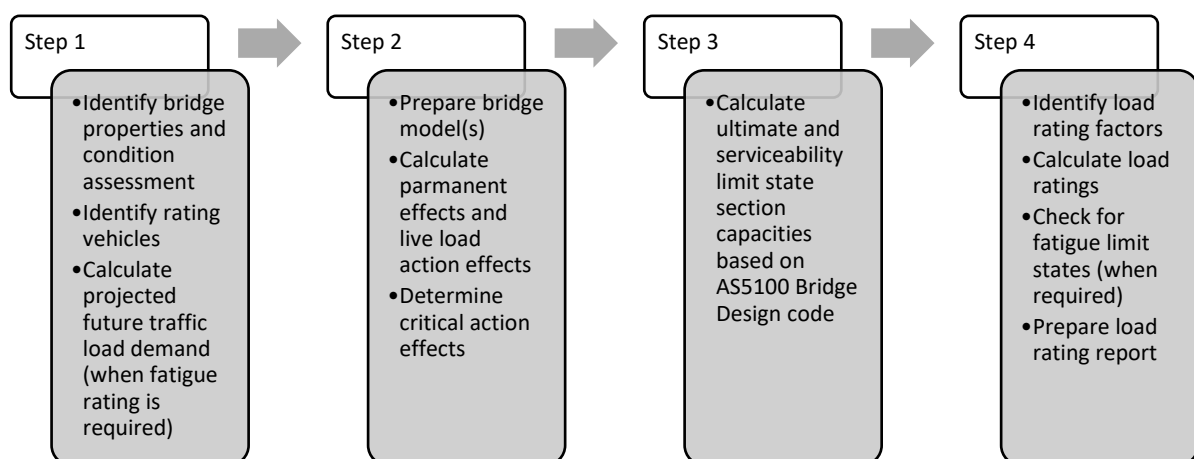
This Section of the Manual shall be used to determine the load rating of non-timber bridges in Western Australia (WA), and to determine the load limit posting requirements for bridges with deficient load capacity. Load rating of existing timber bridges shall be carried out in accordance with the “Load Rating and Refurbishment Design Manual for Existing Timber Bridges”, Document No. 6706-02-2227.

Load ratings are carried out on all new bridges as well as existing bridges. For new bridges the load rating results should be provided as part of the detailed drawing set and referred to as the Design Summary Sheets (DSS). If the load rating of an existing bridge indicates that a bridge is incapable of accommodating Vehicle Standard Regulation (VSR) loads, then, in the interests of public safety, the structure is either repaired or a load limit is posted.

The objective of load rating a bridge is to determine its safe live load carrying capacity in terms of the percentage of each rating vehicle’s action effect. These calculated bridge load ratings are used to update the bridge rating values in the MRWA bridge database, which are used for the assessment of heavy haulage movements throughout the State on publicly accessible roads.

All components of the bridge, including its foundation, should be considered to ensure that all relevant components are load rated. While the general analytical approach for load rating should follow the AS 5100 (2017) Bridge Design code, this Section 4 provides additional guidelines for a standardised approach for analysing bridges and reporting the load rating outcomes. Refer flowchart guideline in Figure 4.1 below.

4.2 FLOWCHART FOR NON-TIMBER BRIDGE LOAD RATING



Note: The above steps are guide only.

Figure 4.1 Bridge Load Rating Process Flowchart

4.3 IDENTIFY BRIDGE PROPERTIES AND CONDITION ASSESSMENT

The first step in carrying out a load rating is to obtain accurate up-to-date drawings of the bridge. These will usually be available from the MRWA Structures Engineering Drawing Office in pdf format. A full set of drawings should be obtained to be able to check for any non-standard features, with all as-constructed, repair, refurbishment details, etc noted.

Also obtain a copy of the latest detailed inspection report or arrange to have an inspection carried out if requested. Although assessments are usually on the basis of “as-new” condition, the actual state of the bridge is obviously important and could lead to a downgrading of the assessed capacity. Where actual material properties are known, these should be incorporated into the rating analysis.

It is also valuable to check the old bridge records and files in the Heavy Loads Group office. Although information on all bridges may not be available, these files often contain material not recorded elsewhere, which could have an important bearing on the bridge capacity, e.g. information on past load approvals, details of precast members, load tests, load limits, etc.

If detailed drawings are not available for a bridge, alternate methods such as local breakouts, destructive/non-destructive testing or bridge load testing can be utilised to determine the load rating within the provisions of the AS 5100 (2017) code. The details of these alternate methods are beyond the scope of this guideline.

Care is necessary when reading old drawings, especially pre-metric ones. Imperial dimensions can be converted readily, but care is needed with concrete strengths, reinforcement sizes and grades, prestressing steel grade, and structural steelwork sizes and grades.

4.3.1 Concrete

On old drawings, concrete strengths are given in pounds per square inch or “psi”, and on the older bridges this will be the crushing strength of a standard 6” cube, rather than the cylinder strength. The cube strength is not exactly the same as the cylinder strength. However, with concrete so old, and given that concrete crushing is rarely a limiting factor, it is usually accurate enough to make a direct conversion, as below:

3,000 psi = 20 MPa

4,500 psi = 30 MPa

6,000 psi = 40 MPa

7,500 psi = 50 MPa

Old concretes generally exceeded the minimum specification requirements for strength, so using concrete strengths on the drawings will generally be conservative. If the decision to strengthen is based purely on the assumption of concrete strength, material sampling can be undertaken within the provisions of the AS 5100 (2017) code.

4.3.2 Reinforcement

Imperial reinforcement is called up either by diameter, e.g. $\frac{5}{8}$ " @ 6" c/c, or by a number, e.g. D9045 @ 8" c/c. The first is reasonably straightforward. In the second, the first digit, (or the first two if the bar diameter $\geq 1\frac{1}{4}$ "), is the bar diameter in $\frac{1}{8}$ ", e.g., 9=1 $\frac{1}{8}$ ", the rest is the bar mark.

The grade of old reinforcement will generally be either of the following.

- ordinary mild steel (plain or deformed), with a yield of 230 MPa and an allowable stress of 125 MPa, also known as Grade S, or Structural Grade, or
- cold worked deformed, also known as CW60, with a yield of 410 MPa and an allowable stress of 170 MPa.
- Refer Section 6 for other reinforcement stress limits

The grade should be stated on the drawings, but generally only mild steel was available until the mid-late 60s, with cold worked steel gradually replacing it and taking over almost completely by the mid 70s. If in doubt refer to the bar schedules, which were usually included with the drawings. Mild steel could be bent round a 2D pin, whereas cold worked used a minimum of 4D. Take care though, as often cold worked was used for the main straight bars and mild steel for stirrups and ligatures. If still in doubt, it is possible to take a sample for testing, from a non-critical region, otherwise err on the side of caution. Refer also to DIS 3912/02-6 "Stress Limits in Structural Concrete" for allowable stresses for various steel grades.

A conversion table for imperial bars is provided below:

Bar Diameter (inches)	$\frac{3}{8}$ "	$\frac{1}{2}$ "	$\frac{5}{8}$ "	$\frac{3}{4}$ "	$\frac{7}{8}$ "	1"	1 $\frac{1}{8}$ "	1 $\frac{1}{4}$ "	1 $\frac{3}{8}$ "
Bar Area (mm ²)	71	126	198	285	388	506	641	792	958

Refer also to the Steel Reinforcement Institute of Australia's "Guide to Historical Steel Reinforcement in Australia" and AS 5100.7:2017 Appendix A.

4.3.3 Prestress

Prestressing steel details must be checked to obtain the correct properties. Usually, even on the older bridges, for wire or strand the yield will be around 1700 MPa and 1250 MPa for prestressing bar.

Sometimes, the tendon capacity can be reported in imperial tons per square inch. (1 ton = 2,240 lbs). For example, *0.276" dia. 100-110 Tons Ultimate H.T. Wire with stresses in wires after release to be 138,000psi at 85°F* can be interpreted as the ultimate strength (i.e., breaking strength) of the HT steel used in the 0.276" dia. prestressing wire was 100 to 110 tons per square inch. Taking a mean value of 105 tons/in², this equates to (105 x 2,240) = 235,200 psi. Usually, wires were pre-tensioned to about 70% UTS (ultimate tensile strength) and allowing for some losses, the stress in each wire at release would be about 60% of UTS – that is: (235,200 x 0.6) = 141,120psi which is close to the 138,000 psi quoted in the sketch.

One issue with older prestressing steel is that it will probably be normal relaxation, as low relaxation steel only became generally available in the mid-70s. This will considerably increase long-term losses. It may be difficult to identify the steel in older bridges, especially in prefabricated, precast elements, as a number of different types, including a lot of imported steel were used. With prestress it is not usually possible to take a sample for testing, except perhaps from the end of a pre-tensioned member, so again err on the side of caution.

Structural Steelwork - Structural steelwork in older bridges, e.g., rolled or fabricated beams, can be of a number of different sizes, grades and origins. For the more recent of the older bridges, i.e., post 1960, beams will probably be BHP RSJs or UBs, Grade 250. Section properties for some of these pre-metric beams are attached at Appendix A. Older beams may well be imported, usually from England, and detailed measurements will have to be taken to calculate section properties. Grade 250 can usually be assumed safely, but some really old beams, (e.g., Horseshoe and Barrack St Bridges), were made of a very brittle, high carbon steel and should be checked carefully, and perhaps a sample taken for testing. Higher strength grades should only be used where they are clearly indicated on the drawings.

4.4 IDENTIFY RATING VEHICLES

For non-timber bridges, unless otherwise specified, ratings shall be carried out for all design vehicles as per code and rating vehicles detailed in this section as well as any additional design vehicles specified for a particular bridge (ex. additional vehicles for Oversize and Over-Mass Vehicle Corridors). EBL shall also be consulted for any special vehicle loadings requiring load rating. Other loads needed to be considered for load rating shall be in accordance with AS 5100.7:2017 bridge assessment code. It is important to use the correct dimensions and axle loads. Where dimensions can vary, the full range of axle spacing must be investigated, as different lengths may be critical for sag and hog moments. Please note, for new bridge design, if there is any conflict between the specifications/requirements and guidelines presented in this document, EBL shall be consulted for resolution prior to proceeding for the final design.

4.4.1 SM1600 Vehicles

As per AS 5100 (2017) code. While positioning vehicles in the most onerous position, any temporary or mountable median/verge/footpath/kerb needs to be ignored and vehicles must be positioned between full width of the bridge between traffic barriers as per Cl. 7.5 of AS5100.2:2017.

4.4.2 T44 Trucks

The T44 truck load shall consist of the magnitude and positioning of loads described in Clause A2.2.2 of AS 5100.7:2004 code/Section 16 of Bridge Branch Design Information Manual (BBDIM). The dynamic load allowance (DLA) shall be calculated based on AS 5100.7:2017 Cl. 11.3.6 and lane modification factors (LMF) shall be calculated based on AS 5100.7:2004 Table A2. To identify the most critical loading pattern for multilane carriageways, all vehicle combinations shall be considered with appropriate (LMF) including the single vehicle case positioned in the most onerous position.

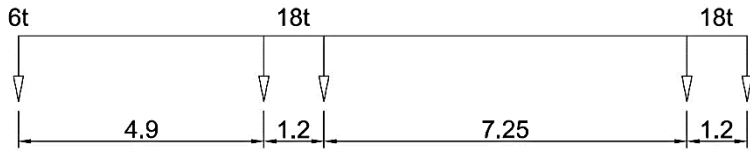
On longer bridges, there is a possibility of getting multiple loaded vehicles in a lane at the same time. Considering such ‘travel in convoy’ scenario, the minimum headway should be 15 metres measured between the rear axle of the front vehicle and the front axle of the rear vehicle in the same lane.

For any carriageway width, the vehicles shall be positioned in the most onerous position (while positioning vehicles in the most onerous position, any temporary or mountable median/verge/footpath/kerb needs to be ignored and vehicles must be positioned between traffic barriers) within the carriageway for the section under consideration but the centre-line of the dual tyre should not be closer than 600 mm to the face of the kerb or not closer than 1200 mm to the centre-line of the dual tyre of the accompanying T44 vehicle (refer to Figure A6 (a) of AS 5100.7:2004 code).

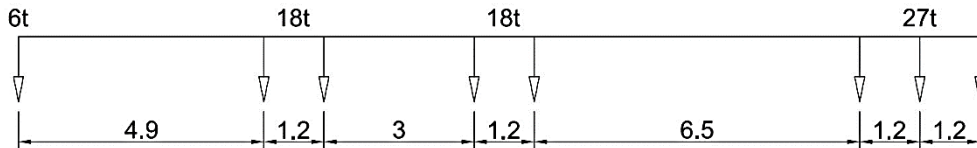
4.4.3 Group 1 Vehicles

Group 1 vehicles shall consist of the magnitude, spread and axle spacings of loads shown in Figure 4.2. The dynamic load allowance (DLA), lane modification factors (LMF) and vehicle position for the Group 1 Vehicles should be calculated as per T44 design vehicle above (consider T44 Vehicle replaced with Group 1 Vehicle while reading).

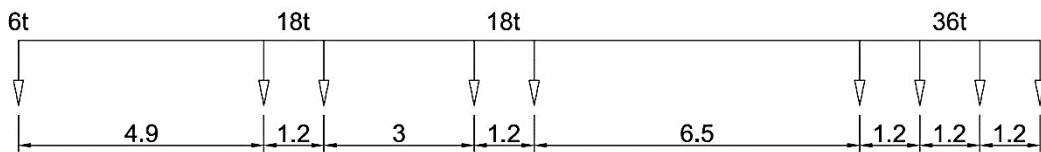
In absence of detailed analysis, the Group 1 Vehicle’s distribution factors can be assumed to have the same value as a T44 design vehicle (not applicable with modified compression field theory (MCFT) analysis).



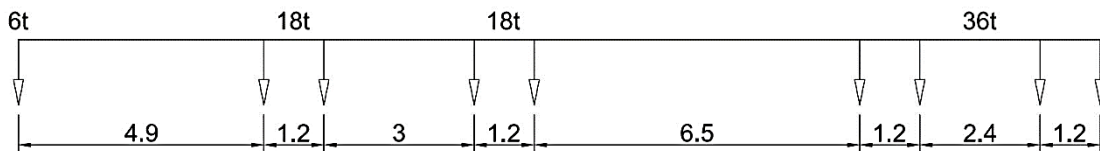
1. PRIME MOVER + 18 TONNE TANDEM
(G.C.M. = 42 TONNES)



2. PRIME MOVER + 18 TONNE DOLLY + 27 TONNE TRIAXLE
(G.C.M. = 69 TONNES)



3. PRIME MOVER + 18 TONNE DOLLY + 36 TONNE STANDARD QUAD
(G.C.M. = 78 TONNES)



4. PRIME MOVER + 18 TONNE DOLLY + 36 TONNE 484 QUAD
(G.C.M. = 78 TONNES)

NOTE
O/A WIDTH OF ALL VEHICLES 2.40m

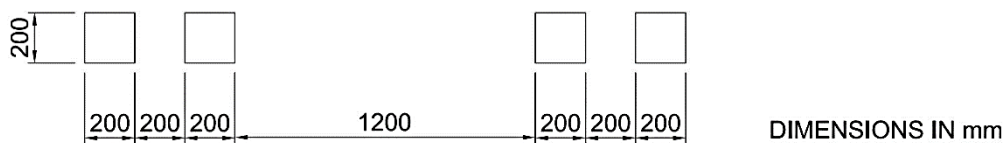


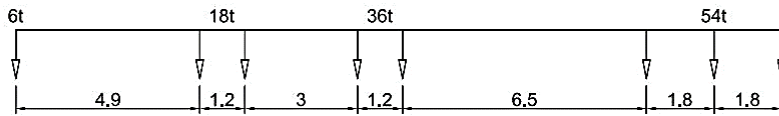
Figure 4.2 Magnitude, Spread and Axle Spacing of Loads for Group 1 Vehicles

4.4.4 HLP 320 and HLP 400

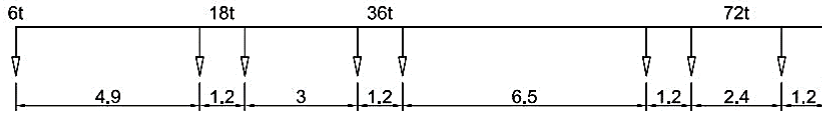
As per AS 5100 (2017) code except HLP 320 and 400 vehicles shall be positioned in accordance with Fig 4.4. The positioning of HLP vehicles shall be the worst case of ignoring or considering temporary/ mountable median/verge/footpath/kerbs. Vehicles must be positioned within full width between barriers on the bridge to ensure the bridge is designed for road traffic to allow for future changes to lane markings.

4.4.5 Group 2 Vehicles (Supervised)

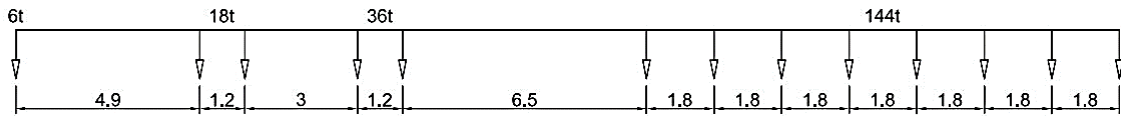
Group 2 Vehicles shall consist of the magnitude, spread and axle spacing of loads shown in Figure 4.3, with the Traffic load factor as per HLP vehicles. As the travel speed is controlled through appropriate supervision, the DLA shall be taken as 0.1. The positioning of Group 2 vehicles shall be, with reference to Figure 4.4, the worst case of ignoring or considering temporary/mountable median/verge/footpath/kerbs. Please note, after ignoring mountable median for divided carriageway bridges, the vehicle positioning should be as per Figure 4.4 (c) or (d) as appropriate instead of Figure 4.4 (a). Vehicles must be positioned within the full width between external barriers on the bridge to ensure the bridge is designed for road traffic to allow for future changes to lane markings.



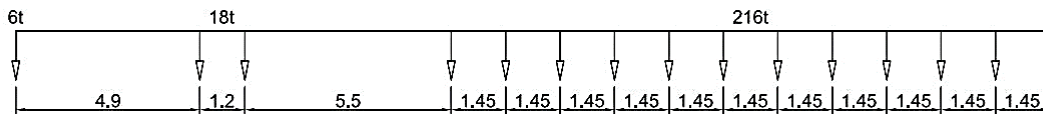
1. PRIME MOVER + 36 TONNE DOLLY + 54 TONNE TRIAXLE
(G.C.M. = 114 TONNES)



2. PRIME MOVER + 36 TONNE DOLLY + 72 TONNE SPREAD QUAD
(G.C.M. = 132 TONNES)

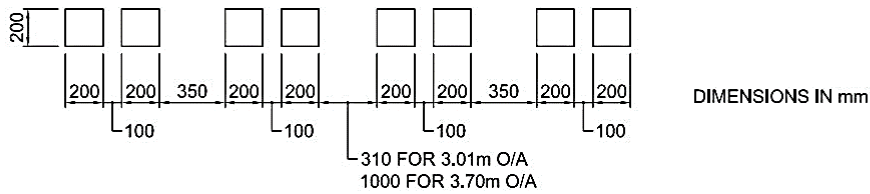


4. PRIME MOVER + 36 TONNE DOLLY + 144 TONNE 8-LINE PLATFORM
(G.C.M. = 204 TONNES)

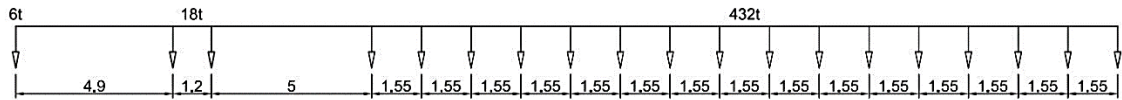


5. PRIME MOVER + 216 TONNE 12-LINE PLATFORM
(G.C.M. = 240 TONNES)

NOTE
 VEHICLES 1+2 CAN HAVE AN O/A WIDTH OF EITHER 3.01m OR 3.70m.
 VEHICLE 5 IS 3.01m O/A
 VEHICLE 4 IS 3.70m O/A

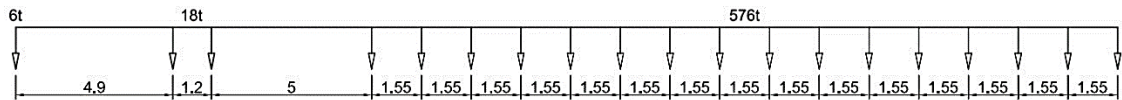
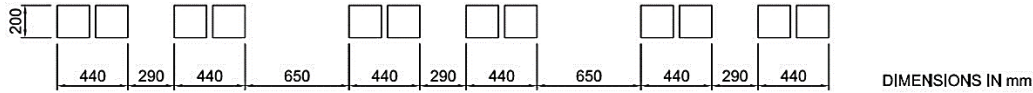


(a)



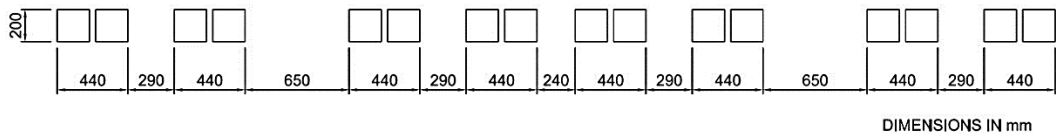
7. PRIME MOVER + 432 TONNE 16-LINE PLATFORM 3 FILE
(G.C.M. = 456 TONNES)

NOTE
VEHICLE SEVEN IS 4.81m O/A



8. PRIME MOVER + 576 TONNE 16-LINE PLATFORM 4 FILE
(G.C.M. = 600 TONNES)

NOTE
VEHICLE EIGHT IS 6.22m O/A



(b)

Figure 4.3 Magnitude, Spread and Axle Spacings of Loads for Group 2 Vehicles, (a) 8-Tyre Vehicles, (b) 12-Tyre & 16-Tyre Vehicles

For undivided bridges (and one carriageway bridges), the vehicle is to be placed up to ± 1.0 m from the bridge centreline and no other co-existing live loading is to be included on the bridge (see Figure 4.4(a)). There should be always a minimum clearance of 200 mm between the kerb and outside edge of the tyres.

For divided carriageway bridges, vehicles are to be placed up to ± 1.0 m from the carriageway centreline (in the direction of travel) with a minimum clearance of 200 mm maintained between the kerb and outside edge of the tyres (see Figure 4.4(b)). No other coincident live loading is to be included within the carriageway considered. 50% of the SM1600 loadings are to be applied in the other carriageway, positioned to give the worst load ratings. The accompanying lane factors shall be applied to these co-existing loadings in this carriageway in accordance with AS5100.2:2017, starting from 1.0 for first lane loaded with 50% of the SM1600. The vehicle positioning and dynamic load allowance of these 50% SM1600 loadings should be as per AS5100.7:2017 Cl. 11.3.

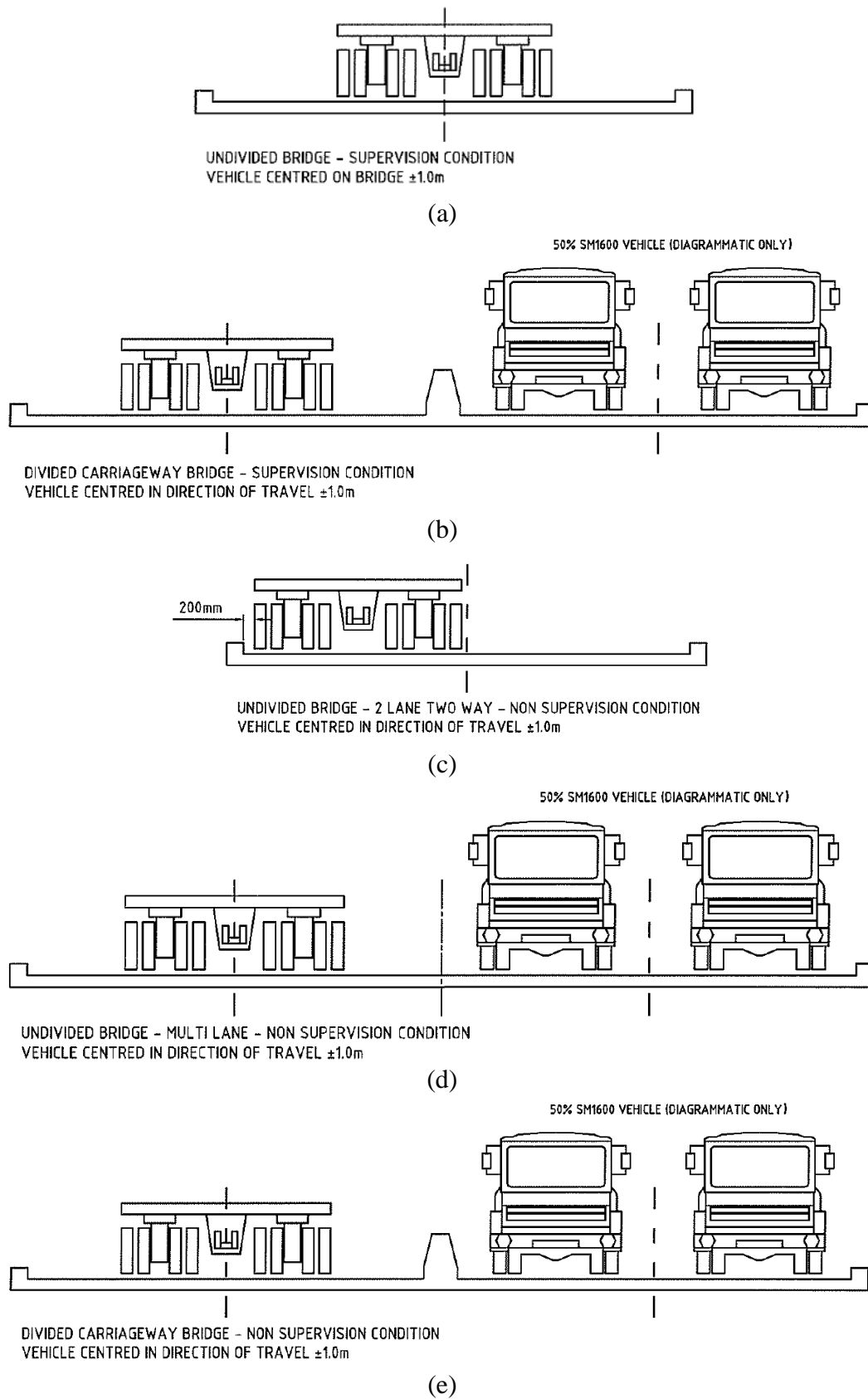


Figure 4.4 Example Vehicle Position for Load Rating of Group 2 Vehicles

4.4.6 Group 2 Vehicles (Non-Supervised)

Non-supervised load rating shall only be calculated for Group 2 Vehicle 4 and Group 2 Vehicle 5. The DLA of non-supervised Group 2 Vehicles shall be taken as 0.3. The positioning of Group 2 vehicles shall be the worst case of ignoring or considering temporary/ mountable median/verge/footpath/kerbs. Vehicles must be positioned within full width between external barriers on the bridge to ensure the bridge is rated for road traffic to allow for future changes to lane markings.

For undivided bridges, vehicles are to be placed up to ± 1.0 m from the carriageway centreline (in the direction of travel) with a minimum clearance of 200 mm between the kerb and outside edge of tyres (see Figure 4.4(c) and 4.4(d)). For bridges with a single lane in the direction of travel and kerb to kerb width less than or equal to 8.2m, no other coincident live loading is to be included. For multilane bridges or bridges with kerb-to-kerb width more than 8.2m, 50% of the SM1600 loadings are to be applied in the other carriageway, positioned to give the worst load ratings. The accompanying lane factors shall be applied to these co-existing loadings in this carriageway in accordance with AS5100.2:2017, starting from 1.0 for first lane loaded with 50% of the SM1600. The vehicle positioning and dynamic load allowance of these 50% SM1600 loadings should be as per AS5100.7:2017 Cl. 11.3.

For divided carriageway bridges, vehicles are to be placed up to ± 1.0 m from the carriageway centreline (in the direction of travel) with a minimum clearance of 200 mm maintained between the kerb and outside edge of the tyres (see Figure 4.4(e)). 50% of the SM1600 loadings are to be applied in the other carriageway, positioned to give the worst load ratings. The accompanying lane factors shall be applied to these co-existing loadings in this carriageway in accordance with AS5100.2:2017, starting from 1.0 for first lane loaded with 50% of the SM1600. The vehicle positioning and dynamic load allowance of these 50% SM1600 loadings should be as per AS5100.7:2017 Cl. 11.3.

Please note, no other co-existing Group 2/HLP vehicle should be considered in any adjacent lanes or in the same lane for Group 2 vehicles (both supervised and unsupervised) load rating.

4.5 CALCULATE PROJECTED FUTURE TRAFFIC LOAD DEMAND

Determining the nominal fatigue life of a bridge requires a fatigue assessment consisting of cumulative fatigue damage of the critical components of a bridge. For the purposes of this assessment, the cumulative fatigue damage shall be the sum of the damage due to historical loading as well as projected future traffic and the nominal fatigue life shall be considered to have been reached when the cumulative damage sums to unity. Thus, projected future traffic demand needs to be calculated for determining the remaining fatigue life of a bridge. As the projected demand will be used for calculating the number of stress cycles, this projection should be in terms of required standard vehicles as per Austroads Vehicle Classification or percentage of design vehicles specified in this section, unless otherwise specified by EBL. Please note, MRWA will provide future traffic demand data when it is not impossible to be calculated due to data access privilege.

4.6 PREPARE BRIDGE MODEL AND CALCULATE ACTION EFFECTS

Structural analysis and action effect determination shall be carried out in accordance with AS 5100 (2017) Bridge Design code and Structures Engineering Design Manual Document 3912/03. The whole of the structure shall be analysed as part of the load rating assessment. The superstructure is to be checked for both longitudinal and transverse load effects.

Moment re-distribution can be included in the rating analysis and the allowable percentage of moment calculated in accordance with AS 5100 (2017). However, for rating of existing bridges with member section capacities calculated from actual or assumed material properties, this allowable percentage is further limited as follows. The hog bending moments may be reduced, but only to the point where the hog and sag ratings balance, as there is no point in re-distributing hog moment to the point where the sag region rating becomes controlling. This limit, based on balancing the hog and sag ratings, may be less than the allowable percentage as determined by AS 5100 (2017). Further, it is important when undertaking re-distribution of moment that the rotational capacity of the section is not exceeded at a plastic hinge (i.e. rupture failure occurs). Therefore, the maximum amount of moment available for re-distribution is directly related to the ultimate section capacity and is limited to the allowable percentage as determined by AS 5100 (2017) multiplied by the member section capacity (NOT the vehicle design moment) at the specific support being assessed. The lesser value of the above two conditions is to be used in the determination of the ratings.

Simply supported bridge decks with up to 20 degrees skew may be modelled and analysed as square bridges with sufficient accuracy and continuous bridge decks with up to 10 degrees skew may be modelled and analysed as square bridges with sufficient accuracy.

For most structures, the effect of the kerb, or edge beam, may be ignored. If it is included it usually attracts a high moment, much more than it can carry, so it will only crack and re-distribute anyway. If the edge beam is stiff and heavily reinforced it may need to be considered, but an iterative approach may be required to assess the amount of load it attracts and balance this to its capacity.

Analysis of piers, columns, capbeams and bearings shall be in accordance with AS 5100 (2017). It is important to check the “as-is” condition and situation, as age, any out of plumb of the columns, or misplacement of bearings can considerably increase forces. Also, any deterioration, e.g. chloride attack at the base of columns or corrosion of steel columns etc., may need to be allowed for. Check for loads calculated as above, although if critical, it may also be necessary to include stream forces for substructure checks as per the code. This will generally be specified when required.

Foundations are only usually checked if there is some doubt about their condition, e.g. following scour from flooding. Any analysis that is deemed required shall be undertaken in accordance with AS 5100 (2017).

The introduction of the MCFT shear design in AS 5100.5:2017 has made the capacity calculation for concrete bridge section more dependent on the combined action effects of bending, shear, torsion, and axial force, as applicable. This change enhances the requirement

on finding action effects for vehicles placed in the most onerous position as per Section 4.4, as the combined action assessment makes judgement of critical positions and actions less reliable. Accordingly, calculation of ULS load ratings at multiple closely spaced locations along a concrete bridge is necessary to correctly identify the critical load rating location (for example, checking at each 100 mm increments within the critical region) prior to reporting the least controlling load rating in terms of bending and shear.

4.7 CAPACITY AND LOAD RATING

4.7.1 Loads and Load Factors

The loadings and load factors (ULS and SLS) shall be based on the AS 5100 (2017) bridge design code with several important modifications as detailed below.

Dead Load and Superimposed Dead Load

For existing structures, it is theoretically possible to measure bridge components and obtain an accurate measure of actual self-weight. However, this is rarely done, and dimensions on the drawings are commonly used. A more accurate assessment of superimposed dead loads can be made though, especially the thickness of any surfacing. This should be measured during the inspection, unless noted on design documentation, or a value (say 50mm) may be assumed based on the agreement with EBL. Unless otherwise specified, the Load Factors for Superimposed Dead Load should be as per code specified for ‘all structures’.

Load

Live Traffic loads should be considered as per AS 5100 (2017) and Section 4.4. The live load factor for the T44 design vehicle shall be used for all Group 1 Vehicles and the live load factor for HLP design vehicles shall be used for all Group 2 Vehicles. For special cases, historical design vehicles or nominated permit vehicles may be added for load rating after consultation and agreement with EBL.

Differential Temperature

Differential temperature effects should be considered as per AS 5100 (2017) code. Please note, differential temperature effects should not control the strength (ULS) rating of the structure for the T44 vehicle. That is, if the ULS ratings for the T44 vehicle fall below 100% when the effects of differential temperature are included, and where the bridge condition is good with no notable evidence of structural distress, consideration shall be given to excluding the differential temperature effects.

Differential Settlement

Differential settlement effects should be considered as per AS 5100 (2017) code. As these effects are long-term effects and will be reduced through creep, the long-term Elastic Modulus is to be used for all differential settlement effects calculation. In absence of accurate calculations, following values shall be adopted for the analysis of differential settlement effects:

Foundation Condition	Abutment Settlement	Pier Settlement	Comments
Spread Footings (non-cohesive soils)	10 mm	20 mm	Free draining granular sands
Spread Footings (cohesive soils)	Varies	Varies	Requires assessment based on geotechnical data
Spread Footings (on sound rock)	5 mm	5 mm	If borelogs indicate sound rock, or rock bit refused, reduce to 0
Piled Foundations	5 mm	5 mm	If borelogs indicate very dense soil or rock with SPT values > 120 at pile toe, reduce to 0

Note: for new bridges the settlement shall be derived using geotechnical analysis based on geotechnical investigation results.

For existing structures, a load factor of 1.0 shall be used for differential settlement effects at both the serviceability and ultimate limit states, whilst load factors should be in accordance with the AS 5100 (2017) code for new structures, ratings for the cases of including and excluding differential settlement shall be carried out.

Shrinkage and Creep

Both long-term shrinkage and creep losses must be considered (for both ULS and SLS) as per AS 5100 (2017) unless otherwise specified by EBL.

Prestress Parasitics

As per AS 5100 (2017).

Other Loads

Several loads, which may be important and have been considered for design, e.g., wind, flood, earthquake etc., are not considered for load rating assessments, except in exceptional circumstances (after the consultation and agreement with EBL). An assessment of the longitudinal braking forces shall be considered and carried out.

Fatigue

Fatigue assessment, if required by EBL/Region, needs to be carry out as per AS 5100 (2017) after the consultation and agreement with EBL.

4.7.2 Capacity and Load Rating Factor Calculation

The capacity assessment and load rating factor calculations should be as per AS 5100 (2017) Bridge Design Code and Senior Engineer Structures (SES) Circulars. Please note, prior to assessing the capacity, all possible failure modes should be identified.

Unless otherwise agreed with EBL, the extension of longitudinal reinforcement and tendons should be as per the para. 1 cl. 8.2.9.1 of AS 5100.5:2017 (incorporating amendments) for calculating the load rating (i.e., at every section, the additional longitudinal forces to be considered as caused by shear and torsion as specified in Cl. 8.2.7, Cl 8.2.8 and Fig. 8.2.9.1).

Where the transverse shear reinforcement changes (A_{sv} or s), a pragmatic approach is to ignore the additional capacity gained through general detailing as per cl. 8.3.2.3 AS 5100.5:2017 (i.e., to ignore additional shear reinforcement area that gained through extending shear reinforcement in the direction of decreasing shear). A note should be added in the load rating report and design summary sheet, clarifying whether this approach has been adopted or not for calculating the load rating.

A detailed example for capacity and load rating factor calculation of a prestressed concrete bridge is given in Appendix B. Please note, Appendix B is provided as an example and for reference only; for each bridge rating the rating engineer shall perform the checks according to the best engineering judgment/practice to assess the most critical structural conditions that determine the rating.

4.7.3 Load Rating Reporting

The load rating of an existing bridge is generally reported as a load rating memo and report. A typical load rating memo and report for a non-timber bridge are provided in Appendix C.

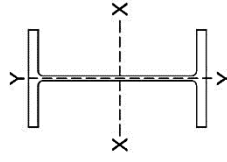
For new bridge design, the load rating results should be reported as Design Summary Sheets (DSS). Typical DSS examples for non-timber bridges are provided in Section 2 of BBDIM.

The DSS incorporating load ratings for all design vehicles must be submitted and get approved at the IFC (i.e., Issued for Construction) design review and approval stage.

APPENDIX A

Typical Steel Section Properties (Old Imperial Beams)

APPENDIX A - TYPICAL STEEL SECTION PROPERTIES (OLD IMPERIAL BEAMS)

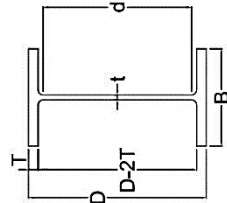


Moment of Inertia - I
Elastic Modulus - Z
Radius of Gyration - r

Universal Beams

Properties for Designing

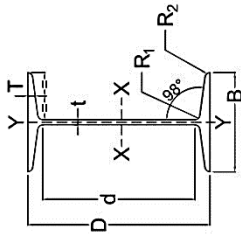
All universal beams produced in Australia have parallel flanges and the section properties listed are based on this geometry.



Designation Nominal Size	Depth of Section D	Flange Width B	Flange Thickness T	Web Thickness t	Radius Root r	Area of Section A	Ratio D/T	Depth Between Fillets d	About X-X			About Y-Y			Torsion Constant (D-2T) ³ /t	Ratio (D-2T) ³ /t	Designation Wt per Foot	Nominal Size	
									I	Z	r	I	Z	r					
30 x 10.5	196	31.22	10.836	1.461	0.900	57.49	21.4	27.00	8790	563	12.36	312	57.5	2.33	31.6	31.44	3.40	196	30 x 10.5
180	31.00	10.766	1.349	0.830	0.65	52.90	23.0	27.00	8030	518	12.32	282	52.4	2.31	24.9	34.10	3.68	180	
164	30.76	10.694	1.232	0.768	0.65	48.16	25.0	27.00	7250	471	12.27	252	47.2	2.29	19.0	37.33	4.03	164	
148	30.53	10.622	1.115	0.686	0.65	43.46	27.4	27.00	6490	425	12.22	224	42.1	2.27	14.2	41.26	4.46	148	
132	30.30	10.551	1.000	0.615	0.65	38.87	30.3	27.00	5750	380	12.18	196	37.2	2.25	10.3	46.02	4.98	132	
116	30.00	10.500	0.850	0.564	0.65	34.17	35.3	27.00	4930	329	12.01	165	31.3	2.19	6.86	50.18	5.85	116	
99	29.68	10.444	0.690	0.508	0.65	29.15	43.0	27.00	4060	274	11.80	131	25.2	2.12	4.17	55.71	7.20	99	
27 x 10	114	27.28	10.070	0.932	0.570	33.57	29.3	24.22	4090	300	11.04	159	31.6	2.18	7.82	44.59	5.10	114	27 x 10
102	27.07	10.018	0.827	0.518	0.60	30.04	32.7	24.22	3610	267	10.96	139	27.7	2.15	5.62	49.07	5.74	102	
94	26.91	9.990	0.747	0.490	0.60	27.69	36.0	24.22	3270	243	10.87	124	24.9	2.12	4.35	51.87	6.36	94	
84	26.69	9.962	0.637	0.462	0.60	24.73	41.9	24.22	2840	212	10.70	105	21.1	2.06	3.03	55.01	7.46	84	
24 x 9	94	24.29	9.061	0.872	0.516	27.65	27.9	21.55	2690	221	9.86	108	23.9	1.98	5.53	43.69	4.90	94	24 x 9
84	24.09	9.015	0.772	0.470	0.50	24.74	31.2	21.55	2370	197	9.79	94.5	21.0	1.95	3.95	47.97	5.53	84	
76	23.91	8.985	0.682	0.440	0.50	22.39	35.1	21.55	2100	176	9.69	82.6	18.4	1.92	2.89	51.24	6.27	76	
68	23.71	8.961	0.582	0.416	0.50	20.02	40.7	21.55	1820	154	9.53	70.0	15.6	1.87	2.00	54.20	7.34	68	
21 x 8.25	82	21.44	8.342	0.840	0.502	24.16	25.5	18.76	1830	171	8.71	81.5	19.5	1.84	4.57	39.36	4.67	82	21 x 8.25
73	21.24	8.295	0.740	0.455	0.50	21.48	28.7	18.76	1600	151	8.64	70.6	17.0	1.81	3.22	43.43	5.30	73	
68	21.13	8.270	0.685	0.430	0.50	20.04	30.8	18.76	1480	140	8.60	64.7	15.7	1.80	2.61	45.95	5.72	68	
62	20.99	8.240	0.615	0.400	0.50	18.35	34.1	18.76	1330	127	8.54	57.5	13.9	1.77	1.97	49.40	6.37	62	
55	20.80	8.216	0.520	0.376	0.50	16.19	40.0	18.76	1140	110	8.40	48.2	11.7	1.72	1.34	52.55	7.54	55	
18 x 7.5	66	18.40	7.592	0.770	0.450	19.42	23.9	16.06	1100	119	7.52	56.3	14.8	1.70	3.07	37.47	4.64	66	18 x 7.5
60	18.25	7.558	0.695	0.416	0.40	17.66	26.3	16.06	986	108	7.47	50.1	13.3	1.68	2.31	40.43	5.14	60	
55	18.12	7.532	0.630	0.390	0.40	16.20	28.8	16.06	891	98.4	7.42	45.0	11.9	1.67	1.77	43.23	5.67	55	
50	18.00	7.500	0.570	0.358	0.40	14.72	31.6	16.06	802	89.1	7.38	40.2	10.7	1.65	1.34	47.10	6.27	50	
45	17.86	7.476	0.500	0.334	0.40	13.24	35.7	16.06	706	79.1	7.30	34.9	9.33	1.62	0.962	50.48	7.14	45	
16 x 7	50	16.25	7.073	0.628	0.380	14.72	25.9	14.19	657	80.8	6.68	37.1	10.5	1.59	1.61	39.46	5.33	50	16 x 7
45	16.12	7.039	0.563	0.346	0.40	13.24	28.6	14.19	585	72.5	6.64	32.8	9.32	1.57	1.18	43.34	5.94	45	
40	16.00	7.000	0.503	0.307	0.40	11.19	31.8	14.19	517	64.6	6.62	28.8	8.23	1.56	0.851	48.84	6.65	40	
36	15.85	6.982	0.428	0.299	0.40	10.01	37.0	14.19	448	56.5	6.50	24.4	6.99	1.52	0.594	50.15	7.82	36	

ROLLED STEEL JOISTS

DIMENSIONS AND PROPERTIES



Reference Number	Size D x B Inches	Weight per foot lbs	PLASTIC MODULI OF SECTION		STANDARD THICKNESS INCHES		RADI INCHES		Straight Portion of Web d Inches	Sectional Area Inches ²	MOMENT OF INERTIA INCHES ⁴		RADI OF GYRATION INCHES		ELASTIC MODULI OF SECTION		D/T	Size D x B x Wt. per Foot
			Axis X-X	Axis Y-Y	Web t	Flange T	Root R1	Toe R2			Axis X-X	Axis Y-Y	Axis X-X	Axis Y-Y	Axis X-X	Axis Y-Y		
ASB 126	24 x 7.5*	100	254.6	29.01	0.64†	1.011	0.73	0.36	20.25	29.44	2605.04	64.30	9.41	1.48	217.09	17.00	23.7	24 x 7.5 x 100
ASB 125	24 x 7.5	95	245.6	28.11	0.57	1.011	0.73	0.36	20.25	27.94	2533.04	62.54	9.52	1.50	211.09	16.68	23.7	24 x 7.5 x 95
ASB 124	22 x 7	75	177.2	19.96	0.50	0.834	0.69	0.34	18.68	22.06	1676.80	41.07	8.72	1.36	152.44	11.73	26.4	22 x 7 x 75
ASB 123	20 x 6.5	65	141.8	16.84	0.45	0.820	0.65	0.32	16.80	19.12	1226.17	32.56	8.01	1.31	122.62	10.02	24.4	20 x 6.5 x 65
ASB 121	18 x 6	55	108.1	13.24	0.42	0.757	0.61	0.30	15.03	16.18	841.76	23.63	7.21	1.21	93.53	7.88	23.8	18 x 6 x 55
ASB 120	16 x 6	50	88.79	12.44	0.40	0.726	0.61	0.30	13.09	14.71	618.09	22.47	6.48	1.24	77.26	7.49	22.0	16 x 6 x 50
ASB 119	15 x 6	45	75.20	11.15	0.38	0.655	0.61	0.30	12.25	13.24	491.91	19.87	6.10	1.23	65.59	6.62	22.9	15 x 6 x 45
ASB 118	14 x 5.5	40	61.95	9.02	0.37	0.627	0.57	0.28	11.39	11.77	377.06	14.79	5.66	1.12	53.87	5.38	22.3	14 x 5.5 x 40
ASB 117	13 x 5	35	50.28	7.26	0.35	0.604	0.53	0.26	10.53	10.30	283.51	10.81	5.25	1.03	43.52	4.33	21.5	13 x 5 x 35
ASB 116	12 x 8	65	92.46	26.63	0.43	0.904	0.77	0.38	8.30	19.12	487.77	65.18	5.05	1.85	81.29	16.30	13.3	12 x 8 x 65
ASB 115	12 x 5	30	39.68	6.01	0.33	0.507	0.53	0.26	9.74	8.63	206.93	8.77	4.84	1.00	34.49	3.51	23.7	12 x 5 x 30
ASB 114	10 x 8	70	80.46	28.97	0.60	0.970	0.70	0.35	6.33	20.58	345.04	71.61	4.09	1.87	69.01	17.90	10.3	10 x 8 x 70
ASB 113	10 x 6	55	65.65	22.59	0.40	0.783	0.77	0.38	6.60	16.18	288.69	54.74	4.22	1.84	57.74	13.69	12.8	10 x 8 x 55
ASB 112	10 x 4.5	40	46.74	11.89	0.36	0.709	0.61	0.30	7.09	11.77	204.80	21.76	4.17	1.36	40.94	7.39	14.1	10 x 6 x 40
ASB 111	9 x 7	25	28.07	4.84	0.30	0.505	0.49	0.24	7.84	7.35	122.34	6.49	4.08	0.94	24.47	2.88	19.8	10 x 4.5 x 25
ASB 110	9 x 4	21	20.85	3.51	0.30	0.457	0.45	0.22	5.61	14.71	208.13	40.17	3.76	1.65	46.25	11.48	10.9	9 x 7 x 50
ASB 109	8 x 6	35	32.94	10.71	0.35	0.648	0.61	0.30	7.03	6.18	81.13	4.15	3.62	0.82	18.03	2.07	19.7	9 x 4 x 21
ASB 108	8 x 4	18	16.02	2.99	0.28	0.398	0.45	0.22	5.36	10.30	115.06	19.54	3.34	1.38	28.76	6.51	12.3	8 x 6 x 35
ASB 107	7 x 3.5	15	11.79	2.30	0.25	0.398	0.41	0.20	6.15	5.30	55.63	3.51	3.24	0.81	13.91	1.75	20.1	8 x 4 x 18
ASB 106	6 x 5	25	17.50	6.48	0.33	0.561	0.53	0.26	5.25	4.42	35.90	2.41	2.85	0.74	10.26	1.38	17.6	7 x 3.5 x 15
ASB 105	6 x 3	12	8.08	1.63	0.23	0.377	0.37	0.18	3.71	7.35	45.16	9.88	2.48	1.16	15.05	3.95	10.7	6 x 5 x 25
ASB 104	5 x 2.5	9	5.06	1.03	0.20	0.347	0.33	0.16	4.40	3.53	20.99	1.46	2.44	0.64	7.00	0.97	15.9	6 x 3 x 12
ASB 103	4 x 3	10	4.54	1.47	0.24	0.347	0.37	0.18	3.60	2.65	10.91	0.79	2.03	0.55	4.36	0.63	14.4	5 x 2.5 x 9
ASB 102	4 x 1.75	5	2.15	0.37	0.17	0.239	0.27	0.13	2.96	2.94	7.79	1.33	1.63	0.67	3.89	0.88	11.5	4 x 3 x 10
									2.86	1.47	3.66	0.19	1.58	0.36	1.83	0.21	16.7	4 x 1.75 x 5

* Nominal size - Actual width is 7% inches.
 † Nominal size - Actual thickness is 0.6325 inches.

APPENDIX B

Example Load Rating of a Prestressed Concrete Tee-Roof Beam

APPENDIX B - EXAMPLE LOAD RATING CALCULATION OF A PRESTRESSED CONCRETE TEE-ROFF BEAM

The following example illustrates the load rating of a prestressed concrete Tee-Roof beam for SM1600 design vehicle based on the AS 5100 (2017) code. This step by step process will help to understand the load rating process with known design vehicle action effects. The introduction of the modified compression field theory (MCFT) has made the bending and shear capacity as well as load rating calculation of a beam dependent on the applied loading action effects, i.e., dependent on bending, shear and torsional action effects. The load rating factor k , therefore, can be determined when scaling the live load action effects with k results in the utilisation of the full capacity for any particular failure mechanism. The bending, shear and torsional action effects at full capacity utilisation will be,

$$M^* = M_{PE} + M_{CE} + k \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k \times T_{LL}^*$$

where,

M_{PE} = Factored ultimate moment due to all permanent effects (PE)

M_{CE} = Factored ultimate moment due to co-existing live load

M_{LL}^* = Factored ultimate moment due to vehicle live load effects (including γ and DLA)

V_{PE} = Factored ultimate shear due to all permanent effects (PE)

V_{CE} = Factored ultimate shear due to co-existing live load

V_{LL}^* = Factored ultimate shear due to vehicle live load effects (including γ and DLA)

T_{PE} = Factored ultimate torsion due to all permanent effects (PE)

T_{CE} = Factored ultimate torsion due to co-existing live load

T_{LL}^* = Factored ultimate torsion due to vehicle live load effects (including γ and DLA)

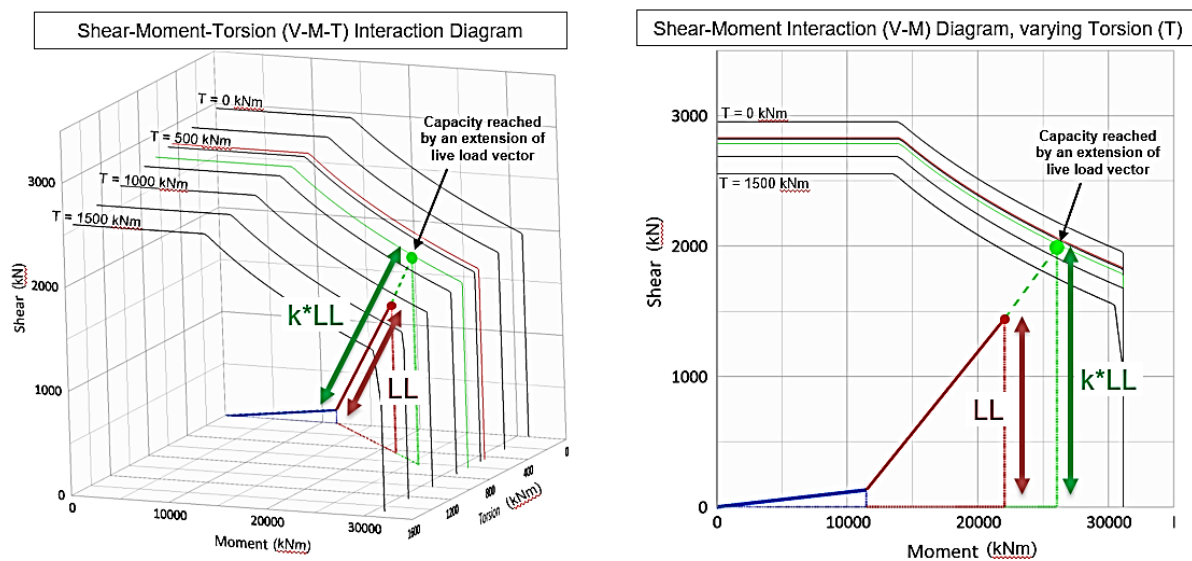


Figure B.1 Three-Dimensional Euclidian Capacity Surface Demonstrating Shear-Moment-Torsion (V-M-T) Interaction

Figure B.1 illustrates this interaction of bending, shear and torsion and the load rating factor k can be interpreted as the scaling factor by which critical live load actions can be increased (or decreased), before the cross sectional capacity is reached.

Performing a beam/grillage analysis of a bridge can generate a huge number of combinations of M_{LL}^* , V_{LL}^* and T_{LL}^* at a critical section due to moving vehicles position. Out of all these combinations, only three combination needs to be considered. They are,

- (i) M_{LL}^* max with corresponding V_{LL}^* and T_{LL}^*
- (ii) V_{LL}^* max with corresponding M_{LL}^* and T_{LL}^*
- (iii) T_{LL}^* max with corresponding M_{LL}^* and V_{LL}^*

The matrix below summarises the Ultimate Limit State (ULS) bending, shear and torsion cases at each cross-section that are required to be load rated as well as capacity calculated in the ultimate limit state load rating.

Longitudinal Bending Scenarios	M_{LL}^* Max (Corr. V_{LL}^* & T_{LL}^*)	V_{LL}^* Max (Corr. M_{LL}^* & T_{LL}^*)	T_{LL}^* Max (Corr. M_{LL}^* & V_{LL}^*)
M1	Y	N/A	N/A
M2	Y	N/A	N/A
M3	Y	N/A	N/A
Combined Shear and Torsion Scenarios	M_{LL}^* Max (Corr. V_{LL}^* & T_{LL}^*)	V_{LL}^* Max (Corr. M_{LL}^* & T_{LL}^*)	T_{LL}^* Max (Corr. M_{LL}^* & V_{LL}^*)
V1	Y	Y	Y
V2	Y	Y	Y
V3	N/A	Y	Y
V4	N/A	Y	Y
V5	Y	Y	Y

Though, the load rating and capacity calculations should be performed at each cross-section for 100mm increments of the beam or a reasonable small increment (unless not required at compression fan regions), the calculations showed in this example has been performed for only one cross section for each scenario for demonstration purpose. Refer Figure B.2 for the cross section at mid-span of Span 1.

Also, no temperature load or support settlement is considered in this example. Furthermore, it is assumed for this example that all other failure modes such as transverse failure, interface shear, anchorage zone etc. are checked and load ratings are adequately above the longitudinal bending and shear rating factors.

B.1 DETERMINE SECTION AND MATERIAL PROPERTIES

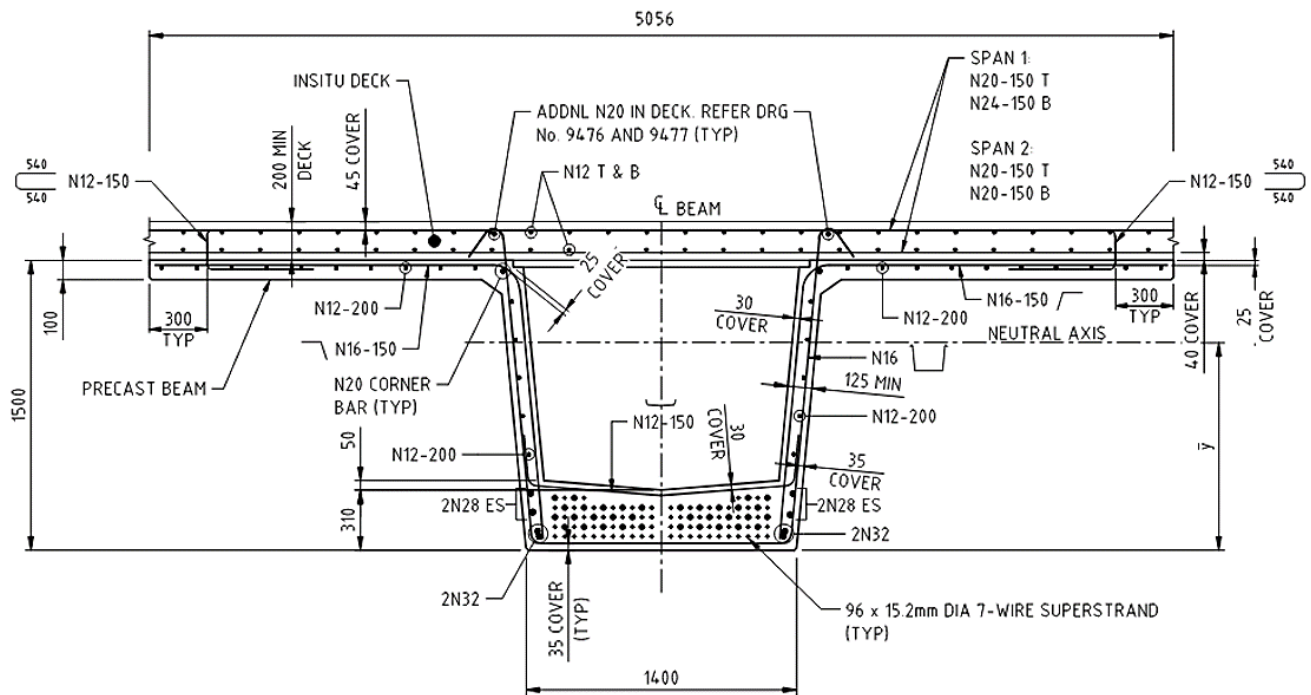


Figure B.2 Beam Cross Section at Mid-Span of Span 1

Material Properties

Concrete strength (Deck), $f'_{c_{deck}}$	40 MPa
Concrete strength (Beam), $f'_{c_{beam}}$	50 MPa
Modulus of elasticity (Deck), $E_{c_{Deck}}$	32,800 MPa (AS 5100.5:2017 Table 3.1.2)
Modulus of elasticity (Beam), $E_{c_{Beam}}$	34,800 MPa (AS 5100.5:2017 Table 3.1.2)
Yield strength (D500N), f_{sy}	500 MPa (AS 5100.5:2017 Table 3.2.1)
Modulus of elasticity (D500N), E_s	200×10^3 MPa (AS 5100.5: 2017 Clause 3.2.2)
Breaking strength (Strand), f_{pb}	1830 MPa (AS 5100.5:2017 Table 3.2.1)

Reinforcement Details

The number of layers and area of the D500N reinforcement within the composite cross section are presented below in Table B.1.

Table B.1 D500N Reinforcement within the Composite Cross Section

Layer	A_{st} (mm ²)	Depth from top of section (mm)
1	2857	71
2	628	75
3	2857	130
4	2260	247
5	628	260
6	226	445
7	226	646
8	226	847
9	226	1038
10	226	1242
11	1232	1400
12	1232	1495
13	1608	1593
14	1608	1625

The number of layers and area of the prestressing strand within the typical composite cross section are presented below in Table B.2.

Table B.2 Prestressing Strand within the Typical Composite Cross Section

Layer	A_{st} (mm ²)	Depth from top of section (mm)
1	1144	1430
2	3146	1480
3	3146	1530
4	3146	1580
5	3146	1630

B.2 ΦM_u CALCULATION

Calculate Transformed Flange Width

The depth to the neutral axis is unknown however, it is assumed to be located in the top flange of the beam i.e. below the deck level. Following transformed flange widths were used to calculate the position of the neutral axis at ULS and SLS loading (note: this approximate transformation is only for identifying the neutral axis when it is below deck level and not for any other calculations).

As the deck of the composite section has a different 28-day compressive strength to that of the precast beam, in the ULS analysis, the width of the top flange is transformed as follows,

$$\text{Transformed Width}_{ULS} = \frac{f'_{c_{deck}}}{f'_{c_{beam}}} \times \text{Top flange width} = \frac{40}{50} \times 5056 = 4045 \text{ mm}$$

This is different to the SLS analysis where the width of the top flange is transformed based on the modular ratio of the elastic moduli of the deck concrete 28-day strength against that of the precast beam,

$$\text{Transformed Width}_{SLS} = \frac{E_{c_Deck}}{E_{c_Beam}} \times \text{Top flange width} = \frac{32,800}{34,800} \times 5056 = 4765 \text{ mm}$$

Calculate $\Phi_b M_u$

The unfactored moment capacity M_u (38115 kNm) was calculated based on the maximum stress reached in tendons at ultimate strength using Eq. 8.1.7(1) of AS 5100.5:2017 (alternatively stress-strain curve can be used in accordance with BBDIM Section 2). Solving for the neutral axis depth, it was determined that the neutral axis is located 203.6 mm from the top of the composite section which places it in the beam top flange as assumed. From this we determine that $\gamma d_n = 142.5$ mm from the top of the composite section ($\gamma = 0.7$ and $\alpha_2 = 0.85$ are assumed conservatively considering neutral axis is below the deck level) and,

$$k_{uo} = \frac{d_n}{d_o} = \frac{203.6}{1630} = 0.125$$

Which gives a Φ_b for bending of 0.8 calculated in accordance with AS 5100.5:2017 Table 2.3.2 for item (b) Bending without axial tension or compression. This gives a factored ultimate beam bending capacity at mid-span of span 2,

$$\Phi_b M_u = 30492 \text{ kNm}$$

Please note, the $\Phi_b M_u$ for the example beam varies along the length due to the varied flange width. The above calculation is an example for determining $\Phi_b M_u$ at 16.96 m from the centreline of the Abutment 1 Bearing (approximately at the mid-span of span 1).

B.3 CALCULATE EFFECTIVE SHEAR DEPTH d_v

AS 5100.5:2017 Cl. 8.2.1.9 defines the effective shear depth (d_v) as “the distance between the resultants of the tensile and compressive forces due to flexure in Clause 8.1.2 but not less than the greater of $0.72D$ or $0.9d$, where d is taken as the distance from the extreme compression fibre to the centroid of the longitudinal tension reinforcement in the half-depth of the section containing the flexural tension zone”.

From the calculations above the distance between the resultants of the tensile and compressive forces due to flexure in Clause 8.1.2 is determined to be 1439 mm.

Similarly, the distance d from the extreme compression fibre to the centroid of the longitudinal

tension reinforcement in the half-depth of the section containing the flexural tension zone is determined to be 1543 mm which gives,

$$0.9d = 0.9 \times 1543 = 1387 \text{ mm}$$

$$0.72D = 0.72 \times 1700 = 1224 \text{ mm}$$

The lower limit on d_v is then $Maximum(1387, 1224) = 1387 \text{ mm}$

Thus, d_v is calculated at 16.96 m from the centreline of the Abutment 1 Bearing (approximately at the mid-span of span 1) to be $Maximum(1387, 1439) = 1439 \text{ mm}$

B.4 0.25 ΦT_{cr} CALCULATION

Refer AS 5100.5:2017 equation 8.2.1.2(2) reproduced below:

$$T_{cr} = 0.33\sqrt{f'_c} \frac{A_{cp}^2}{u_c} \sqrt{\left(1 + \frac{\sigma_{cp}}{0.33\sqrt{f'_c}}\right)}$$

A_{cp} is diagrammatically (ignoring overhanging flanges) shown in Figure B.3 below:

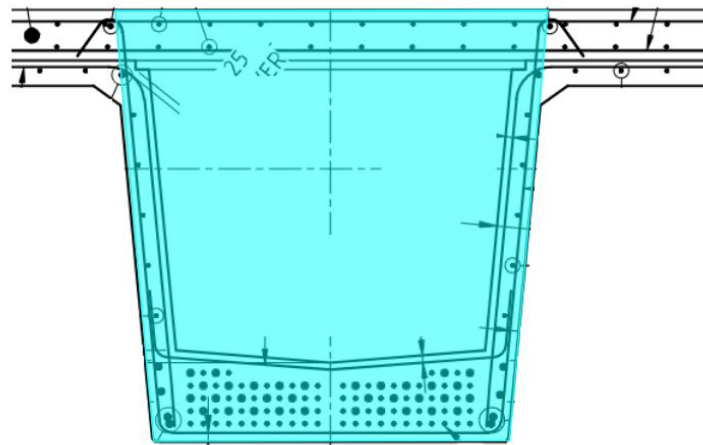


Figure B.3 Diagrammatic Representation of Torsional Parameter A_{cp}

And is determined from the following calculation:

$$\begin{aligned} A_{cp} &= b_f D + 2 \times 0.5 \times D \times D \times \tan(\theta_w) \\ &= 1.4 \times 1.7 + 2 \times 0.5 \times 1.7 \times 1.7 \times \tan(5.45^\circ) \\ &= 2.38 + 0.276 = 2.656 \text{ m}^2 \end{aligned}$$

Where:

b_f = Bottom flange width

D = Overall depth of the composite section

θ_w = web angle to the vertical

u_c is simply the perimeter of this shape and is calculated by the following equation:

$$\begin{aligned}
 u_c &= 2b_f + 2 \times D \times \tan(\theta_w) + 2 \times \sqrt{D^2 + (D \times \tan(\theta_w))^2} \\
 &= 2 \times 1.4 + 2 \times 1.7 \times \tan(5.45) + 2 \times \sqrt{1.7^2 + (1.7 \times \tan(5.45^\circ))^2} \\
 &= 2.8 + 0.324 + 2 \times 1.708 = 6.54 \text{ m}
 \end{aligned}$$

Note that AS 5100.5:2017 equation 8.2.1.2(3) places a limit on $\frac{A_{cp}^2}{u_c}$ for cellular structures such as this configuration of beam and slab such that

$$\frac{A_{cp}^2}{u_c} \leq 2A_o b_v$$

Where:

A_o = area enclosed by shear flow path, including any areas of holes therein

b_v = effective width of the critical web, 125 mm at this location.

A_o is defined by the mid-depth of the bottom flange, webs and the deck and is shown diagrammatically in Figure B.4 below:

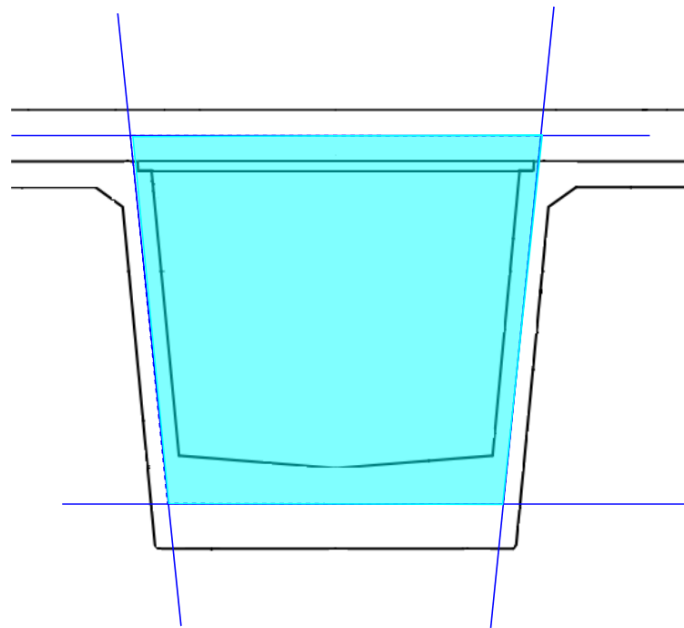


Figure B.4 Diagrammatic Representation of Torsional Parameter A_o

A_o is determined to be 2.084 m^2 based on a bottom flange thickness of 310 mm, a nominal deck thickness of 200 mm at this location and web thicknesses of 125 mm respectively. Substituting these values into equation 8.2.1.2(3) we have,

$$\frac{A_{cp}^2}{u_c} \leq 2A_o b_v = \frac{2.656^2}{6.54} \leq 2 \times 2.084 \times 0.125 = 1.07 \leq 0.521 = 0.521$$

σ_{cp} is defined as the average intensity of effective prestress in concrete at the centroid, or at the junction of the web and flange when the centroid lies inside the flange.

In this instance, the centroid of the concrete cross section is near the mid-depth of the composite section and as such σ_{cp} is taken at this location.

$$\sigma_{cp} = 6.1567 \text{ MPa}$$

Substituting these values into the equation for T_{cr} we have,

$$T_{cr} = 0.33\sqrt{50} \times 0.521 \times \sqrt{\left(1 + \frac{6.1567}{0.33\sqrt{50}}\right)} = 2319 \text{ kNm}$$

$$\text{And } \Phi_t T_{cr} = 0.7 \times 2391 = 1624 \text{ kNm}$$

And the limit in AS 5100.5:2017 equation 8.2.1.2(1) for when torsional effects are to be considered at 16.96 m from the centreline of the Abutment 1 Bearing (approximately at the mid-span of span 1),

$$0.25\Phi_t T_{cr} = 0.25 \times 1674 = 405.9 \text{ kN}$$

B.5 CALCULATE LOAD RATING FACTOR k_{M1} FOR SCENARIO M1

Scenario M1

The load rating factor k_{M1} for scenario M1 is the factor of live loads that results in full utilisation of the bending capacity of the cross section under consideration. The objective function is,

$$\Phi_b M_u = M_{PE} + M_{CE} + k_{M1} \times M_{LL}^*$$

This equation needs to be solved for k_{M1} .

Location

16.96 m from the centreline of the abutment 1 bearing (approximately at the mid-span of span 1) with beam flange width 5056 mm.

Section Parameters

$\alpha_2 = 0.85$	$z = 1439 \text{ mm}$	$A_{sv} = 402 \text{ mm}^2$	$A_{cp} = 2.656 \times 10^6 \text{ mm}^2$
$\gamma = 0.70$	$d_v = 1439 \text{ mm}$	$s = 150 \text{ mm}$	$u_c = 6540 \text{ mm}$
$\Phi_b = 0.80$	$\bar{y} = 541 \text{ mm}$	$\alpha_v = 90^\circ$	$A_o = 2.084 \times 10^6 \text{ mm}^2$
$\Phi_s = 0.70$	$b_v = 250 \text{ mm}$	$A_{sc} = 6341 \text{ mm}^2$	$A_{oh} = 2.363 \times 10^6 \text{ mm}^2$
$\Phi_t = 0.70$	$t_w = 125 \text{ mm}$	$A_{st.D/2} = 6132 \text{ mm}^2$	$u_h = 6169 \text{ mm}$
$d = 1543 \text{ mm}$	$\sigma_{cp} = 6.157 \text{ MPa}$	$A_{pt.D/2} = 13728 \text{ mm}^2$	$A_{ct} = 0.609 \times 10^6 \text{ mm}^2$
$d_n = 203.6 \text{ mm}$	$d_g = 20 \text{ mm}$	$\Sigma A_{sc} f_s = -1974 \times 10^3 \text{ N}$	$\Sigma A_{st} f_s + \Sigma A_{pt} \sigma_{pt} = 26480 \times 10^3 \text{ N}$
$k_{uo} = 0.125$	$P_v = 0.0 \text{ N}$	$f_{po} = 1830 \times 0.7 = 1281 \text{ MPa}$	$\Phi M_u = 30492 \times 10^6 \text{ Nmm}$
$D = 1700 \text{ mm}$	$\gamma_p = 0.90$		$0.25\Phi T_{CR} = 405.9 \times 10^6 \text{ Nmm}$

Action Effects

$M_{PE} = 11659 \times 10^6 Nmm$	$V_{PE} = 92 \times 10^3 N$	$T_{PE} = 239 \times 10^6 Nmm$
$M_{CE} = 0 Nmm$	$V_{CE} = 0 N$	$T_{CE} = 0 Nmm$
$M_{LL}^* = 18320 \times 10^6 Nmm$	$V_{LL}^* = 9 \times 10^3 N$	$T_{LL}^* = 319 \times 10^6 Nmm$

Solve for k_{M1}

Solving for k_{M1} we determine its value to be 1.03 or 103%.

B.6 CALCULATE LOAD RATING FACTOR k_{M2} FOR SCENARIO M2

Scenario M2

The load rating factor k_{M2} for scenario M2 is the factor of live loads that results in the utilisation of the total longitudinal reinforcement on the flexural tensile side. The objective function is,

for shear only,

$$\left(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt} \right) = \frac{(M_{PE} + M_{CE} + k_{M2} \times M_{LL}^*)}{\Phi_b z} + \frac{0.5 \times N^*}{\Phi_n} + \left[\left(\frac{(V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*) - \gamma_p P_v}{\Phi_s} \right) - 0.5 V_{us} \right] \cot(\theta_v)$$

for combined shear and torsion,

$$\left(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt} \right) = \frac{(M_{PE} + M_{CE} + k_{M2} \times M_{LL}^*)}{\Phi_b z} + \frac{0.5 \times N^*}{\Phi_n} + \sqrt{\left[\left(\frac{(V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*) - \gamma_p P_v}{\Phi_s} \right) - 0.5 V_{us} \right]^2 + \left(\frac{0.45 * (T_{PE} + T_{CE} + k_{M2} \times T_{LL}^*) \times u_h}{2A_o \Phi_t} \right)^2} \cot(\theta_v)$$

where,

$$V_{us} = \frac{A_{sv} f_{sy} d_v}{s} (\sin(\alpha_v) \cot(\theta_v) + \cos(\alpha_v))$$

$$\left[\left(\frac{(V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*) - \gamma_p P_v}{\Phi_s} \right) - 0.5 V_{us} \right] \geq 0$$

and,

z is the internal moment lever arm between the centroids of the flexural compression force and the flexural tension force acting on the section, similar to d_v but without the limits 0.72D or 0.9d. Please note, the approach to use of z as the internal moment lever arm is an approximate

method. This approximation should NOT be used while designing and subsequently for the load rating of the Design Vehicles as the quantity of additional longitudinal reinforcements and tendons are known. An iterative method should be used for more accurate rating calculation.

In this equation, f_s should not exceed f_{sy} and σ_{pt} needs to be determined from the tendon stress-strain relationship based on bending strain compatibility.

This equation needs to be solved for k_{M2} . As the value of θ_v in the objective function depends on the action effects, it is also dependent on the value k_{M2} . The value of k_{M2} , therefore, needs to be determined using appropriate iterative solvers (for example using *goalseek* function). Furthermore, according to AS 5100.5:2017 Cl. 8.2.4, longitudinal strain ε_x needs to be calculated based on one of the four alternative equations determined by their sign and magnitude of the torsional action effect T^* . But, the value of T^* is also dependent on k_{M2} . Thus, four separate k_{M2} needs to be calculated through iterative processes for following four alternative cases. The final value of k_{M2} , then, needs to be selected based on the sign of ε_x and magnitude of T^* compared against $0.25\Phi T_{CR}$. Please note, as per AS 5100.5:2017 Cl. 8.2.4.3 and 8.2.4.4, for sections closer than d_o to the face of the support, the value of ε_x calculated at d_o from the face of the support may be used in evaluating ε_x and k_v . Furthermore, as per AS 5100.5:2017 Cl. 8.2.9, the regions adjacent to maximum moment not subject to significant torsion where the support or load introduces direct compression and a fan-shaped pattern of compressive stresses radiating from the point load or the support, the M2 (and V3) rating may be omitted, provided that extension of longitudinal reinforcement and tendons are compliant with this clause.

Case 1 – shear only and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$\left(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt} \right) = \frac{M^*}{\Phi_b Z} + \frac{0.5 \times N^*}{\Phi_n} + \left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s} \right) - 0.5 V_{us} \right] \cot(\theta_v)$$

Case 2 – shear only and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{M3} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$\left(\sum_{i=1}^n A_{st}f_s + \sum_{i=1}^n A_{pt}\sigma_{pt} \right) = \frac{M^*}{\Phi_{bz}} + \frac{0.5 \times N^*}{\Phi_n} + \left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s} \right) - 0.5V_{us} \right] \cot(\theta_v)$$

Case 3 – combined shear & torsion and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{M3} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o} \right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$\left(\sum_{i=1}^n A_{st}f_s + \sum_{i=1}^n A_{pt}\sigma_{pt} \right) = \frac{M^*}{\Phi_{bz}} + \frac{0.5N^*}{\Phi_n} + \sqrt{\left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s} \right) - 0.5V_{us} \right]^2 + \left(\frac{0.45 \times T^* \times u_h}{2A_o \Phi_t} \right)^2} \cot(\theta_v)$$

Case 4 – combined shear & torsion and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o} \right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$\left(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt} \right) = \frac{M^*}{\Phi_b z} + \frac{0.5N^*}{\Phi_n} + \sqrt{\left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s} \right) - 0.5V_{us} \right]^2 + \left(\frac{0.45 \times T^* \times u_h}{2A_o \Phi_t} \right)^2} \cot(\theta_v)$$

Location

16.96 m from the centreline of the abutment 1 bearing (approximately at the mid-span of span 1) with beam flange width 5056 mm.

Section Parameters

$\alpha_2 = 0.85$	$z = 1439 \text{ mm}$	$A_{sv} = 402 \text{ mm}^2$	$A_{cp} = 2.656 \times 10^6 \text{ mm}^2$
$\gamma = 0.70$	$d_v = 1439 \text{ mm}$	$s = 150 \text{ mm}$	$u_c = 6540 \text{ mm}$
$\Phi_b = 0.80$	$\bar{y} = 541 \text{ mm}$	$\alpha_v = 90^\circ$	$A_o = 2.084 \times 10^6 \text{ mm}^2$
$\Phi_s = 0.70$	$b_v = 250 \text{ mm}$	$A_{sc} = 6341 \text{ mm}^2$	$A_{oh} = 2.363 \times 10^6 \text{ mm}^2$
$\Phi_t = 0.70$	$t_w = 125 \text{ mm}$	$A_{st.D/2} = 6132 \text{ mm}^2$	$u_h = 6169 \text{ mm}$
$d = 1543 \text{ mm}$	$\sigma_{cp} = 6.157 \text{ MPa}$	$A_{pt.D/2} = 13728 \text{ mm}^2$	$A_{ct} = 0.609 \times 10^6 \text{ mm}^2$
$d_n = 203.6 \text{ mm}$	$d_g = 20 \text{ mm}$	$\Sigma A_{sc} f_s = -1974 \times 10^3 \text{ N}$	$\Sigma A_{st} f_s + \Sigma A_{pt} \sigma_{pt} = 26480 \times 10^3 \text{ N}$
$k_{uo} = 0.125$	$P_v = 0.0 \text{ N}$	$f_{po} = 1830 \times 0.7$	$\Phi M_u = 30492 \times 10^6 \text{ Nmm}$
$D = 1700 \text{ mm}$	$\gamma_p = 0.90$	$= 1281 \text{ MPa}$	$0.25 \Phi T_{CR} = 405.9 \times 10^6 \text{ Nmm}$

Action Effects

$M_{PE} = 11659 \times 10^6 \text{ Nmm}$	$V_{PE} = 92 \times 10^3 \text{ N}$	$T_{PE} = 239 \times 10^6 \text{ Nmm}$
$M_{CE} = 0 \text{ Nmm}$	$V_{CE} = 0 \text{ N}$	$T_{CE} = 0 \text{ Nmm}$
$M_{LL}^* = 18320 \times 10^6 \text{ Nmm}$	$V_{LL}^* = 9 \times 10^3 \text{ N}$	$T_{LL}^* = 319 \times 10^6 \text{ Nmm}$

Solve for k_{M2}

	Case 1	Case 2	Case 3	Case 4
k_{M2} solved using iteration	1.03	1.03	0.98	0.97
ϵ_x	0.474×10^{-3}	0.074×10^{-3}	0.471×10^{-3}	0.072×10^{-3}
ϵ_x sign check	Selected	Ignored	Selected	Ignored
k_{M2} selected	1.03		0.98	
T^*	$567 \times 10^6 \text{ N-mm}$		$550 \times 10^6 \text{ N-mm}$	
Check $T^* > 0.25 \Phi T_{CR}$	Ignored*		Selected	
k_{M2}	0.98 or 98%			

* If selected, the T^* (calculated value for rating vehicle factored with selected k_{M2}) should be re-calculated as an uncracked sectional analysis and the re-check as per Eq. 8.2.1.2(1) of AS5100.5:2017. If torsion needs to be considered, ignore Case 1/2 and select Case 3/4.

B.7 CALCULATE LOAD RATING FACTOR k_{M3} FOR SCENARIO M3

Scenario M3

The load rating factor k_{M3} for scenario M3 is the factor of live loads that results in the utilisation of the total longitudinal reinforcement on the flexural compressive side. The objective function is,

$$\frac{M_u}{z} - \left| \frac{\Delta A_{sc}}{A_{sc}} \times \sum_{i=1}^n A_{sc} f_s \right| = \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_b z} + \frac{0.5 \times N^*}{\Phi_n}$$

Now, replacing $\frac{M_u}{z}$ with $(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt})$ considering tensile and compressive force are equal, we get updated objective function,

$$\left(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt} \right) - \left| \frac{\Delta A_{sc}}{A_{sc}} \times \sum_{i=1}^n A_{sc} f_s \right| = \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_b z} + \frac{0.5 \times N^*}{\Phi_n}$$

where,

$$\Delta A_{sc} = \frac{\Delta F_{cd}}{\Phi f_{sy}}$$

for shear only,

$$\frac{\Delta F_{cd}}{\Phi} = \left[\left(\frac{(V_{PE} + V_{CE} + k_{M3} \times V_{LL}^*) - \gamma_p P_v}{\Phi_s} \right) - 0.5 V_{us} \right] \cot(\theta_v) + \frac{0.5 * N^*}{\Phi_n} - \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_b z} \geq 0$$

for combined shear and torsion,

$$\begin{aligned} \frac{\Delta F_{cd}}{\Phi} &= \sqrt{\left[\left(\frac{(V_{PE} + V_{CE} + k_{M3} \times V_{LL}^*) - \gamma_p P_v}{\Phi_s} \right) - 0.5 V_{us} \right]^2 + \left(\frac{0.45 * (T_{PE} + T_{CE} + k_{M3} \times T_{LL}^*) \times u_h}{2A_o \Phi_t} \right)^2} \cot(\theta_v) \\ &\quad + \frac{0.5 \times N^*}{\Phi_n} - \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_b z} \geq 0 \end{aligned}$$

where,

$$V_{us} = \frac{A_{sv} f_{sy} d_v}{s} (\sin(\alpha_v) \cot(\theta_v) + \cos(\alpha_v))$$

$$\left[\left(\frac{(V_{PE} + V_{CE} + k_{M2} \times V_{LL}^*) - \gamma_p P_v}{\Phi_s} \right) - 0.5 V_{us} \right] \geq 0$$

and,

z is the internal moment lever arm between the centroids of the flexural compression force and the flexural tension force acting on the section, similar to d_v but without the limits 0.72D or 0.9d. Please note, the approach to use of z as the internal moment lever arm is an approximate method. This approximation should NOT be used while designing and subsequently for the load rating of the Design Vehicles as the quantity of additional longitudinal reinforcements and tendons are known. An iterative method should be used for more accurate rating calculation.

This equation needs to be solved for k_{M3} . As the value of θ_v in the objective function depends on the action effects, it is also dependent on the value k_{M3} . The value of k_{M3} , therefore, needs to be determined through using appropriate iterative solvers (for example using *goalseek* function). Furthermore, according to AS 5100.5:2017 Cl. 8.2.4, longitudinal strain ε_x needs to be calculated based on one of the four alternative equations determined by their sign and magnitude of the torsional action effect T^* . But, the value of T^* is also dependent on k_{M3} . Thus, four separates k_{M3} needs to be calculated through iterative processes for following four alternative cases. The final value of k_{M3} , then, needs to be selected based on the sign of ε_x and magnitude of T^* compared against $0.25\Phi T_{CR}$. Please note, as per AS 5100.5:2017 Cl. 8.2.4.3 and 8.2.4.4, for sections closer than d_o to the face of the support, the value of ε_x calculated at d_o from the face of the support may be used in evaluating ε_x and k_v .

Case 1 – shear only and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M3} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{M3} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$\frac{\Delta F_{cd}}{\Phi} = \left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s} \right) - 0.5V_{us} \right] \cot(\theta_v) + \frac{0.5 \times N^*}{\Phi_n} - \frac{M^*}{\Phi_b z} \geq 0$$

$$\Delta A_{sc} = \frac{\Delta F_{cd}}{\Phi f_{sy}}$$

$$\left(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt} \right) - \left| \frac{\Delta A_{sc}}{A_{sc}} \times \sum_{i=1}^n A_{sc} f_s \right| = \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_b z}$$

Case 2 – shear only and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M3} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{M3} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$\frac{\Delta F_{cd}}{\Phi} = \left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s} \right) - 0.5V_{us} \right] \cot(\theta_v) + \frac{0.5 \times N^*}{\Phi_n} - \frac{M^*}{\Phi_{bZ}} \geq 0$$

$$\Delta A_{sc} = \frac{\Delta F_{cd}}{\Phi f_{sy}}$$

$$\left(\sum_{i=1}^n A_{st}f_s + \sum_{i=1}^n A_{pt}\sigma_{pt} \right) - \left| \frac{\Delta A_{sc}}{A_{sc}} \times \sum_{i=1}^n A_{sc}f_s \right| = \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_{bZ}}$$

Case 3 – combined shear & torsion and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M3} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{M3} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o} \right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$\frac{\Delta F_{cd}}{\Phi} = \sqrt{\left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s} \right) - 0.5V_{us} \right]^2 + \left(\frac{0.45 \times T^* \times u_h}{2A_o \Phi_t} \right)^2} \cot(\theta_v) + \frac{0.5 \times N^*}{\Phi_n} - \frac{M^*}{\Phi_{bZ}} \geq 0$$

$$\Delta A_{sc} = \frac{\Delta F_{cd}}{\Phi f_{sy}}$$

$$\left(\sum_{i=1}^n A_{st}f_s + \sum_{i=1}^n A_{pt}\sigma_{pt} \right) - \left| \frac{\Delta A_{sc}}{A_{sc}} \times \sum_{i=1}^n A_{sc}f_s \right| = \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_{bZ}}$$

Case 4 – combined shear & torsion and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{M3} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{M3} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o}\right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$\frac{\Delta F_{cd}}{\Phi} = \sqrt{\left[\left(\frac{V^* - \gamma_p P_v}{\Phi_s}\right) - 0.5V_{us}\right]^2 + \left(\frac{0.45 \times T^* \times u_h}{2A_o \Phi_t}\right)^2} \cot(\theta_v) + \frac{0.5 \times N^*}{\Phi_n} - \frac{M^*}{\Phi_{bz}} \geq 0$$

$$\Delta A_{sc} = \frac{\Delta F_{cd}}{\Phi f_{sy}}$$

$$\left(\sum_{i=1}^n A_{st} f_s + \sum_{i=1}^n A_{pt} \sigma_{pt}\right) - \left|\frac{\Delta A_{sc}}{A_{sc}} \times \sum_{i=1}^n A_{sc} f_s\right| = \frac{(M_{PE} + M_{CE} + k_{M3} \times M_{LL}^*)}{\Phi_{bz}}$$

Location

16.96 m from the Abutment 1 Centreline (for comparison to M1 check)

Section Parameters

$\alpha_2 = 0.85$	$z = 1439 \text{ mm}$	$A_{sv} = 402 \text{ mm}^2$	$A_{cp} = 2.656 \times 10^6 \text{ mm}^2$
$\gamma = 0.70$	$d_v = 1439 \text{ mm}$	$s = 150 \text{ mm}$	$u_c = 6540 \text{ mm}$
$\Phi_b = 0.80$	$\bar{y} = 541 \text{ mm}$	$\alpha_v = 90^\circ$	$A_o = 2.084 \times 10^6 \text{ mm}^2$
$\Phi_s = 0.70$	$b_v = 250 \text{ mm}$	$A_{sc} = 6341 \text{ mm}^2$	$A_{oh} = 2.363 \times 10^6 \text{ mm}^2$
$\Phi_t = 0.70$	$t_w = 125 \text{ mm}$	$A_{st.D/2} = 6132 \text{ mm}^2$	$u_h = 6169 \text{ mm}$
$d = 1543 \text{ mm}$	$\sigma_{cp} = 6.157 \text{ MPa}$	$A_{pt.D/2} = 13728 \text{ mm}^2$	$A_{ct} = 0.609 \times 10^6 \text{ mm}^2$
$d_n = 203.6 \text{ mm}$	$d_g = 20 \text{ mm}$	$\Sigma A_{sc} f_s = -1974 \times 10^3 \text{ N}$	$\Sigma A_{st} f_s + \Sigma A_{pt} \sigma_{pt} = 26480 \times 10^3 \text{ N}$
$k_{uo} = 0.125$	$P_v = 0.0 \text{ N}$	$f_{po} = 1830 \times 0.7$	$\Phi M_u = 30492 \times 10^6 \text{ Nmm}$
$D = 1700 \text{ mm}$	$\gamma_p = 0.90$	$= 1281 \text{ MPa}$	$0.25 \Phi T_{CR} = 405.9 \times 10^6 \text{ Nmm}$

Action Effects

$M_{PE} = 11659 \times 10^6 \text{ Nmm}$	$V_{PE} = 92 \times 10^3 \text{ N}$	$T_{PE} = 239 \times 10^6 \text{ Nmm}$
$M_{CE} = 0 \text{ Nmm}$	$V_{CE} = 0 \text{ N}$	$T_{CE} = 0 \text{ Nmm}$
$M_{LL}^* = 18320 \times 10^6 \text{ Nmm}$	$V_{LL}^* = 9 \times 10^3 \text{ N}$	$T_{LL}^* = 319 \times 10^6 \text{ Nmm}$

Solve for k_{M3}

	Case 1	Case 2	Case 3	Case 4
k_{M3} solved using iteration	1.03	1.03	1.03	1.03
ε_x	0.474×10^{-3}	0.074×10^{-3}	0.559×10^{-3}	0.087×10^{-3}
ε_x sign check	Selected	Ignored	Selected	Ignored
k_{M3} selected	1.03		1.03	
T^*	567x10 ⁶ N-mm		567 x10 ⁶ N-mm	
Check $T^* > 0.25\phi T_{CR}$	Ignored*		Selected	
k_{M3}	1.03 or 103%			

* If selected, the T^* (calculated value for rating vehicle factored with selected k_{M3}) should be re-calculated as an uncracked sectional analysis and the re-check as per Eq. 8.2.1.2(1) of AS5100.5:2017. If torsion needs to be considered, ignore Case 1/2 and select Case 3/4.

B.8 CALCULATE LOAD RATING FACTOR k_{M4} FOR SCENARIO M4

Scenario M4 (SLS Longitudinal Bending Load Rating)

The Serviceability Limit State (SLS) Longitudinal bending load rating is calculated in accordance with AS 5100.5:2017 Clause 8.6.2.1(b) in which the increment in steel stress near the tension face is limited to the value obtained from Table 8.6.2.1 where the increment is defined as the increase from the value when the extreme concrete tensile fibre is at zero stress to the SLS load combination values. The moment on the cross section when the extreme concrete tensile fibre is at zero is defined as the decompression moment. The moment which corresponds to the achievement of the increment in the steel stress from the value determined at the decompression moment is defined as the serviceability bending capacity of the beam (M_s).

(Note: Detailed calculations for other provisions of AS 5100.5:2017 Cl. 8.6.2 are not shown in this example; but needs to be considered while calculating SLS crack control load rating.)

The load rating factor k_{M4} for scenario M4 is the factor of live loads that results in full utilisation of the SLS bending capacity of the cross section under consideration. The objective function is,

$$M_{sls} = M_{PE,sls} + M_{CE,sls} + k_{M4} \times M_{LL,sls}^*$$

Where:

M_{sls} = Serviceability capacity in bending (per beam)

$M_{PE,sls}$ = Serviceability design moment due to all Permanent Effects (PE)

$M_{CE,sls}$ = Serviceability design moment due to co-existing live load

$M_{LL,sls}$ = Factored serviceability design moment due to Vehicle Live Load effects (Including Gamma and DLA)

This equation needs to be solved for k_{M4} .

Location

16.96 m from the centreline of the abutment 1 bearing (approximately at the mid-span of span 1) with beam flange width 5056 mm.

Action Effects and Capacity

$$M_{PE,sls} = 9342 \text{ kNm}$$

$$M_{CE,sls} = 0 \text{ kNm}$$

$$M_{LL,sls} = 10209 \text{ kNm}$$

$$M_s = 24172 \text{ kNm}$$

Solve for k_{M4}

Solving for k_{M4} we determine its value to be 1.453 or 145%.

B.9 CALCULATE LOAD RATING FACTOR k_{V1} FOR SCENARIO V1

Scenario V1

The load rating factor k_{V1} for scenario V1 is the factor of live loads that results in the utilisation of the shear capacity. Main Roads WA SES Circular 01-20 amendment to shear design formulas amended the AS 5100.5:2017 Eq. 8.2.3.1 and the objective function is,

$$\Phi_s V_u = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

where,

$$\Phi_s V_u = \Phi_s V_{uc} + \Phi_s V_{us} + P_v \leq V_{u,max}$$

or,

$$\Phi_s V_u = \Phi_s k_v \sqrt{f'_c} b_v d_v + \frac{\Phi_s A_{sv} f_{sy} d_v}{s} (\sin(\alpha_v) \cot(\theta_v) + \cos(\alpha_v)) + P_v \leq \Phi_s V_{u,max}$$

and,

$$\sqrt{f'_c} \leq 8 \text{ MPa}$$

$$V_{u,max} = 0.55 f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

This equation needs to be solved for k_{V1} . As the value of θ_v in the objective function depends on the action effects, it is also dependent on the value k_{V1} . The value of k_{V1} , therefore, needs to be determined through using appropriate iterative solvers (for example using *goalseek* function). Furthermore, according to AS 5100.5:2017 Cl. 8.2.4, longitudinal strain ϵ_x needs to

be calculated based on one of the four alternative equations determined by their sign and magnitude of the torsional action effect T^* . But, the value of T^* is also dependent on k_{V1} . Thus, four separate k_{V1} needs to be calculated through iterative processes for following four alternative cases. The final value of k_{V1} , then, needs to be selected based on the sign of ε_x and magnitude of T^* compared against $0.25\Phi T_{CR}$. Please note, as per AS 5100.5:2017 Cl. 8.2.4.3 and 8.2.4.4, for sections closer than d_o to the face of the support, the value of ε_x calculated at d_o from the face of the support may be used in evaluating ε_x and k_v .

Case 1 – shear only and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V1} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V1} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

$$\Phi_s V_u = \Phi_s k_v \sqrt{f'_c} b_v d_v + \frac{\Phi_s A_{sv} f_{sy} d_v}{s} (\sin(\alpha_v) \cot(\theta_v) + \cos(\alpha_v)) + P_v \leq \Phi_s V_{u,max}$$

$$\Phi_s V_u = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

Case 2 – shear only and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V1} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V1} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

$$\Phi_s V_u = \Phi_s k_v \sqrt{f'_c} b_v d_v + \frac{\Phi_s A_{sv} f_{sy} d_v}{s} (\sin(\alpha_v) \cot(\theta_v) + \cos(\alpha_v)) + P_v \leq \Phi_s V_{u,max}$$

$$\Phi_s V_u = V_{PE} + V_{CE} + k_{V1} * V_{LL}^*$$

Case 3 – combined shear & torsion and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V1} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V1} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o} \right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

$$\Phi_s V_u = \Phi_s k_v \sqrt{f'_c} b_v d_v + \frac{\Phi_s A_{sv} f_{sy} d_v}{s} (\sin(\alpha_v) \cot(\theta_v) + \cos(\alpha_v)) + P_v \leq \Phi_s V_{u,max}$$

$$\Phi_s V_u = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

Case 4 – combined shear & torsion and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V1} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V1} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o} \right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

$$\Phi_s V_u = \Phi_s k_v \sqrt{f'_c} b_v d_v + \frac{\Phi_s A_{sv} f_{sy} d_v}{s} (\sin(\alpha_v) \cot(\theta_v) + \cos(\alpha_v)) + P_v \leq \Phi_s V_{u,max}$$

$$\Phi_s V_u = V_{PE} + V_{CE} + k_{V1} \times V_{LL}^*$$

Location

8.68 m from the Abutment 1 Centreline.

Section Parameters

$\alpha_2 = 0.85$	$z = 1439 \text{ mm}$	$A_{sv} = 402 \text{ mm}^2$	$A_{cp} = 2.656 \times 10^6 \text{ mm}^2$
$\gamma = 0.70$	$d_v = 1439 \text{ mm}$	$s = 150 \text{ mm}$	$u_c = 6540 \text{ mm}$
$\Phi_b = 0.80$	$\bar{y} = 541 \text{ mm}$	$\alpha_v = 90^\circ$	$A_o = 2.084 \times 10^6 \text{ mm}^2$
$\Phi_s = 0.70$	$b_v = 250 \text{ mm}$	$A_{sc} = 6341 \text{ mm}^2$	$A_{oh} = 2.363 \times 10^6 \text{ mm}^2$
$\Phi_t = 0.70$	$t_w = 125 \text{ mm}$	$A_{st.D/2} = 6132 \text{ mm}^2$	$u_h = 6169 \text{ mm}$
$d = 1543 \text{ mm}$	$\sigma_{cp} = 6.142 \text{ MPa}$	$A_{pt.D/2} = 13728 \text{ mm}^2$	$A_{ct} = 0.609 \times 10^6 \text{ mm}^2$
$d_n = 203.6 \text{ mm}$	$d_g = 20 \text{ mm}$	$\Sigma A_{sc} f_s = -1974 \times 10^3 \text{ N}$	$\Sigma A_{st} f_s + \Sigma A_{pt} \sigma_{pt} = 26480 \times 10^3 \text{ N}$
$k_{uo} = 0.125$	$P_v = 0.0 \text{ N}$	$f_{po} = 1830 \times 0.7$ $= 1281 \text{ MPa}$	$\Phi M_u = 30492 \times 10^6 \text{ Nmm}$
$D = 1700 \text{ mm}$	$\gamma_p = 0.90$		$0.25 \Phi T_{CR} = 405.5 \times 10^6 \text{ Nmm}$

Action Effects

$M_{PE} = 9241 \times 10^6 \text{ Nmm}$	$V_{PE} = 683 \times 10^3 \text{ N}$	$T_{PE} = 348 \times 10^6 \text{ Nmm}$
$M_{CE} = 0 \text{ Nmm}$	$V_{CE} = 0 \text{ N}$	$T_{CE} = 0 \text{ Nmm}$
$M_{LL}^* = 12510 \times 10^6 \text{ Nmm}$	$V_{LL}^* = 1463 \times 10^3 \text{ N}$	$T_{LL}^* = 458 \times 10^6 \text{ Nmm}$

Solve for k_{V1}

	Case 1	Case 2	Case 3	Case 4
k_{V1} solved using iteration	1.33	1.57	1.32	1.56
ε_x	0.391×10^{-3}	0.108×10^{-5}	0.411×10^{-3}	0.113×10^{-3}
ε_x sign check	Selected	Ignored	Selected	Ignored
k_{V1} selected	1.33		1.32	
T^*	958x10 ⁶ N-mm		952 x10 ⁶ N-mm	
Check $T^* > 0.25 \Phi T_{CR}$	Ignored*		Selected	
k_{V1}	1.32 or 132%			

* If selected, the T^* (calculated value for rating vehicle factored with selected k_{V1}) should be re-calculated as an uncracked sectional analysis and the re-check as per Eq. 8.2.1.2(1) of AS5100.5:2017. If torsion needs to be considered, ignore Case 1/2 and select Case 3/4.

B.10 CALCULATE LOAD RATING FACTOR k_{V2} FOR SCENARIO V2

Scenario V2

The load rating factor k_{V2} for scenario V2 is the factor of live loads that results in the utilisation of the web crushing capacity. Main Roads WA SES Circular 01-20 amendment to shear design formulas amended the AS 5100.5:2017 Eq. 8.2.4.5 and the objective function is,

For box sections,

(i) Where wall thickness $t_w > A_{oh}/u_h$

$$\frac{\Phi_b V_{u,max}}{b_v d_v} = \frac{(V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*)}{b_v d_v} + \frac{(T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*) \times u_h}{1.7 A_{oh}^2}$$

(ii) Where wall thickness $t_w \leq A_{oh}/u_h$

$$\frac{\Phi_b V_{u,max}}{b_v d_v} = \frac{(V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*)}{b_v d_v} + \frac{(T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*)}{1.7 t_w A_{oh}}$$

For other sections,

$$\frac{\Phi_b V_{u,max}}{b_v d_v} = \sqrt{\left[\frac{(V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*)}{b_v d_v} \right]^2 + \left[\frac{(T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*) \times u_h}{1.7 A_{oh}^2} \right]^2}$$

where,

$$V_{u,max} = 0.55 f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

This equation needs to be solved for k_{V2} . As the value of θ_v in the objective function depends on the action effects, it is also dependent on the value k_{V2} . The value of k_{V2} , therefore, needs to be determined through using appropriate iterative solvers (for example using *goalseek* function). Furthermore, according to AS 5100.5:2017 Cl. 8.2.4, longitudinal strain ϵ_x needs to be calculated based on one of the four alternative equations determined by their sign and magnitude of the torsional action effect T^* . But, the value of T^* is also dependent on k_{V2} . Thus, four separate k_{V2} needs to be calculated through iterative processes for following four alternative cases. The final value of k_{V2} , then, needs to be selected based on the sign of ϵ_x and magnitude of T^* compared against $0.25 \Phi T_{CR}$. Please note, as per AS 5100.5:2017 Cl. 8.2.4.3 and 8.2.4.4, for sections closer than d_o to the face of the support, the value of ϵ_x calculated at d_o from the face of the support may be used in evaluating ϵ_x and k_v .

Case 1 – shear only and $\epsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

As $t_w \leq A_{oh}/u_h$,

$$\frac{\Phi_s V_{u,max}}{b_v d_v} = \frac{(V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*)}{b_v d_v} + \frac{(T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*)}{1.7t_w A_{oh}}$$

Case 2 – shear only and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

As $t_w \leq A_{oh}/u_h$,

$$\frac{\Phi_s V_{u,max}}{b_v d_v} = \frac{(V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*)}{b_v d_v} + \frac{(T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*)}{1.7t_w A_{oh}}$$

Case 3 – combined shear & torsion and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o}\right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

$$\text{As } t_w \leq A_{oh}/u_h,$$

$$\frac{\Phi_s V_{u,max}}{b_v d_v} = \frac{(V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*)}{b_v d_v} + \frac{(T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*)}{1.7 t_w A_{oh}}$$

Case 4 – combined shear & torsion and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o}\right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$V_{u,max} = 0.55f'_c b_v d_v \left(\frac{\cot(\theta_v)}{1 + \cot^2(\theta_v)} \right) + P_v$$

$$\text{As } t_w \leq A_{oh}/u_h,$$

$$\frac{\Phi_s V_{u,max}}{b_v d_v} = \frac{(V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*)}{b_v d_v} + \frac{(T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*)}{1.7 t_w A_{oh}}$$

Location

1.93 m from the Abutment 1 Centreline.

Section Parameters

$\alpha_2 = 0.85$	$z = 1347 \text{ mm}$	$A_{sv} = 628 \text{ mm}^2$	$A_{cp} = 2.656 \times 10^6 \text{ mm}^2$
$\gamma = 0.70$	$d_v = 1393 \text{ mm}$	$s = 150 \text{ mm}$	$u_c = 6540 \text{ mm}$
$\Phi_b = 0.80$	$\bar{y} = 559 \text{ mm}$	$\alpha_v = 90^\circ$	$A_o = 1.976 \times 10^6 \text{ mm}^2$
$\Phi_s = 0.70$	$b_v = 400 \text{ mm}$	$A_{sc} = 6341 \text{ mm}^2$	$A_{oh} = 2.354 \times 10^6 \text{ mm}^2$
$\Phi_t = 0.70$	$t_w = 200 \text{ mm}$	$A_{st.d/2} = 6584 \text{ mm}^2$	$u_h = 6157 \text{ mm}$
$d = 1548 \text{ mm}$	$\sigma_{cp} = 4.011 \text{ MPa}$	$A_{pt.d/2} = 8866 \text{ mm}^2$	$A_{ct} = 0.609 \times 10^6 \text{ mm}^2$
$d_n = 157.6 \text{ mm}$	$d_g = 20 \text{ mm}$	$\Sigma A_{sc} f_s = -1439.3 \times 10^3 \text{ N}$	$\Sigma A_{st} f_s + \Sigma A_{pt} \sigma_{pt} = 20402.3 \times 10^3 \text{ N}$
$k_{uo} = 0.097$	$P_v = 0.0 \text{ N}$	$f_{po} = 1830 \times 0.7 = 1281 \text{ MPa}$	$\Phi M_u = N/A$
$D = 1700 \text{ mm}$	$\gamma_p = 0.90$		$0.25 \Phi T_{CR} = 532.2 \times 10^6 \text{ Nmm}$

Action Effects

$M_{PE} = 1933 \times 10^6 \text{ Nmm}$	$V_{PE} = 1370 \times 10^3 \text{ N}$	$T_{PE} = 378 \times 10^6 \text{ Nmm}$
$M_{CE} = 0 \text{ Nmm}$	$V_{CE} = 0 \text{ N}$	$T_{CE} = 0 \text{ Nmm}$
$M_{LL}^* = 3318 \times 10^6 \text{ Nmm}$	$V_{LL}^* = 2331 \times 10^3 \text{ N}$	$T_{LL}^* = 480 \times 10^6 \text{ Nmm}$

Solve for k_{V2}

	Case 1	Case 2	Case 3	Case 4
k_{V2} solved using iteration	0.88	1.08	0.89	1.08
ε_x	-0.734×10^{-3}	-0.066×10^{-3}	-0.694×10^{-3}	-0.062×10^{-3}
ε_x sign check	Ignored	Selected	Ignored	Selected
k_{V2} selected	1.08		1.08	
T^*	894 $\times 10^6$ N-mm		895 $\times 10^6$ N-mm	
Check $T^* > 0.25 \Phi T_{CR}$	Ignored*		Selected	
k_{V2}	1.08 or 108%			

* If selected, the T^* (calculated value for rating vehicle factored with selected k_{V2}) should be re-calculated as an uncracked sectional analysis and the re-check as per Eq. 8.2.1.2(1) of AS5100.5:2017. If torsion needs to be considered, ignore Case 1/2 and select Case 3/4.

B.11 CALCULATE LOAD RATING FACTOR k_{V3} FOR SCENARIO V3 AND k_{V4} FOR SCENARIOS V4

The load rating factor k_{V3} should be calculated following the similar method for calculating k_{M2} and k_{V4} should be calculated following the similar method for calculating k_{M3} .

B.12 CALCULATE LOAD RATING FACTOR k_{V5} FOR SCENARIO V5

Scenario V5

The load rating factor k_{V2} for scenario V2 is the factor of live loads that results in the utilisation of the closed tie cross sectional area for shear and coexisting torsion. The objective function is,

For closed tie reinforcement,

$$\frac{A_{sv}}{2} = \left[0.5 \times \left\{ \frac{(V_{PE} + V_{CE} + k_{V5} \times V_{LL}^*) - \Phi_s V_{uc}}{\Phi_s f_{sy} \left(\frac{d_v}{s}\right) \cot(\theta_v)} \right\} + \frac{(T_{PE} + T_{CE} + k_{V5} \times T_{LL}^*) \times s}{\Phi_t 2A_o f_{sy} \cot(\theta_v)} \right]$$

where,

A_{sv} = Total cross-sectional area of closed tie reinforcement provided to resist shear and torsion. Thus, $A_{sv} / 2$ the cross-sectional area provided to resist shear and torsion for the critical web.

In principle, this equation states that the utilisation of the closed tie reinforcement occurs when the demand from shear on one web is added to the demand from co-existing torsion. Please note, the demand from torsion is additive to one web and deductive on the other. The V5 formula has been provided for the critical web where the effects are additive and assumes that the design shear is shared evenly between all webs in the cross section based on the webs having the same stiffnesses.

This equation needs to be solved for k_{V5} . As the value of θ_v in the objective function depends on the action effects, it is also dependent on the value k_{V5} . The value of k_{V5} , therefore, needs to be determined through using appropriate iterative solvers (for example using *goalseek* function). Furthermore, according to AS 5100.5:2017 Cl. 8.2.4, longitudinal strain ϵ_x needs to be calculated based on one of the four alternative equations determined by their sign and magnitude of the torsional action effect T^* . But, the value of T^* is also dependent on k_{V5} . Thus, four separate k_{V5} needs to be calculated through iterative processes for following four alternative cases. The final value of k_{V5} , then, needs to be selected based on the sign of ϵ_x and magnitude of T^* compared against $0.25\Phi T_{CR}$. Please note, as per AS 5100.5:2017 Cl. 8.2.4.3 and 8.2.4.4, for sections closer than d_o to the face of the support, the value of ϵ_x calculated at d_o from the face of the support may be used in evaluating ϵ_x and k_v .

Case 1 – shear only and $\epsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$\Phi_s V_{uc} = \Phi_s k_v \sqrt{f'_c} b_v d_v$$

$$\frac{A_{sv}}{2} = \left[0.5 \times \left\{ \frac{(V_{PE} + V_{CE} + k_{V5} \times V_{LL}^*) - \Phi_s V_{uc}}{\Phi_s f_{sy} \left(\frac{d_v}{s} \right) \cot(\theta_v)} \right\} + \frac{(T_{PE} + T_{CE} + k_{V5} \times T_{LL}^*) \times s}{\Phi_t 2A_o f_{sy} \cot(\theta_v)} \right]$$

Note: for calculating k_v , use limits $-0.2 \times 10^{-3} \leq \varepsilon_x \leq 3.0 \times 10^{-3}$

Case 2 – shear only and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\left| \frac{M^*}{d_v} + V^* \right| - P_v + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$\Phi_s V_{uc} = \Phi_s k_v \sqrt{f'_c} b_v d_v$$

$$\frac{A_{sv}}{2} = \left[0.5 \times \left\{ \frac{(V_{PE} + V_{CE} + k_{V5} \times V_{LL}^*) - \Phi_s V_{uc}}{\Phi_s f_{sy} \left(\frac{d_v}{s} \right) \cot(\theta_v)} \right\} + \frac{(T_{PE} + T_{CE} + k_{V5} \times T_{LL}^*) \times s}{\Phi_t 2A_o f_{sy} \cot(\theta_v)} \right]$$

Note: for calculating k_v , use limits $-0.2 \times 10^{-3} \leq \varepsilon_x \leq 3.0 \times 10^{-3}$

Case 3 – combined shear & torsion and $\varepsilon_x \leq 3.0 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o}\right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt})}$$

$$\theta_v = (29 + 7000 \times \varepsilon_x)$$

$$\Phi_s V_{uc} = \Phi_s k_v \sqrt{f'_c} b_v d_v$$

$$\frac{A_{sv}}{2} = \left[0.5 \times \left\{ \frac{(V_{PE} + V_{CE} + k_{V5} \times V_{LL}^*) - \Phi_s V_{uc}}{\Phi_s f_{sy} \left(\frac{d_v}{s}\right) \cot(\theta_v)} \right\} + \frac{(T_{PE} + T_{CE} + k_{V5} \times T_{LL}^*) \times s}{\Phi_t 2A_o f_{sy} \cot(\theta_v)} \right]$$

Note: for calculating k_v , use limits $-0.2 \times 10^{-3} \leq \varepsilon_x \leq 3.0 \times 10^{-3}$

Case 4 – combined shear & torsion and $\varepsilon_x \geq -0.2 \times 10^{-3}$

$$M^* = M_{PE} + M_{CE} + k_{V2} \times M_{LL}^*$$

$$V^* = V_{PE} + V_{CE} + k_{V2} \times V_{LL}^*$$

$$T^* = T_{PE} + T_{CE} + k_{V2} \times T_{LL}^*$$

$$\varepsilon_x = \frac{\frac{M^*}{d_v} + \sqrt{(V^* - P_v)^2 + \left(\frac{0.9 \times T^* \times u_h}{2A_o}\right)^2} + 0.5N^* - A_{pt}f_{po}}{2(E_s A_{st} + E_p A_{pt} + E_c A_{ct})}$$

$$\theta_v = 29 + 7000 \times \varepsilon_x$$

$$\Phi_s V_{uc} = \Phi_s k_v \sqrt{f'_c} b_v d_v$$

$$\frac{A_{sv}}{2} = \left[0.5 * \left\{ \frac{(V_{PE} + V_{CE} + k_{V5} \times V_{LL}^*) - \Phi_s V_{uc}}{\Phi_s f_{sy} \left(\frac{d_v}{s}\right) \cot(\theta_v)} \right\} + \frac{(T_{PE} + T_{CE} + k_{V5} \times T_{LL}^*) \times s}{\Phi_t 2A_o f_{sy} \cot(\theta_v)} \right]$$

Note: for calculating k_v , use limits $-0.2 \times 10^{-3} \leq \varepsilon_x \leq 3.0 \times 10^{-3}$

Location

8.68 m from the Abutment 1 Centreline.

Section Parameters

$\alpha_2 = 0.85$	$z = 1439 \text{ mm}$	$A_{sv} = 402 \text{ mm}^2$	$A_{cp} = 2.656 \times 10^6 \text{ mm}^2$
$\gamma = 0.70$	$d_v = 1439 \text{ mm}$	$s = 150 \text{ mm}$	$u_c = 6540 \text{ mm}$
$\Phi_b = 0.80$	$\bar{y} = 541 \text{ mm}$	$\alpha_v = 90^\circ$	$A_o = 2.084 \times 10^6 \text{ mm}^2$
$\Phi_s = 0.70$	$b_v = 250 \text{ mm}$	$A_{sc} = 6341 \text{ mm}^2$	$A_{oh} = 2.363 \times 10^6 \text{ mm}^2$
$\Phi_t = 0.70$	$t_w = 125 \text{ mm}$	$A_{st.D/2} = 6132 \text{ mm}^2$	$u_h = 6169 \text{ mm}$
$d = 1543 \text{ mm}$	$\sigma_{cp} = 6.142 \text{ MPa}$	$A_{pt.D/2} = 13728 \text{ mm}^2$	$A_{ct} = 0.609 \times 10^6 \text{ mm}^2$
$d_n = 203.6 \text{ mm}$	$d_g = 20 \text{ mm}$	$\Sigma A_{sc} f_s = -1974 \times 10^3 \text{ N}$	$\Sigma A_{st} f_s + \Sigma A_{pt} \sigma_{pt} = 26480 \times 10^3 \text{ N}$
$k_{uo} = 0.125$	$P_v = 0.0 \text{ N}$	$f_{po} = 1830 \times 0.7 = 1281 \text{ MPa}$	$\Phi M_u = 30492 \times 10^6 \text{ Nmm}$
$D = 1700 \text{ mm}$	$\gamma_p = 0.90$		$0.25 \Phi T_{CR} = 405.5 \times 10^6 \text{ Nmm}$

Action Effects

$M_{PE} = 9241 \times 10^6 \text{ Nmm}$	$V_{PE} = 683 \times 10^3 \text{ N}$	$T_{PE} = 348 \times 10^6 \text{ Nmm}$
$M_{CE} = 0 \text{ Nmm}$	$V_{CE} = 0 \text{ N}$	$T_{CE} = 0 \text{ Nmm}$
$M_{LL}^* = 12510 \times 10^6 \text{ Nmm}$	$V_{LL}^* = 1463 \times 10^3 \text{ N}$	$T_{LL}^* = 458 \times 10^6 \text{ Nmm}$

Solve for k_{V5}

	Case 1	Case 2	Case 3	Case 4
k_{V5} solved using iteration	1.13	1.22	1.12	1.21
ϵ_x	0.132×10^{-3}	0.037×10^{-3}	0.149×10^{-3}	0.042×10^{-3}
ϵ_x sign check	Selected	Ignored	Selected	Ignored
k_{V5} selected	1.13		1.12	
T^*	867x10 ⁶ N-mm		861x10 ⁶ N-mm	
Check $T^* > 0.25 \Phi T_{CR}$	Ignored*		Selected	
k_{V5}	1.12 or 112%			

* If selected, the T^* (calculated value for rating vehicle factored with selected k_{V5}) should be re-calculated as an uncracked sectional analysis and the re-check as per Eq. 8.2.1.2(1) of AS5100.5:2017. If torsion needs to be considered, ignore Case 1/2 and select Case 3/4.

APPENDIX C

Example of Load Rating Memo and Report (Non-Timber Bridges)

APPENDIX C - EXAMPLE OF LOAD RATING MEMO AND REPORT

C.1 MEMORANDUM

File : **20/9842**
To : **Engineer Bridge Loading**
Subject : **Bridge No. 1694 on Murdoch Drive over Farrington Road**
Heavy Loads Assessment / Load Rating

1. In response to your request to assess the above bridge, a load rating check for SM1600, T44, HLP, Group 1 and Group 2 vehicles has been completed. A detailed Load Rating Report is attached with this memo.
2. The bridge is a two-span simply supported precast tee-roff structure on a skew (21.7°) and curve of approximately 477 m radius. The spans are 31.9 m and 21.6 m respectively and the 4 No. beams are spaced at 4.949 m, 5.302 m and 5.231 m, with an 18.5 m width between edge kerbs. A 2.5 m median kerb separates dual carriageways.

At the abutments, each beam is supported on a column behind MSE wall panels, which are founded on spread footings. At the pier, 2 No. columns support the superstructure via a footing and piles. Elastomeric bearings are used at each end of each beam at both abutments and pier.

The structure was built in 2019 and is owned and operated by Main Roads WA. Refer Load Rating Report for general arrangement of Bridge No. 1694.

3. The analysis incorporates the following approach:
 - 5 No. standard design lanes for SM1600, and 6 No. standard design lanes for T44 and Group 1 vehicles without the median kerb.
 - 2 No. lane carriageways in both directions, assessed with and without the median kerb for HLP and Group 2 vehicles.
 - All materials as per IFC drawings (“as new” condition).
 - Yield stress of 500 MPa in the reinforcement and 1500 MPa in the prestressed strands.
 - Precast concrete tee-roff beams grade 50 MPa and in-situ deck slab 40 MPa.
 - Moment re-distribution has not been considered in this load rating (structure is simply supported).
 - Moment and shear capacities were derived using modified compression field theory (MCFT).
 - Settlement and temperature were not considered for the simply supported structure.
4. Cross-sections have been checked at 0.1 m intervals along the length of the beam to account for the interaction between moment, shear and torsion and the cross-section capacities of the associated section.
5. The bridge was analysed using Structural Bridge Design (SBD) software. The grillage type, aspect ratio, node locations and transverse member orientation were determined in line with Bridge Deck Behaviour (Hambly, 1991).

Each beam was modelled by a longitudinal member using properties of the transformed beam-slab section, accounting for varying flange widths. The ends of beams were free to rotate over the pier, to model cracking expected in the link slabs.

Transverse members comprised rigid links extending to the webs of beams, and deck-slab members connected the rigid links of adjacent beams.

Refer Load Rating Report for grillage setup and models.

6. Torsional stiffness of all members was factored by 0.2 to account for cracking at ULS.
7. The section capacities were obtained using in-house software/spreadsheet. The minimum flange width of each span was used, and the deck-slab width was transformed using concrete section properties.
8. Dead loads included self-weight of the beams with 200 mm nominated minimum slab thickness plus an additional 50 mm allowance for beam hog.

Guardrails, kerbs and 100 mm thick asphalt were applied as superimposed dead loads, factored by 1.4 as they are controlled by the relevant authority.

9. Vehicles were assessed to travel in both directions. Group 2 Vehicle 8 was limited in the 8.0 m wide carriageway to within 0.2 m of the kerbs. HLP and Group 2 vehicles were assessed with and without:
 - The 2.5 m median kerb; and
 - Co-existing effects (CE) of 50% SM1600 in the opposite carriageway.
10. External beams governed the load ratings for both spans. Bending and shear load rating factors were calculated for 3 No. cases; (a) Maximum moment, associated shear and torsion, (b) Maximum shear, associated moment and torsion and (c) Maximum torsion, associated moment and shear.
11. 4 No. bending ratings (M1-M4) and 5 No. shear ratings (V1-V5) were obtained to determine the controlling condition, as the interaction between bending, shear and torsion impacts the cross-section capacities and the critical locations also vary.

Moment capacities were adjusted by percentage demand for bending, as a proportion of applied bending, shear and torsion.

Shear capacities were adjusted by percentage demand for shear, as proportion of applied shear and torsion.

12. Based on the above criteria, the table below shows the summary of governing load ratings for each vehicle. s

Load Rating Summary					
Vehicle	Span	Load Rating (%)	Location from Support CL (m)*	Governing Case	Governing Capacity
SM1600	1	98%	16.957	M	k_{M2}
T44	2	157%	10.297	M	k_{M1}
HLP 320	1	104%	14.962	M	k_{M2}
HLP 400	1	89%	16.159	M	k_{M2}
GROUP 1, VEHICLE 1	2	285%	9.097	M	k_{M1}
GROUP 1, VEHICLE 2	1	208%	14.962	M	k_{M2}
GROUP 1, VEHICLE 3	1	188%	14.962	M	k_{M2}
GROUP 1, VEHICLE 4	1	194%	14.962	M	k_{M2}
GROUP 2, VEHICLE 1 - 3.01	2	272%	8.997	M	k_{M1}
GROUP 2, VEHICLE 1 - 3.70	2	272%	8.997	M	k_{M1}
GROUP 2, VEHICLE 2 - 3.01	2	239%	13.295	V	k_{V5}
GROUP 2, VEHICLE 2 - 3.70	2	250%	9.097	M	k_{M1}
GROUP 2, VEHICLE 4	2	174%	10.297	M	k_{M1}
GROUP 2, VEHICLE 4 - NS	2	147%	10.297	M	k_{M1}
GROUP 2, VEHICLE 5	2	133%	10.297	M	k_{M1}
GROUP 2, VEHICLE 5 - NS	2	112%	10.297	M	k_{M1}
GROUP 2, VEHICLE 7	1	88%	16.159	M	k_{M2}
GROUP 2, VEHICLE 8	1	70%	16.159	M	k_{M2}

Notes: k_{m1} indicates no additional longitudinal force acquired from shear and torsion.
 σ_{pu} has been used as per AS 5100.5:2017 Clause 8.1.7.
 *Support at end of lowest chainage.

13. The following have been checked and found not to govern the load ratings:

- Transverse bending and shear of the deck slab;
- Interface shear – longitudinal and transverse;
- Bearings, substructure and foundations; and
- Compression fan regions.

14. For your information, as requested.

ENGINEER
 01 June 2022

C.2 LOAD RATING REPORT

C.2.1 Introduction

This load rating report of Bridge No. 1694 incorporates the shear strength analysis using the Modified Compression Field Theory (MCFT) approach of concrete sections in AS 5100.5:2017 (incorporating Amendment 1 issued 2018). It is similar to design guides AASHTO Load and Resistance Factor Design (LRFD) and Canadian Highway Bridge Design Code (CHBDC). Shear capacities were derived through combining design shear, bending and torsion actions at a given cross-section.

C.2.2 List of Symbols and Abbreviations

CE	Co-existing Loads
DL	Dead Loads
EBL	Engineer Bridge Loading
EQ	Earthquake (Load)
LL	Live Loads
MCFT	Modified Compression Field Theory
MRWA	Main Roads Western Australia
PE	Permanent Effects
PSP	Principal Shared Path
SDL	Superimposed Dead Loads
SES	Senior Engineer Structures
SLS	Serviceability Limit State
ULS	Ultimate Limit State
d_o	Distance from the outermost compression fibre to the centroid of outer-most tensile reinforcement
f'_c	Characteristic compressive (cylinder) strength of concrete at 28 days
f_{PB}	Characteristic minimum breaking strength of tendons
f_{PY}	Yield strength of tendons
f_{PO}	Stress in prestressed reinforcement when stress in the surrounding concrete is zero
f_{SY}	Characteristic yield strength of reinforcement
A_P	Area of tendons
E_C	Mean value of the modulus of elasticity of concrete at 28 days
E_P	Modulus of elasticity of tendons
E_S	Modulus of elasticity of reinforcement
θ_v	Angle between axis of the concrete compression strut and longitudinal axis of a member
M^*	Design bending moment at a cross-section
V^*_{LL}	Design shear force at a cross-section due to live loads
V_{PE+CE}	Design shear force at a cross-section due to permanent effects and co-existing loads
V_{SDL+CE}	Design shear force at a cross-section due to superimposed dead loads and co-existing loads

V_{CORR}	Corresponding design shear force at a cross-section
M_S	Design serviceability strength in bending at a cross-section, derived from maximum allowable increment of steel stress from the decompression moment
ϕM_U	Design ultimate strength in bending at a cross-section
$\phi M_{U,M}$	Design ultimate strength in bending at a cross-section adjusted by % tensile force demand from bending as a proportion of axial, bending, shear and torsion actions
ϕV_{UC}	Design ultimate shear strength at a cross-section excluding shear reinforcement
$q_{ALLOWABLE}$	Design shear flow capacity at a cross-section
q_{LL}	Shear flow at a cross-section due to live loads
q_{PE+CE}	Shear flow at a cross-section due to permanent effects and co-existing loads
q_{SDL+CE}	Shear flow at a cross-section due to superimposed dead loads and co-existing loads

C.2.3 References

- Hambly, E. C. (1991). *Bridge deck behaviour*. CRC Press.
- BBR Australia (1973). *BBR Multi-wire System: Prestressing Manual (metric)*. BBR Australia Pty Ltd.

C.2.4 Bridge Details

Bridge No. 1694 was constructed in 2019. It carries Murdoch Drive Extension over Farrington Road in the City of Cockburn, within the Metropolitan region. The bridge is owned and operated by Main Roads Western Australia (MRWA). Refer Figure C.1 for the location of the bridge.

The bridge is a two-span simply supported precast tee-roff structure on a skew (21.7°) and curve of approximately 477 m radius. The span lengths are 31.9 m and 20.6 m respectively and the 4No. beams are spaced at 4.949 m, 5.302 m and 5.231 m, with an 18.5 m width between kerbs. At the abutments, each beam is supported on a column located behind MSE walls, which are founded on a shared spread footing. At the Pier, 2No. blade piers support the superstructure via a shared footing and piles. Elastomeric bearings are used at both the abutments and the pier.

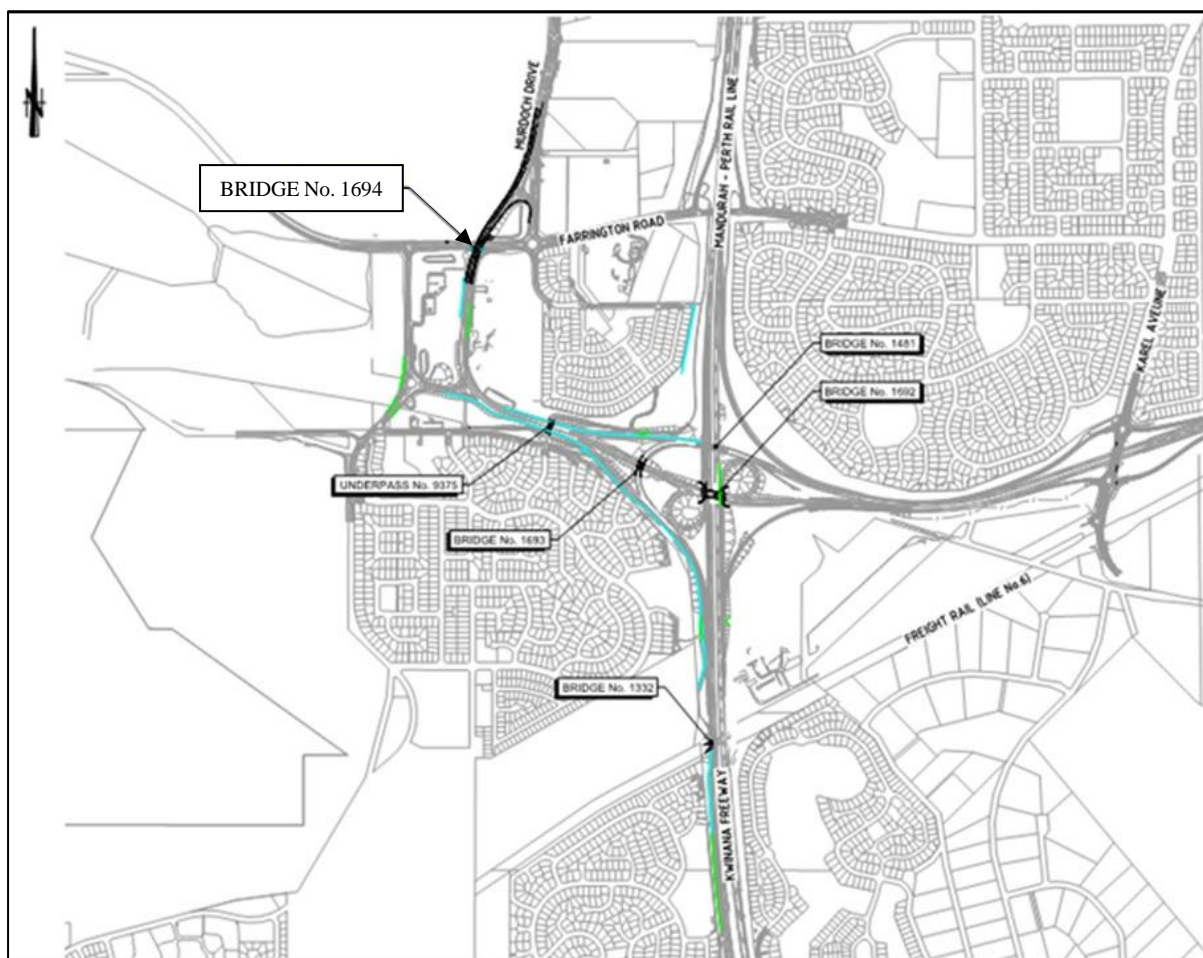


Figure C.1 Location of Bridge No. 1694

Bridge No. 1694 has dual-lane carriageways in both directions (north and south) separated by a 2.5 m wide median kerb. Figure C.2 and Figure C.3 show the plan and typical cross section of the bridge.

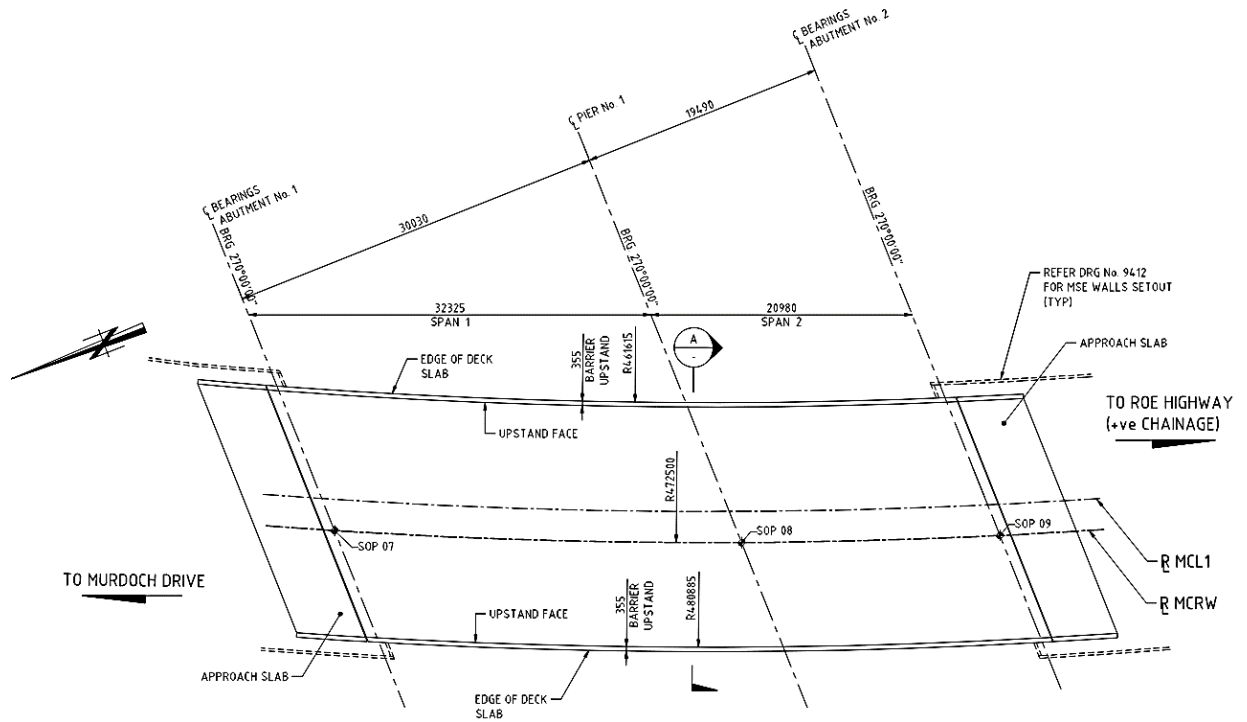


Figure C.2 Plan View of the Bridge

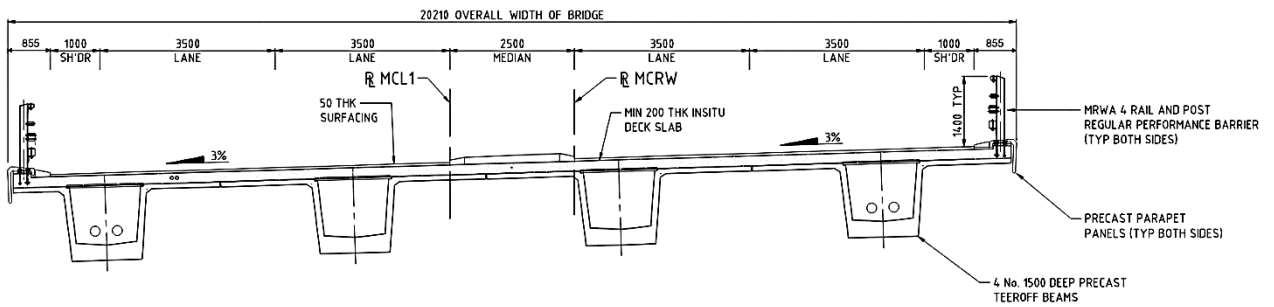


Figure C.3 Typical Cross Section of the Bridge

C.2.5 Material Properties

Material properties of Bridge No. 1694 are shown in Table C.1. The bridge is approximately two years old and is in good condition.

Table C.1 Bridge No. 1694 Material Properties

Material	Property	Symbol	Unit	Value	Reference
Prestress (15.2mm Dia. 7-Wire Super Strand)	Breaking Stress	f_{PB}	MPa	1830	T 3.3.1 AS 5100.5:2017
	Yield Stress	f_{PY}	MPa	1501	Cl 3.3.1(b) AS 5100.5:2017
	Elastic Modulus	E_P	MPa	195000	Cl 3.3.2 AS 5100.5:2017
	Area per Tendon	A_P	mm ²	143	T 3.3.1 AS 5100.5:2017
Reinforcement	Yield Strength	f_{SY}	MPa	500	T 3.2.1 AS 5100.5:2017
	Elastic Modulus	E_S	MPa	200000	Cl 3.2.2 AS 5100.5:2017
Concrete Precast Beam	28 Day Strength	f'_c	MPa	50	10-0107-040-BR- DG-9402
	Elastic Modulus	E_C	MPa	34800	T 3.1.2 AS 5100.5:2017
Concrete In-situ Slab	28 Day Strength	f'_c	MPa	40	10-0107-040-BR- DG-9402
	Elastic Modulus	E_C	MPa	32800	T 3.1.2 AS 5100.5:2017

C.2.6 Critical Locations and Section Parameters

The beams are supported on bearings via a heavily reinforced diaphragm. A compression fan region (refer AS 5100.5:2017 Cl 8.2.9.2) was therefore idealised over supports and extended to d_o . The heavily reinforced end-diaphragms provided adequate stress paths through strut-and-tie action. The longitudinal load rating was therefore carried out starting from d_o from face of bearings, at 0.1 m increments along the spans for all beams (complying with AS 5100.5:2017 Cl 8.2.9.1 requirements through detailed calculations rather than considering these requirements may be satisfied by extending the flexural tension reinforcements and tendons), to capture locations governed either by a change in section or a worst-case combination of shear, bending and torsion.

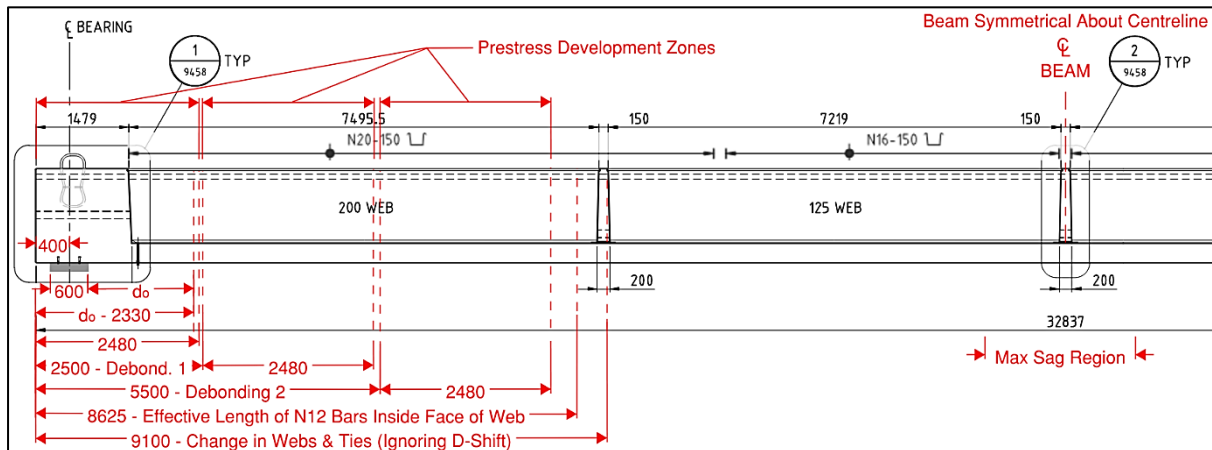
Conventional reinforcement was ignored within development zones. Development lengths of deformed bars at the ends of the beams were within d_o from the face of support. While the development length of the internal web face bars was calculated to be 348 mm and in a non-critical location.

Prestress losses were calculated in accordance with Clause 3.3.4 and Clause 3.4 of

AS 5100.5:2017. Effective prestress within development zones was determined using a linear approach that started at zero at the end of debonding to fully developed at a distance in accordance with Equation 13.3.2.2 of AS 5100.5:2017. Development zones of de-bonded strands were checked for any concrete tension from SLS loading (2Lp check) in accordance with Clause 13.3.2.2. The corresponding effective prestress was used at each increment to assess capacities against design actions.

The critical locations along the beams marked by changes in cross-sectional properties are shown in Figure C.4 below.

SPAN 1



SPAN 2

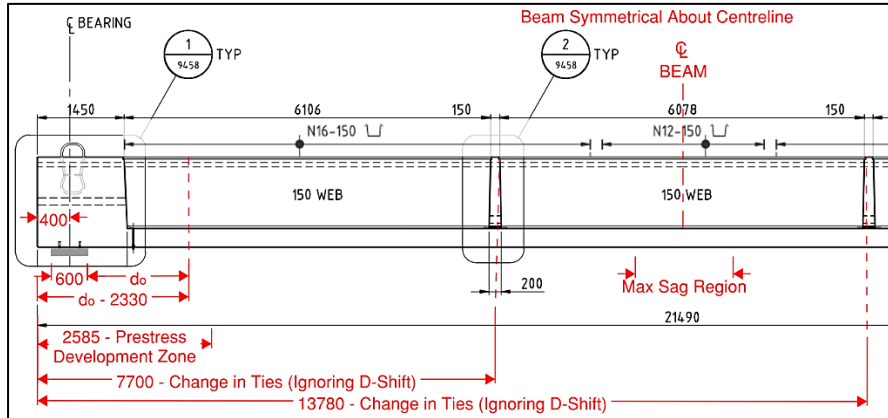


Figure C.4 Changes in Beam Section Properties (Some of the Critical Locations)

The prestress parameter f_{p0} outside the development length was taken as $0.7f_{pb}$ when calculating ϕV_{UC} , as per notes in Clause 8.2.4 of AS 5100.5:2017. Capacities were derived using the minimum flange width in each span, with the deck-slab portion transformed to effective width to account for the difference in concrete properties between the precast beam and the in-situ slab. In the derivation of the ULS bending capacity (ϕM_U) the 28-day concrete strength ratio was used, whilst for the SLS bending capacity (M_S) the ratio of the elastic moduli was used to determine the transformed deck-slab width. The difference in the methods accounts for concrete compression stress block approach for ULS, versus the linear stress-strain model for SLS.

C.2.7 Modelling and Assumptions

AutoCAD was used to draw the curves and skews of Bridge No. 1694 and the grillage was constructed using Structural Bridge Design (SBD) software. An ACES line-beam was used to check the sum of longitudinal member design actions.

The grillage type, aspect ratio, node locations and transverse member orientation were determined in line with Bridge Deck Behaviour (Hambly, 1991).

Grillage Details

Each beam was modelled by a longitudinal member using properties of the transformed beam-slab section. Transverse members were perpendicular to longitudinal members, to match the orientation of deck reinforcement. Additional nodes were placed at the mid-point of transverse slab members to better capture wheel loads and provide preliminary transverse member design action outputs. Refer Figure C.5 and Figure C.6 for grillage setup and plan view.

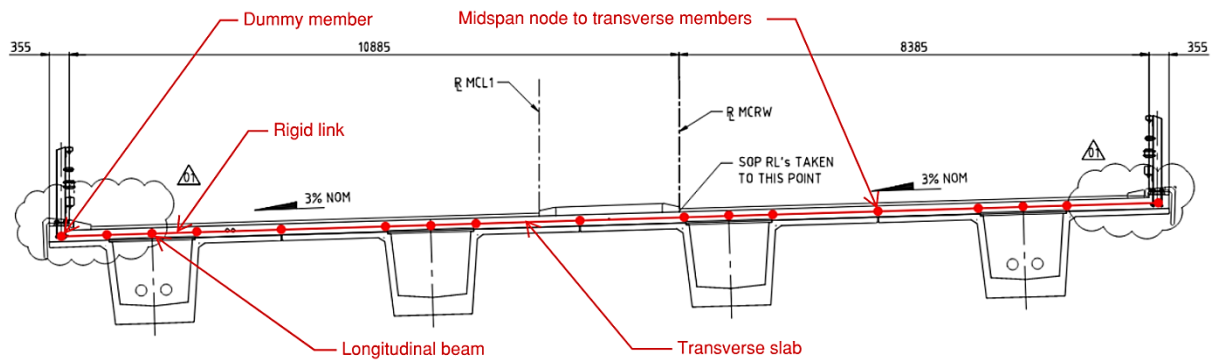


Figure C.5 2D Grillage Setup

Grillage

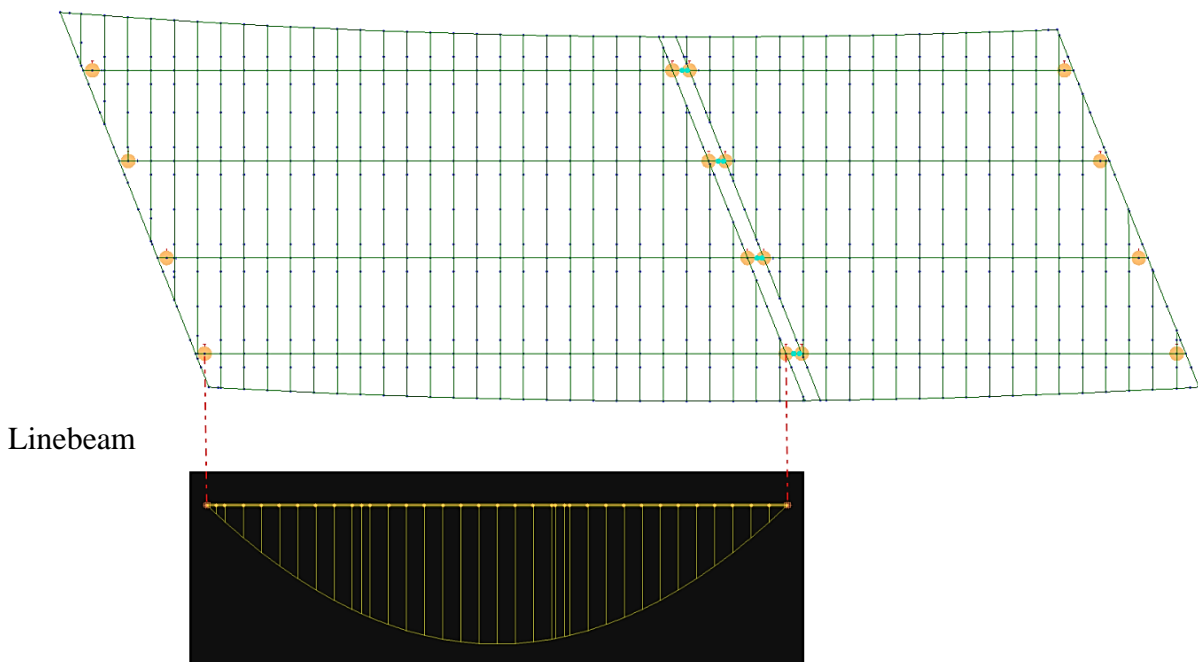


Figure C.6 Bridge Grillage and Line Beam Models

Longitudinal edge dummy members were coincident with the edge of the external beams, which was an approximate centroid to the combined upstand, barrier and overhanging fascia panels. Rigid links were at right angles to the longitudinal beams, extending to the web centrelines at the height of the centroid of the composite section. Transverse deck-slab members connected rigid links of adjacent tee-roff beams.

Longitudinal member ends were released over the piers to allow rotation of the beams, modelling a cracked link slab.

For transverse slab analysis, 3 No. evenly spaced longitudinal dummy members were introduced between tee-roffs. The additional members, and subsequent nodes, provided better local distribution and ‘smoother’ design action diagrams.

Member Properties

The longitudinal member properties of the Bridge No. 1694 tee-roffs were calculated for each grillage element. The torsional stiffness was calculated as per the method outlined in Bridge Deck Behaviour (Hambly, 1991). The torsional stiffness of all members was further factored by 0.2 as per AS 5100.5:2017 and with reference to Structures Engineering Design Manual (3912/03). The reduced torsional stiffness was applied for ULS analysis, as the torsional cracking moment capacity was exceeded.

Transverse slab members adopted the properties of the deck slab alone for conservative longitudinal analysis. Transverse assessment adopted the properties of 200 mm deck slab for mid-span bending and 300 mm combined deck and flange for bending and shear elsewhere.

Dummy members were assigned a low nominal stiffness to prevent computational error. Infinitely rigid pinned supports were conservatively used in the load rating assessment.

Permanent Effects

Bridge No. 1694 permanent effects considered only DL and SDL, without temperature and differential settlement, due to the simply supported spans.

Dead loads included self-weight of the tee-roff beams with the minimum 200 mm slab thickness plus an additional 50 mm allowance throughout for beam hog, which were multiplied by a factor of 1.2 for ULS in accordance with Table 6.2 in AS 5100.2:2017.

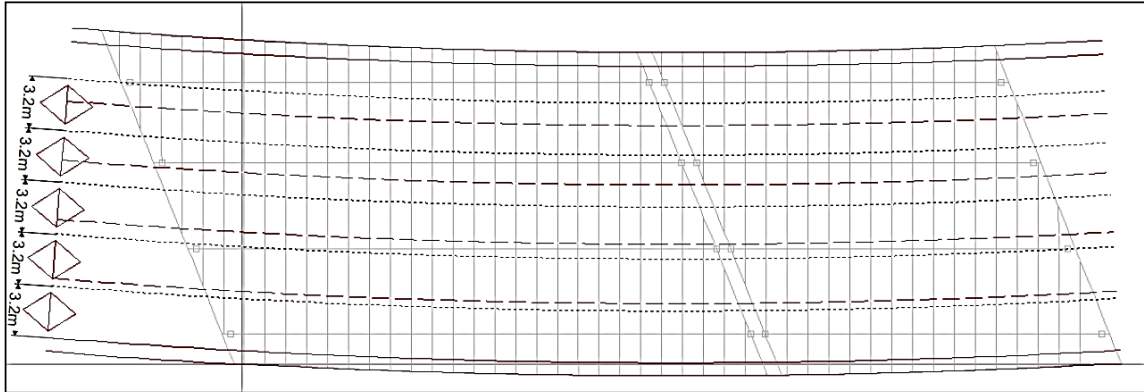
SDLs included 100 mm thick asphalt between kerbs, kerbs and guardrails, and were multiplied by a factor of 1.4 for ULS in accordance with Table 6.3 Item (b) in AS 5100.2:2017, as these are controlled by the relevant authority.

Vehicles

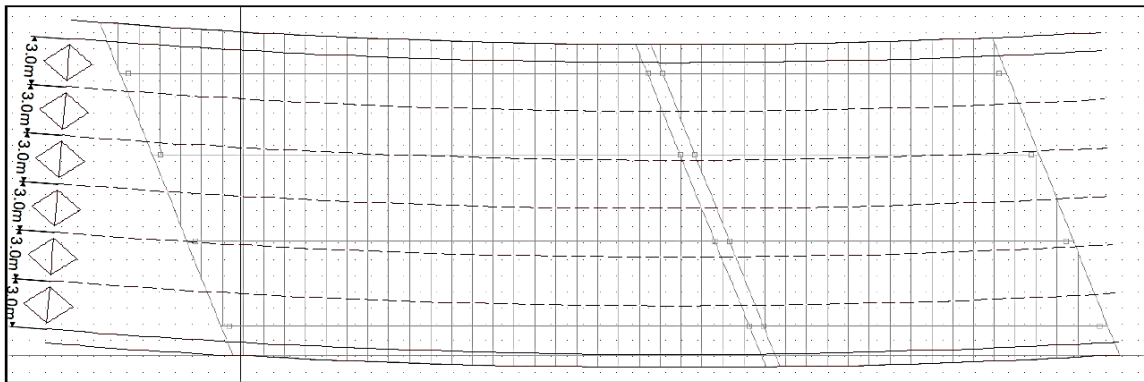
Bridge No. 1694 load rating included SM1600, T44, HLP, Group 1 and Group 2 vehicles. Design lanes were offset by the edge-kerb width for SM1600, T44 and Group 1 vehicles. HLP and Group 2 vehicle lanes were positioned considering movements with and without (a) the 2.5m median kerb; and (b) co-existing effects (CE) of 50% SM1600 in the opposite carriageway.

The movement of Group 2 Vehicle 8 was limited in the 8.0 m wide carriageway to within 0.2 m of the kerbs. Refer Figure C.7 for design lanes positions in the SBD model. All vehicles were assessed to travel in both directions.

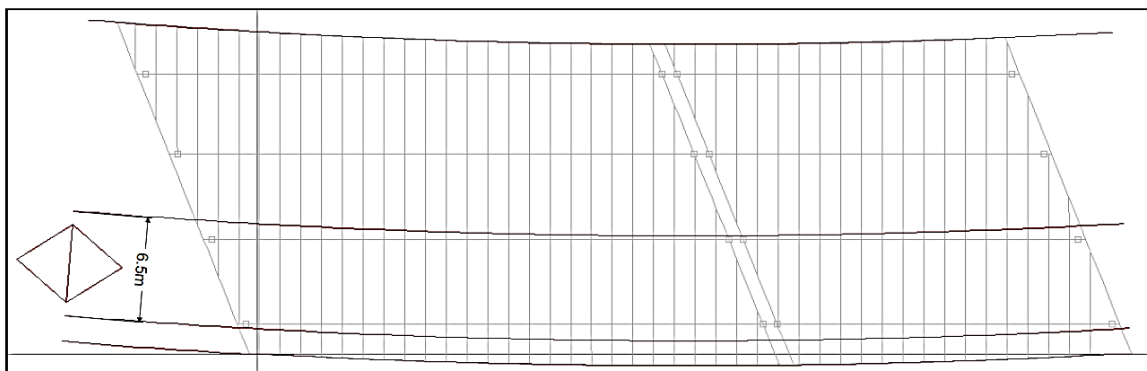
SM1600 Design Lanes



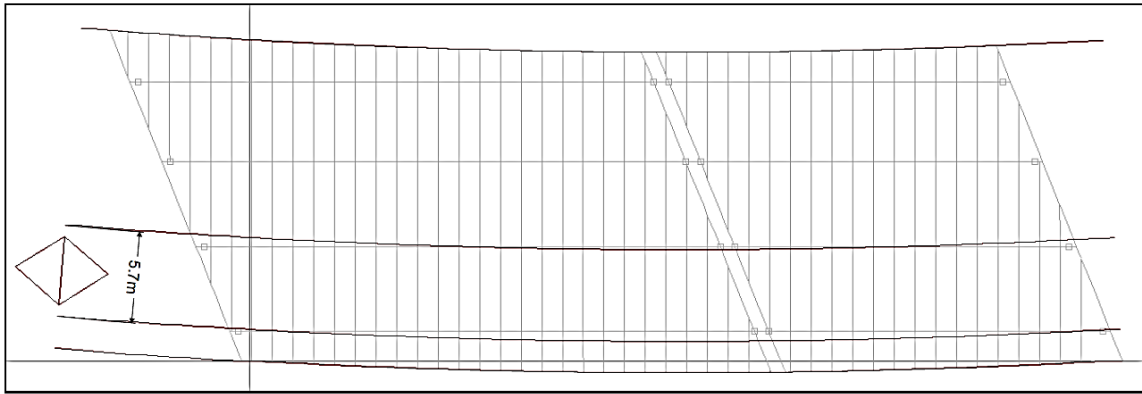
T44 Design Lanes



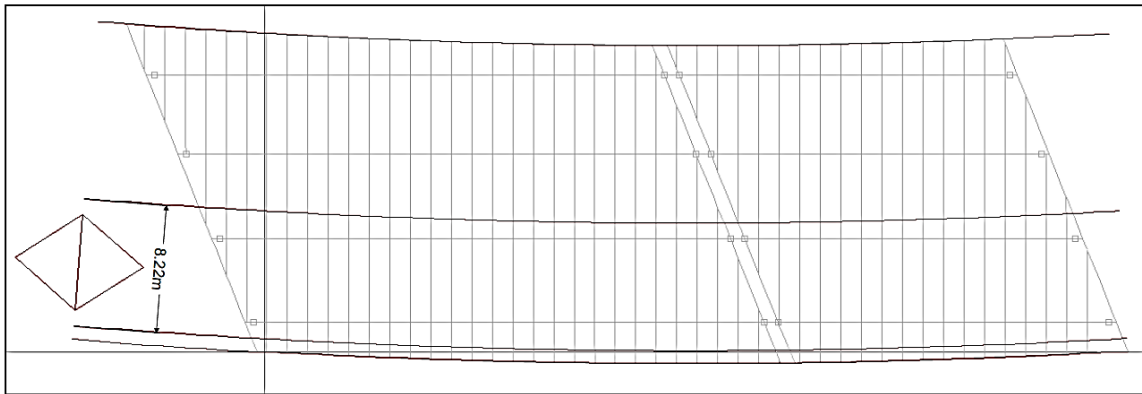
HLP400 Movement



Group 2 – 3.7 m Movement



Group 2 Vehicle 8 Movement



50% SM1600 Lanes in Opposite Carriageway

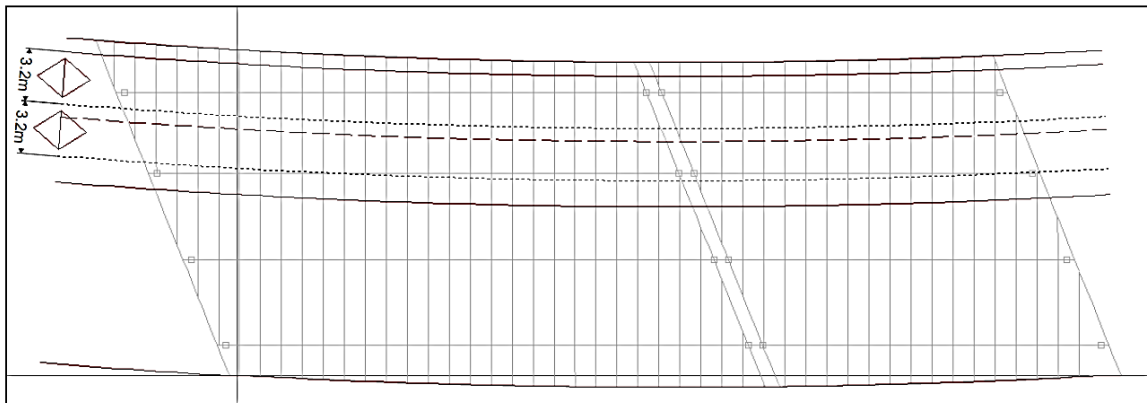


Figure C.7 Some of the Vehicle Lanes

Analysis

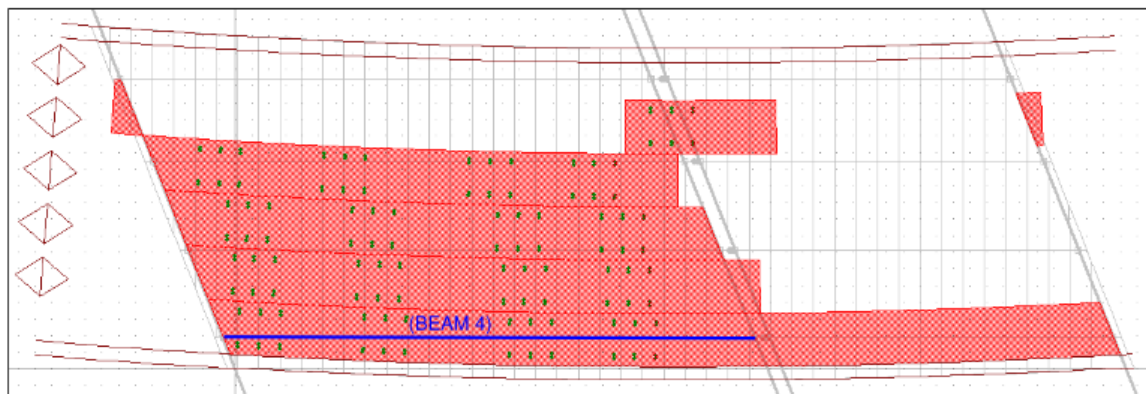
Longitudinal movement of the vehicles on Bridge No. 1694 grillage was refined to 0.1 m increments. Transverse movements were also refined to 0.1 m increments for HLP and Group 2 vehicles within the ± 1.0 m offset from centreline of carriageway.

The critical number of lanes was derived separately for SM1600, T44 and Group 1 vehicles for each of the 3No. cases:

- Maximum Bending (+ve) – simply supported spans
- Maximum Shear (+/-ve)
- Maximum Torsion (+/-ve)

Refer Figure C.8 for governing number of lanes for SM1600 critical bending and shear cases.

SM1600 – Span 1 Sag (External Beam)



SM1600 – Span 1 Shear AT 8.68m from Abutment 1 Centreline (External Beam)

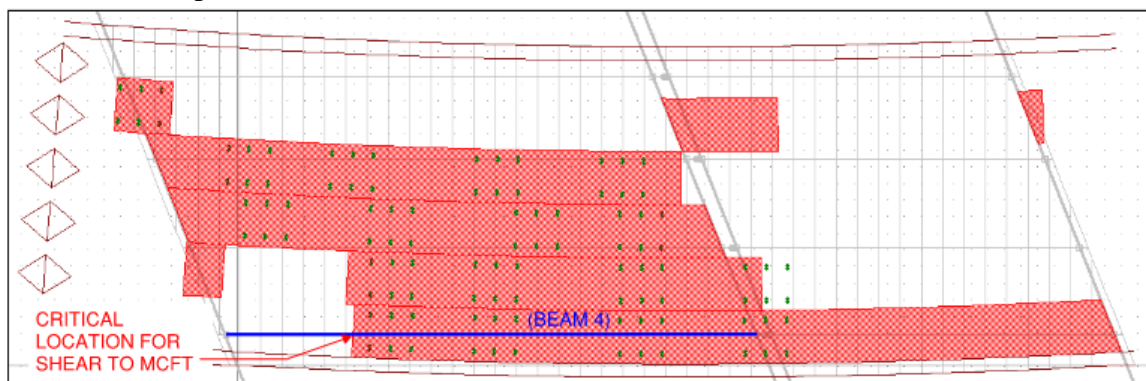


Figure C.8 SM1600 Patterned Loading for Critical Bending and Shear of Beam 4

Grillage Results

Positive and negative shear and torsion envelopes accounted for worst-case results at both ends of the beam. The direction of shear and torsion were recorded prior to combining with PE and CE effects. The maximum torsion case did not govern for any vehicles for Bridge No. 1694.

The output results of the critical combinations were visually cross-checked against diagrammatic grillage results in SBD. HLP and the longer Group 2 vehicles were checked by manual adjustment for critical loading on the curve.

Retaining the 2.5 m wide median kerb for HLP and Group 2 vehicles resulted in the highest design actions on the external beams. The median kerb offset the CE loading in the opposite carriageway further away from the critical edge beam in both spans, but still had a minor impact on the critical Span 1 edge beam. While the higher stiffness of shorter Span 2 prevented CE loads from reaching the external beam on the opposite side of the bridge.

Output Data

Beam PE data, as well as LL and CE data for the 3 No. cases (maximum bending, maximum shear and maximum torsion) were output with corresponding design actions. Shear values were averaged, and all output data was refined to 0.1 m increments using linear interpolation.

C.2.8 Load Rating Results

The load rating was checked for each 0.1 m increment using in-house software, for each of the 3No. cases (maximum bending, maximum shear and maximum torsion) and for each of the checks M1-M4 and V1-V5. The critical section for each vehicle was checked with an Excel spreadsheet to confirm the ratings for both bending and shear.

Longitudinal Actions

The longitudinal bending and longitudinal shear load rating factors for Span 1 are shown in Table C.2 and for Span 2 are shown in Table C.3.

Table C.2 Bridge 1694 Span 1 Load Rating Factors (Longitudinal)

Load Rating Factors - Span 1										
Vehicle	Factor	k _{M1}	k _{M2}	k _{M3}	k _{M4}	k _{V1}	k _{V2}	k _{V3}	k _{V4}	k _{V5}
	Distance from Abut. 1 CL (m)	d _{M1}	d _{M2}	d _{M3}	d _{M4}	d _{V1}	d _{V2}	d _{V3}	d _{V4}	d _{V5}
SM1600	M	1.03	0.98	1.03	1.45	1.44	1.21	NA	NA	1.16
		17.46	16.96	17.46	17.46	8.68	2.19	NA	NA	8.68
	V	NA	NA	NA	NA	1.32	1.08	1.30	1.47	1.12
		NA	NA	NA	NA	8.68	1.93	12.37	12.37	8.68
	T	NA	NA	NA	NA	2.05	1.33	1.53	1.64	3.85
	NA	NA	NA	NA	29.72	1.93	14.96	14.96	8.68	
T44	M	2.05	1.92	2.05	3.22	2.93	2.59	NA	NA	2.77
		16.26	16.16	16.26	16.26	29.72	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	2.37	2.03	2.16	2.26	2.03
		NA	NA	NA	NA	23.24	8.68	16.26	16.26	8.68
	T	NA	NA	NA	NA	3.76	2.48	3.14	3.62	5.51
	NA	NA	NA	NA	8.68	8.68	12.37	12.37	8.68	
HLP 320	M	1.11	1.04	1.11	1.35	1.64	1.17	NA	NA	1.19
		16.26	14.96	16.26	16.26	8.68	2.19	NA	NA	8.68
	V	NA	NA	NA	NA	1.62	1.13	1.63	1.98	1.29
		NA	NA	NA	NA	1.93	2.19	11.07	11.07	8.68
	T	NA	NA	NA	NA	1.66	1.24	1.04	1.12	3.21
	NA	NA	NA	NA	8.68	2.19	14.86	14.86	8.68	
HLP 400	M	0.95	0.89	0.95	1.15	1.40	1.04	NA	NA	1.04
		16.26	16.16	16.26	16.26	8.68	2.19	NA	NA	8.68
	V	NA	NA	NA	NA	1.40	1.01	1.39	1.68	1.11
		NA	NA	NA	NA	1.93	2.19	11.07	11.07	8.68
	T	NA	NA	NA	NA	1.41	1.14	0.89	0.96	2.70
	NA	NA	NA	NA	8.68	30.22	14.86	14.86	8.68	
GROUP 1, VEHICLE 1	M	3.26	3.06	3.26	5.12	4.53	4.43	NA	NA	3.90
		14.96	14.96	14.96	14.96	8.68	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	3.79	3.08	3.63	4.15	3.17
		NA	NA	NA	NA	8.68	8.68	12.37	12.37	8.68
	T	NA	NA	NA	NA	6.98	4.48	3.58	3.87	17.55
	NA	NA	NA	NA	8.68	8.68	16.26	16.26	12.37	
GROUP 1, VEHICLE 2	M	2.22	2.08	2.22	3.49	3.11	2.98	NA	NA	2.70
		14.96	14.96	14.96	16.16	8.68	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	2.71	2.26	2.68	3.03	2.28
		NA	NA	NA	NA	8.68	8.68	20.05	20.05	8.68
	T	NA	NA	NA	NA	4.09	3.00	2.28	2.47	8.11
	NA	NA	NA	NA	11.17	8.68	16.16	16.16	11.37	

Notes:

Red values represent governing factors for each case (M, V and T).

* This 98% rating has resulted as σ_{pu} has been used for all calculations as per AS 5100.5:2017 Clause 8.1.7 in lieu of a non-linear stress-strain curve for the strand. This methodology has been adopted to present generalised load rating results when appropriate test data is not available and approved by MRWA prior to the final design. The load rating using stress-strain tendon test data is 100%.

Load Rating Factors Continued - Span 1										
Vehicle	Factor	k _{M1}	k _{M2}	k _{M3}	k _{M4}	k _{V1}	k _{V2}	k _{V3}	k _{V4}	k _{V5}
	Distance from Abut. 1 CL (m)	d _{M1}	d _{M2}	d _{M3}	d _{M4}	d _{V1}	d _{V2}	d _{V3}	d _{V4}	d _{V5}
GROUP 1, VEHICLE 3	M	2.01	1.88	2.01	3.16	3.89	3.87	NA	NA	2.43
		14.96	14.96	14.96	14.96	11.17	8.68	NA	NA	8.68
	V	NA	NA	NA	NA	2.54	2.13	2.31	2.62	1.94
		NA	NA	NA	NA	30.22	30.22	20.15	20.15	8.68
	T	NA	NA	NA	NA	4.04	2.60	2.15	2.30	7.58
	NA	NA	NA	NA	8.68	8.68	16.26	16.26	11.37	
GROUP 1, VEHICLE 4	M	2.07	1.94	2.07	3.25	2.94	2.63	NA	NA	2.55
		14.96	14.96	14.96	14.96	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	2.50	2.01	2.49	2.96	2.08
		NA	NA	NA	NA	8.68	8.68	11.07	11.07	8.68
	T	NA	NA	NA	NA	4.00	2.62	2.16	2.32	6.15
	NA	NA	NA	NA	8.68	8.68	14.86	14.86	8.68	
GROUP 2, VEHICLE 1 - 3.01	M	2.93	2.75	2.93	3.45	4.07	3.66	NA	NA	3.46
		17.46	14.96	17.46	16.26	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	3.43	3.30	3.39	3.91	3.08
		NA	NA	NA	NA	23.24	8.68	20.05	20.05	8.68
	T	NA	NA	NA	NA	4.98	4.43	4.31	4.63	8.37
	NA	NA	NA	NA	27.73	23.24	14.96	14.96	23.24	
GROUP 2, VEHICLE 1 - 3.70	M	2.94	2.73	2.94	3.46	4.09	3.56	NA	NA	3.42
		17.46	14.96	17.46	16.26	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	3.46	3.12	3.42	3.93	3.02
		NA	NA	NA	NA	23.24	8.68	20.05	20.05	8.68
	T	NA	NA	NA	NA	4.93	4.54	4.49	5.56	8.46
	NA	NA	NA	NA	26.53	23.24	26.53	26.53	23.14	
GROUP 2, VEHICLE 2 - 3.01	M	2.65	2.50	2.65	3.13	3.53	3.20	NA	NA	3.16
		17.56	14.86	17.56	17.56	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	2.98	2.97	2.94	3.39	2.71
		NA	NA	NA	NA	23.24	8.68	20.05	20.05	8.68
	T	NA	NA	NA	NA	4.49	4.04	3.99	4.18	7.73
	NA	NA	NA	NA	27.73	23.24	12.47	12.47	23.24	
GROUP 2, VEHICLE 2 - 3.70	M	2.72	2.56	2.72	3.21	3.66	3.28	NA	NA	3.29
		17.56	14.96	17.56	17.56	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	3.09	3.02	3.04	3.49	2.78
		NA	NA	NA	NA	23.24	8.68	20.05	20.05	8.68
	T	NA	NA	NA	NA	4.64	4.08	3.83	4.03	7.43
	NA	NA	NA	NA	27.73	23.24	12.47	12.47	23.24	

Notes: Red values represent governing factors for each case (M, V and T).

Load Rating Factors Continued - Span 1										
Vehicle	Factor	k _{M1}	k _{M2}	k _{M3}	k _{M4}	k _{V1}	k _{V2}	k _{V3}	k _{V4}	k _{V5}
	Distance from Abut. 1 CL (m)	d _{M1}	d _{M2}	d _{M3}	d _{M4}	d _{V1}	d _{V2}	d _{V3}	d _{V4}	d _{V5}
GROUP 2, VEHICLE 4	M	2.01	1.91	2.01	2.37	2.81	2.46	NA	NA	2.42
		17.46	16.26	17.46	16.26	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	2.53	2.27	2.50	2.87	2.23
		NA	NA	NA	NA	23.24	1.93	20.05	20.05	8.68
	T	NA	NA	NA	NA	3.42	2.88	2.98	3.23	4.07
	NA	NA	NA	NA	27.83	30.22	16.26	16.26	30.22	
GROUP 2, VEHICLE 4 - NS	M	1.70	1.61	1.70	2.00	2.37	2.08	NA	NA	2.05
		17.46	16.26	17.46	16.26	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	2.14	1.92	2.12	2.43	1.89
		NA	NA	NA	NA	23.24	1.93	20.05	20.05	8.68
	T	NA	NA	NA	NA	2.89	2.44	2.53	2.73	3.44
	NA	NA	NA	NA	27.83	30.22	16.26	16.26	30.22	
GROUP 2, VEHICLE 5	M	1.51	1.43	1.51	1.78	2.17	1.96	NA	NA	1.83
		16.26	16.16	16.26	16.26	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	1.96	1.87	1.93	2.22	1.74
		NA	NA	NA	NA	23.24	8.68	20.05	20.05	8.68
	T	NA	NA	NA	NA	2.59	2.28	2.45	2.66	5.59
	NA	NA	NA	NA	27.83	30.22	14.96	14.96	21.35	
GROUP 2, VEHICLE 5 - NS	M	1.28	1.21	1.28	1.51	1.84	1.66	NA	NA	1.55
		16.26	16.16	16.26	16.26	30.22	30.22	NA	NA	8.68
	V	NA	NA	NA	NA	1.66	1.58	1.63	1.88	1.47
		NA	NA	NA	NA	23.24	8.68	20.05	20.05	8.68
	T	NA	NA	NA	NA	2.19	1.93	2.07	2.25	4.73
	NA	NA	NA	NA	27.83	30.22	14.96	14.96	21.35	
GROUP 2, VEHICLE 7	M	0.94	0.88	0.94	1.11	1.36	1.15	NA	NA	1.09
		16.26	16.16	16.26	16.26	8.68	2.19	NA	NA	8.68
	V	NA	NA	NA	NA	1.33	1.05	1.34	1.58	1.13
		NA	NA	NA	NA	23.24	1.93	21.35	21.35	8.68
	T	NA	NA	NA	NA	1.49	1.24	1.28	1.37	1.73
	NA	NA	NA	NA	30.22	30.22	16.16	16.16	30.22	
GROUP 2, VEHICLE 8	M	0.75	0.70	0.75	0.88	1.09	0.94	NA	NA	0.88
		16.26	16.16	16.26	16.26	8.68	2.19	NA	NA	8.68
	V	NA	NA	NA	NA	1.06	0.85	1.06	1.24	0.90
		NA	NA	NA	NA	23.24	1.93	21.35	21.35	8.68
	T	NA	NA	NA	NA	1.23	1.02	0.95	1.00	1.42
	NA	NA	NA	NA	30.22	30.22	15.36	15.36	30.22	

Notes: Red values represent governing factors for each case (M, V and T).

Table C.3 Bridge 1694 Span 2 Load Rating Factors (Longitudinal)

Load Rating Factors - Span 2										
Vehicle	Factor	k _{M1}	k _{M2}	k _{M3}	k _{M4}	k _{V1}	k _{V2}	k _{V3}	k _{V4}	k _{V5}
	Distance from Abut. 1 CL (m)	d _{M1}	d _{M2}	d _{M3}	d _{M4}	d _{V1}	d _{V2}	d _{V3}	d _{V4}	d _{V5}
SM1600	M	1.03	1.03	1.03	1.44	1.47	1.51	NA	NA	1.47
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	1.26	1.41	1.15	1.37	1.23
		NA	NA	NA	NA	13.30	1.93	12.80	12.80	13.30
	T	NA	NA	NA	NA	3.20	4.04	2.37	2.68	6.82
		NA	NA	NA	NA	14.10	1.93	14.10	14.10	14.10
T44	M	1.57	1.57	1.57	2.44	2.39	2.56	NA	NA	2.19
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	3.50
	V	NA	NA	NA	NA	1.77	2.41	1.62	1.95	1.75
		NA	NA	NA	NA	13.30	1.93	12.80	12.80	13.30
	T	NA	NA	NA	NA	3.75	4.93	2.95	3.38	6.91
		NA	NA	NA	NA	15.30	1.93	14.10	14.10	15.30
HLP 320	M	1.16	1.16	1.16	1.36	1.83	1.99	NA	NA	1.88
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	1.05	3.25	1.57	1.96	1.20
		NA	NA	NA	NA	1.93	3.80	13.30	13.30	1.93
	T	NA	NA	NA	NA	2.69	2.25	2.45	3.18	5.82
		NA	NA	NA	NA	13.30	18.89	12.80	12.80	13.30
HLP 400	M	1.01	1.01	1.01	1.19	1.59	1.72	NA	NA	1.63
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	1.55	2.80	1.36	1.69	1.58
		NA	NA	NA	NA	1.93	3.70	13.30	13.30	1.93
	T	NA	NA	NA	NA	1.91	1.75	1.75	2.26	4.10
		NA	NA	NA	NA	13.30	18.89	13.30	13.30	13.30
GROUP 1, VEHICLE 1	M	2.85	2.85	2.85	4.43	4.11	4.49	NA	NA	3.83
		9.10	9.10	9.10	9.10	1.93	1.93	NA	NA	3.90
	V	NA	NA	NA	NA	3.29	3.98	3.04	3.66	3.21
		NA	NA	NA	NA	13.30	1.93	12.80	12.80	13.30
	T	NA	NA	NA	NA	5.70	11.77	4.29	4.54	11.88
		NA	NA	NA	NA	13.30	1.93	12.80	12.80	15.30
GROUP 1, VEHICLE 2	M	2.13	2.13	2.13	3.31	2.93	3.12	NA	NA	2.95
		9.00	9.10	9.00	9.00	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	2.79	2.84	2.40	2.97	2.87
		NA	NA	NA	NA	1.93	1.93	13.30	13.30	1.93
	T	NA	NA	NA	NA	4.71	7.60	2.73	2.80	5.19
		NA	NA	NA	NA	18.89	1.93	6.40	6.40	18.89

Notes: Red values represent governing factors for each case (M, V and T).

Load Rating Factors Continued - Span 2										
Vehicle	Factor	k _{M1}	k _{M2}	k _{M3}	k _{M4}	k _{V1}	k _{V2}	k _{V3}	k _{V4}	k _{V5}
	Distance from Abut. 1 CL (m)	d _{M1}	d _{M2}	d _{M3}	d _{M4}	d _{V1}	d _{V2}	d _{V3}	d _{V4}	d _{V5}
GROUP 1, VEHICLE 3	M	1.91	1.91	1.91	2.96	2.50	2.68	NA	NA	2.52
		9.00	9.10	9.00	9.00	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	2.16	2.60	2.00	2.48	2.12
		NA	NA	NA	NA	13.30	1.93	13.30	13.30	13.30
	T	NA	NA	NA	NA	3.97	4.63	2.24	2.32	4.87
	NA	NA	NA	NA	7.60	1.93	7.70	7.70	18.89	
GROUP 1, VEHICLE 4	M	2.04	2.04	2.04	3.18	2.74	2.96	NA	NA	2.77
		9.00	9.10	9.00	9.00	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	2.39	2.75	2.20	2.65	2.33
		NA	NA	NA	NA	13.30	1.93	12.80	12.80	13.30
	T	NA	NA	NA	NA	4.30	7.68	3.17	3.17	10.38
	NA	NA	NA	NA	13.30	1.93	9.00	9.00	13.30	
GROUP 2, VEHICLE 1 - 3.01	M	2.72	2.72	2.72	3.17	3.74	3.65	NA	NA	3.62
		9.00	9.00	9.00	9.00	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	3.24	3.38	3.04	3.88	2.80
		NA	NA	NA	NA	13.30	1.93	13.30	13.30	13.30
	T	NA	NA	NA	NA	4.76	4.20	3.63	3.91	9.81
	NA	NA	NA	NA	1.93	1.93	9.40	9.40	13.30	
GROUP 2, VEHICLE 1 - 3.70	M	2.72	2.72	2.72	3.17	3.77	3.77	NA	NA	3.70
		9.00	9.00	9.00	9.00	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	3.27	3.54	3.08	3.86	3.08
		NA	NA	NA	NA	13.30	1.93	13.30	13.30	12.80
	T	NA	NA	NA	NA	4.66	4.74	3.73	4.12	10.38
	NA	NA	NA	NA	12.80	1.93	11.50	11.50	13.30	
GROUP 2, VEHICLE 2 - 3.01	M	2.40	2.40	2.40	2.80	3.25	3.15	NA	NA	3.14
		9.10	9.10	9.10	9.10	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	2.74	3.00	2.58	3.28	2.39
		NA	NA	NA	NA	13.30	1.93	13.30	13.30	13.30
	T	NA	NA	NA	NA	3.46	4.03	3.01	3.36	7.44
	NA	NA	NA	NA	13.30	1.93	11.50	11.50	13.30	
GROUP 2, VEHICLE 2 - 3.70	M	2.50	2.50	2.50	2.91	3.36	3.29	NA	NA	3.29
		9.10	9.10	9.10	9.10	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	2.86	3.20	2.68	3.39	2.51
		NA	NA	NA	NA	13.30	1.93	13.30	13.30	13.30
	T	NA	NA	NA	NA	3.64	4.73	3.22	3.62	7.83
	NA	NA	NA	NA	13.30	1.93	11.50	11.50	13.30	

Notes: Red values represent governing factors for each case (M, V and T).

Load Rating Factors Continued - Span 2										
Vehicle	Factor	k _{M1}	k _{M2}	k _{M3}	k _{M4}	k _{V1}	k _{V2}	k _{V3}	k _{V4}	k _{V5}
	Distance from Abut. 1 CL (m)	d _{M1}	d _{M2}	d _{M3}	d _{M4}	d _{V1}	d _{V2}	d _{V3}	d _{V4}	d _{V5}
GROUP 2, VEHICLE 4	M	1.74	1.74	1.74	2.03	2.68	2.67	NA	NA	2.66
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	2.34	2.49	2.19	2.73	2.31
		NA	NA	NA	NA	13.30	1.93	13.30	13.30	12.30
	T	NA	NA	NA	NA	4.38	3.89	3.10	3.10	10.90
	NA	NA	NA	NA	18.89	1.93	10.20	10.20	13.30	
GROUP 2, VEHICLE 4 - NS	M	1.47	1.47	1.47	1.72	2.27	2.26	NA	NA	2.25
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	1.98	2.11	1.85	2.31	1.96
		NA	NA	NA	NA	13.30	1.93	13.30	13.30	12.30
	T	NA	NA	NA	NA	3.71	3.29	2.62	2.62	9.22
	NA	NA	NA	NA	18.89	1.93	10.20	10.20	13.30	
GROUP 2, VEHICLE 5	M	1.33	1.33	1.33	1.55	2.02	1.96	NA	NA	1.98
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	2.02	1.93	1.79	2.28	1.64
		NA	NA	NA	NA	1.93	1.93	13.30	13.30	13.30
	T	NA	NA	NA	NA	2.84	2.47	1.91	1.91	7.63
	NA	NA	NA	NA	1.93	1.93	11.40	11.40	13.30	
GROUP 2, VEHICLE 5 - NS	M	1.12	1.12	1.12	1.31	1.71	1.66	NA	NA	1.68
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	1.71	1.63	1.51	1.93	1.39
		NA	NA	NA	NA	1.93	1.93	13.30	13.30	13.30
	T	NA	NA	NA	NA	2.40	2.09	1.62	1.62	6.46
	NA	NA	NA	NA	1.93	1.93	11.40	11.40	13.30	
GROUP 2, VEHICLE 7	M	0.93	0.93	0.93	1.09	1.43	1.50	NA	NA	1.45
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	1.44	1.46	1.28	1.59	1.47
		NA	NA	NA	NA	1.93	1.93	13.30	13.30	1.93
	T	NA	NA	NA	NA	2.32	2.17	1.61	1.61	6.39
	NA	NA	NA	NA	1.93	1.93	10.40	10.40	13.30	
GROUP 2, VEHICLE 8	M	0.76	0.76	0.76	0.88	1.16	1.22	NA	NA	1.18
		10.30	10.30	10.30	10.30	1.93	1.93	NA	NA	1.93
	V	NA	NA	NA	NA	1.17	1.19	1.04	1.29	1.20
		NA	NA	NA	NA	1.93	1.93	13.30	13.30	1.93
	T	NA	NA	NA	NA	1.62	1.53	1.05	1.05	4.32
	NA	NA	NA	NA	1.93	1.93	10.20	10.20	13.30	

Notes: Red values represent governing factors for each case (M, V and T).

C.2.9 Other Superstructure Checks

Interface Shear

Interface shear between deck slab and tee-roff beams was checked for both longitudinal and transverse design shear actions in accordance with Clause 8.4 in AS 5100.5:2017 and was found not to govern the load ratings. The anchored N12-150 U bars in the flanges were used in the transverse interface shear assessment. The N12-150 U bars were used together with the shear/torsion reinforcement in the longitudinal interface shear assessment. Group 2 Vehicle 8 governed both longitudinal and transverse design actions. The interface shear results are shown in the following Table C.4.

Table C.4 Interface Shear for Group 2 Vehicle 8 (as per AS 5100.5:2017)

Interface Shear - Longitudinal	Symbol	PE+CE	LL	Units
ULS Design Shear	V^*	1346	2884	kN
Shear Flow	q^*	544	1165	kN/m
Capacity	q_{ALLOW}	4541		kN/m
Load Rating	%LR	343%		%
Interface Shear - Transverse				
Symbol	Symbol	SDL+CE	LL	Units
ULS Design Shear	V^*	6	184	kN
Shear Flow	q^*	27	818	kN/m
Capacity	q_{ALLOW}	14565		kN/m
Load Rating	%LR	1778%		%

Transverse Bending & Shear

Bridge No. 1694 has sufficiently anchored interface shear reinforcement between the deck slab and tee-roff flange and therefore a 300 mm thick composite section was used in transverse hog bending and shear – refer Figure C.9 below. Critical hog bending was located where the flange meets the web of the beam.

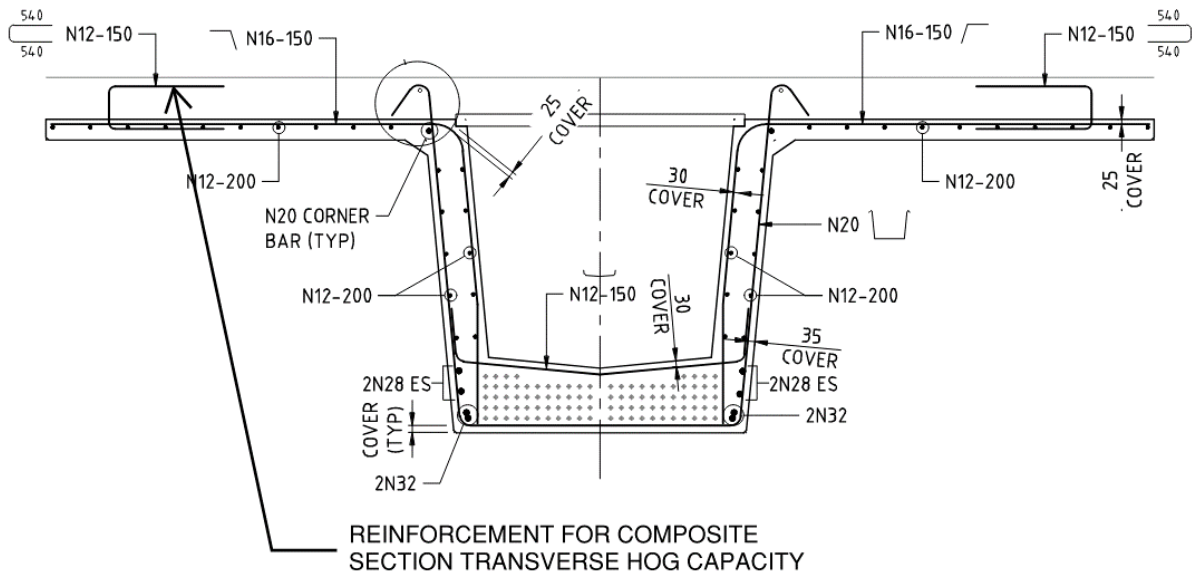


Figure C.9 Transverse Hog Reinforcement

For transverse sag bending check at mid-span between tee-rolfs, a 200 mm thick deck slab was used for capacity considering the discontinuity of adjacent flanges. This was the critical location for transverse checks, governed by Group 2 Vehicle 8. The results are shown in Table C.5.

Table C.5 Critical Transverse Check for Group 2 Vehicle 8 (as per AS 5100.5:2017)

Transverse Bending	Symbol	SDL	LL	Units
ULS Bending Moment	M^*	-6.6	177.6	kNm
Corresponding Shear	V_{CORR}	-0.3	40.2	kN
Total Force in Longitudinal Reinforcement	F_{td}	1627		kN
Total Available Force	F_{AVAIL}	1640		kN
Transverse Load Rating	%LR	101%		%
Longitudinal Load Rating (for Comparison)	%LR	72%		%

Note: PE effects were in the opposite direction at the critical location and therefore ignored.

Transverse bending and shear were checked in line with the MCFT approach considering shear and bending interaction, complying with AS 5100.5:2017. Transverse design actions were found not to govern the load ratings.

Compression Fan Regions

Locations within d_o from face of supports are reinforced with adequate shear reinforcement to transfer stresses via compression fan-shaped strut-and-tie action. These compression fan regions were checked using strut and tie modelling (shown in Figure C.10 below) and did not govern the load ratings.

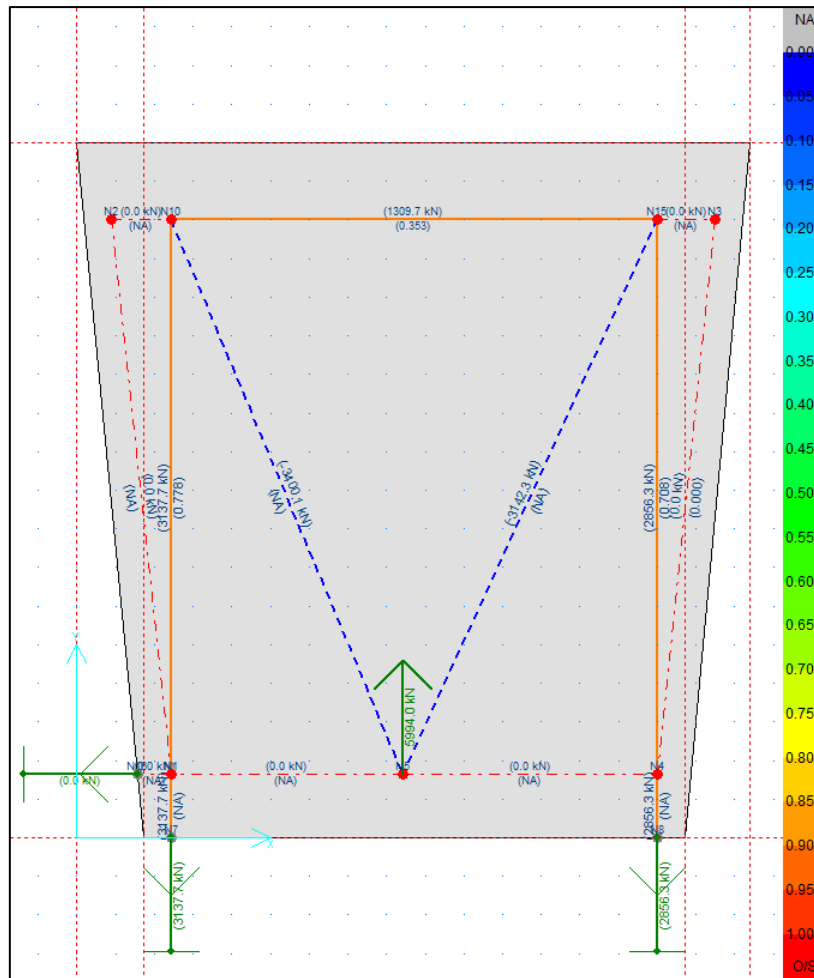


Figure C.10 End Diaphragm Strut & Tie Model

Bearing No. 3 was critical for maximum PE + SM1600 loading. The load rating is shown in Table C.6 below.

Table C.6 End Diaphragm Check (as per AS 5100.5:2017)

Pier Pilecap	Symbol	PE+LL	PE	LL	Units
ULS Bearing Load	N*	5994	1838	4156	kN
Vertical Reinforcement Utilisation		0.778	0.238	0.540	
Load Rating	%LR	141%			%

C.2.10 Detailed Substructure Checks

Note: Detailed substructure check reporting is optional when substructure rating is significantly higher than the superstructure load ratings. Example given here is only for demonstration purpose.

The bearings, capbeam, columns, footings and piles were checked and found not to govern the load ratings. Please note this section is only required when substructure rating governs for design vehicles, or the substructure rating is requested.

Bearings

Loads on the bearings with corresponding rotations were checked against AS 5100.4:2017. Maximum compressive stress in accordance with clause 12.6.2 controlled the bearings on span 1. The SM1600 loading results on bearing part No. 161212C are shown in Table C.7 below.

Table C.7 Load Rating Check of Elastomeric Bearings (as per AS 5100.4:2017)

Compressive Stress	Symbol	PE	LL	Units
SLS Vertical Bearing Load	N	1470	2309	kN
Bonded Area of Bearing	A_b	255176	255176	mm ²
Mean Compressive Stress	σ_{N/A_b}	5.761	9.049	MPa
Compressive Stress Limit	σ_{max}	15.00		MPa
Load Rating	%LR	102%		%
Shear Strain				
Symbol	PE	LL	Units	
Rotation - Longitudinal	α_a	0.00272	0.00428	Radians
Rotation - Transverse	α_b	0.00194	0.00306	Radians
Vector Sum	α	0.00335	0.00526	Radians
Compressive Strain	ϵ_c	0.011	0.017	
Shear Strain – Vertical	e_{sc}	0.761	1.196	
Shear Strain – Rotation	e_{sr}	0.290	0.456	
Shear Strain – Tangential	e_{sh}	0.000	0.239	
Shear Strain – Total	ϵ	1.052	1.891	
Shear Strain – Limit	ϵ_{max}	3.130		
Load Rating	%LR	110%		%

Abutment Capbeam & Columns

A global model was used to analyse the Abutments, shown in Figure C.11 below. Bursting stresses at bearing locations were also checked in accordance with the BBR Multi-wire System prestressing (and bearings) manual (BBR Australia Pty Ltd, 1973).

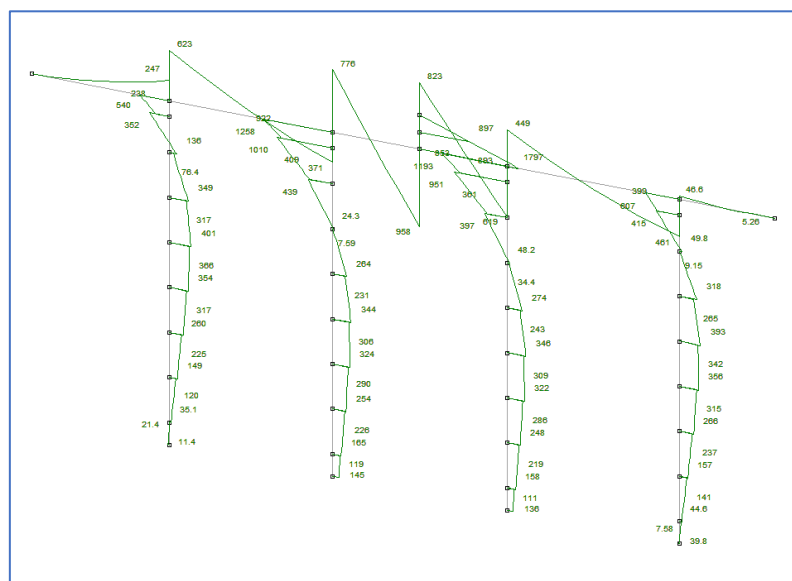


Figure C.11 Abutment 1 Capbeam & Columns with Lateral MSE Stiffnesses – EQ Transverse Moment Diagram (Note Shear Key Full Extent Between Columns 2 & 3)

ULS maximum PE and transverse EQ governed both the capbeam and column bending load ratings, while maximum PE and SM1600 governed the capbeam bursting and spalling ratings, which are summarised in Table C.8 below.

Table C.8 Load Rating of Abutment Capbeam and Columns (as per AS 5100.5:2017 and BBR Multi-wire System: Prestressing Manual 1973)

Capbeam Bending At Pile 1	Symbol	PE	EQ	Units
ULS Moment	$-M^*$	-49.5	-573.5	kNm
Corresponding Shear	V_{Corr}	46.2	188.8	kN
Corresponding Torsion	T_{Corr}	11.9	191.1	kNm
Load Rating	%LR	113%		%
Governing Check		M2		
Capbeam Bending At Pile 2 ($-M^*$ Check Adjacent Shear Key)				
Symbol	PE	EQ	Units	
ULS Moment	$-M^*$	-40.8	-546.6	kNm
ULS Bending Capacity	ϕM_u	-889.0		kNm
Load Rating	%LR	155%		%
Governing Check		M1		
Capbeam Bursting				
Symbol	PE	LL	Units	
ULS Bearing Load	N^*	1838	4156	kN
Tensile Capacity of Bars Provided (Each Direction)	ϕN	880		kN
Bursting Forces	T_b^*	259	586	kN
Load Rating	%LR	106%		%
Capbeam Spalling				
Symbol	PE	LL	Units	
ULS Bearing Loads	N^*	1838	4156	kN
Tensile Capacity of Top Longitudinal Bars Provided	ϕN	1488		kN
Spalling Forces	T_s^*	418	944	kN
Load Rating	%LR	113%		%
Columns – Biaxial Bending				
Symbol	PE	EQ	Units	
$-M^*_x$	$-M^*_x$	-14.0	-266.0	kNm
$-M^*_y$	$-M^*_y$	-83.9	-926.1	kNm
ϕM_{ux}	ϕM_{ux}	1604		kNm
ϕM_{uy}	ϕM_{uy}	1237		kNm
N^*	N_{Corr}	-1890	-371	kN
ϕN_{uo}	ϕN_{uo}	12870		kN
α_n	α_n	1.00		
Utilisation		0.077	0.915	
Load Rating	%LR	101%		%

Pad Footings

Bearing reactions from the superstructure grillage (shown in Figure C.12 below) and hand calculations were used to determine abutment pad footing bearing pressures. Bearing capacities are from Geotechnical Report 10-0107-030-BR-RP-0001-00.

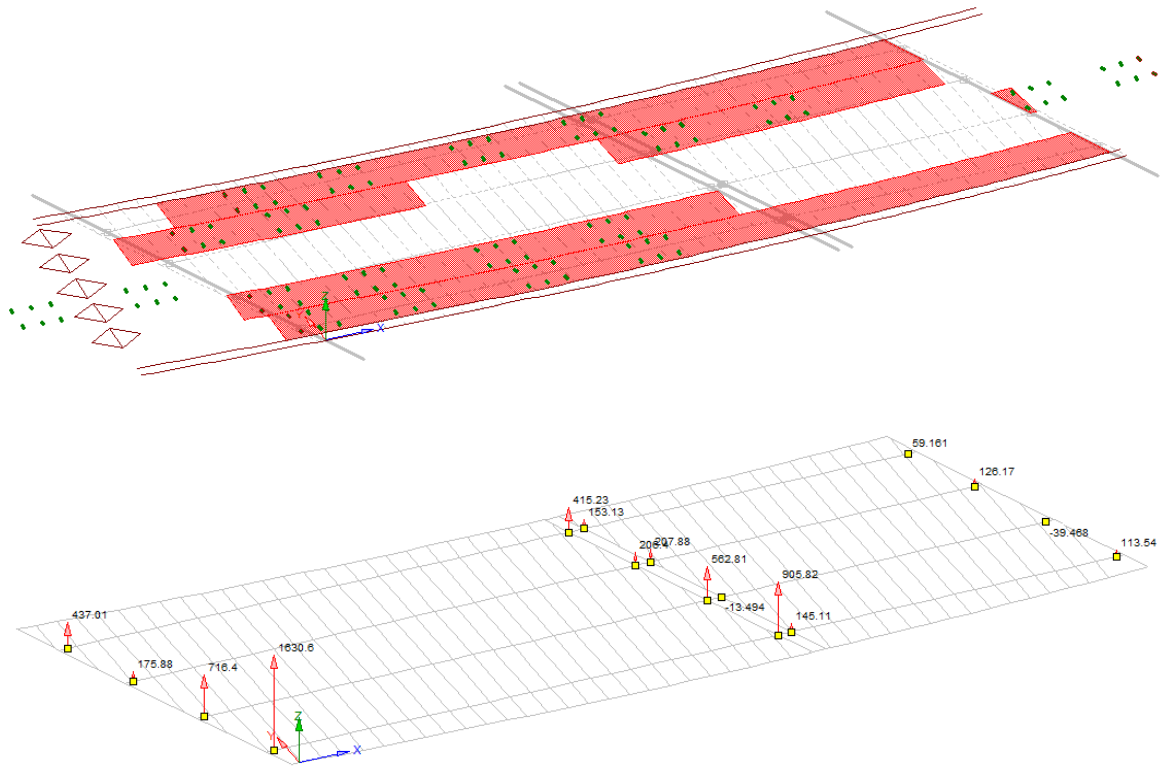


Figure C.12 SBD Model – SLS SM1600 Bearing Reactions for Pad Footing Bearing Check

SLS Abutment 1 footing pressures for SM1600 with transverse wind design actions were checked against acceptable settlements provided in Geotechnical Report 10-0107-030-BR-RP-0001-00. ULS pressures were also checked against ultimate bearing capacity for the SM1600 transverse bending case, however, maximum PE and longitudinal EQ case governed the ULS rating. ULS bearing capacities were derived with the Meyerhof method using soil parameters from the geotechnical report. The load ratings are shown in Table C.9 below.

Table C.9 Critical Pad Footing Bearing Check for Abutment 1 (as per AS 5100.5:2017)

Abutment 1 Pad Footing Bearing - SLS	Symbol	PE	LL	0.7*Wind	Units
Bearing 1 Reaction	N ₁	-	437	-	kN
Bearing 2 Reaction	N ₂	-	176	-	kN
Bearing 3 Reaction	N ₃	-	716	-	kN
Bearing 4 Reaction	N ₄	-	1631	-	kN
Total Vertical Force	N _{SLS}	23733	2960	0	kN
Transverse Force	F _{T,SLS}	0	0	18	kN
Longitudinal Force	F _{L,SLS}	0	180	0	kN
Transverse Moment	M _{T,SLS}	233	11847	153	kNm
Longitudinal Moment	M _{L,SLS}	7080			kNm
H/V Ratio		0.007			
Transverse Eccentricity	e _T	0.458			m
Longitudinal Eccentricity	e _L	0.265			m
Effective Length	L'	26.383			m
Effective Width	B'	3.770			m
SLS Bearing Pressure	q _{SLS}	239	30	0	kPa
H/V Reduction Factor		0.983			
SLS Required Bearing Capacity	q _{SLS,REQ'D}	273			kPa
Load Rating	%LR	100%			%
Abutment 1 Pad Footing Bearing – ULS Transverse SM1600 + Wind					
Symbol	PE+LL	PE	LL	Units	
Total Vertical Force	N*	34796	29468	kN	
Transverse Force	F _{T,ULS}	22	0	kN	
Longitudinal Force	F _{L,ULS}	324	0	kN	
Transverse Moment	M _{T,ULS}	21764	276	kNm	
Longitudinal Moment	M _{L,ULS}	11218	3199	kNm	
H/V Ratio		0.009	0.000		
Transverse Eccentricity	e _T	0.625	0.009	m	
Longitudinal Eccentricity	e _L	0.322	0.109	m	
Effective Length	L'	26.049	27.281	m	
Effective Width	B'	3.655	4.083	m	
ULS Bearing Pressure	q*	365	265	101	kPa
ULS Bearing Capacity (Meyerhof)	φq _{ULT}	598			kPa
Load Rating	%LR	330%			%
Abutment 1 Pad Footing Bearing – ULS Longitudinal EQ					
Symbol	PE+EQ	PE	EQ	Units	
Total Vertical Force	N*	29468	29468	-	kN
Transverse Force	F _{T,ULS}	0	0	-	kN
Longitudinal Force	F _{L,ULS}	2248	0	-	kN
Transverse Moment	M _{T,ULS}	276	276	-	kNm
Longitudinal Moment	M _{L,ULS}	20022	3199	-	kNm
H/V Ratio		0.076	0.000	-	
Transverse Eccentricity	e _T	0.009	0.009	-	m
Longitudinal Eccentricity	e _L	0.679	0.109	-	m
Effective Length	L'	27.281	27.281	-	m
Effective Width	B'	2.941	4.083	-	m
ULS Bearing Pressure	q*	367	265	103 (equiv.)	kPa
ULS Bearing Capacity (Meyerhof)	φq _{ULT}	468	-	-	kPa
Load Rating	%LR	198%			%

Similarly, for the structural capacity of the footing, the SM1600 transverse case governed in the transverse direction (transverse to bridge) and the maximum PE and longitudinal EQ in the longitudinal direction. For the structural check the footing was modelled using Strand7, shown in Figure C.13 below.

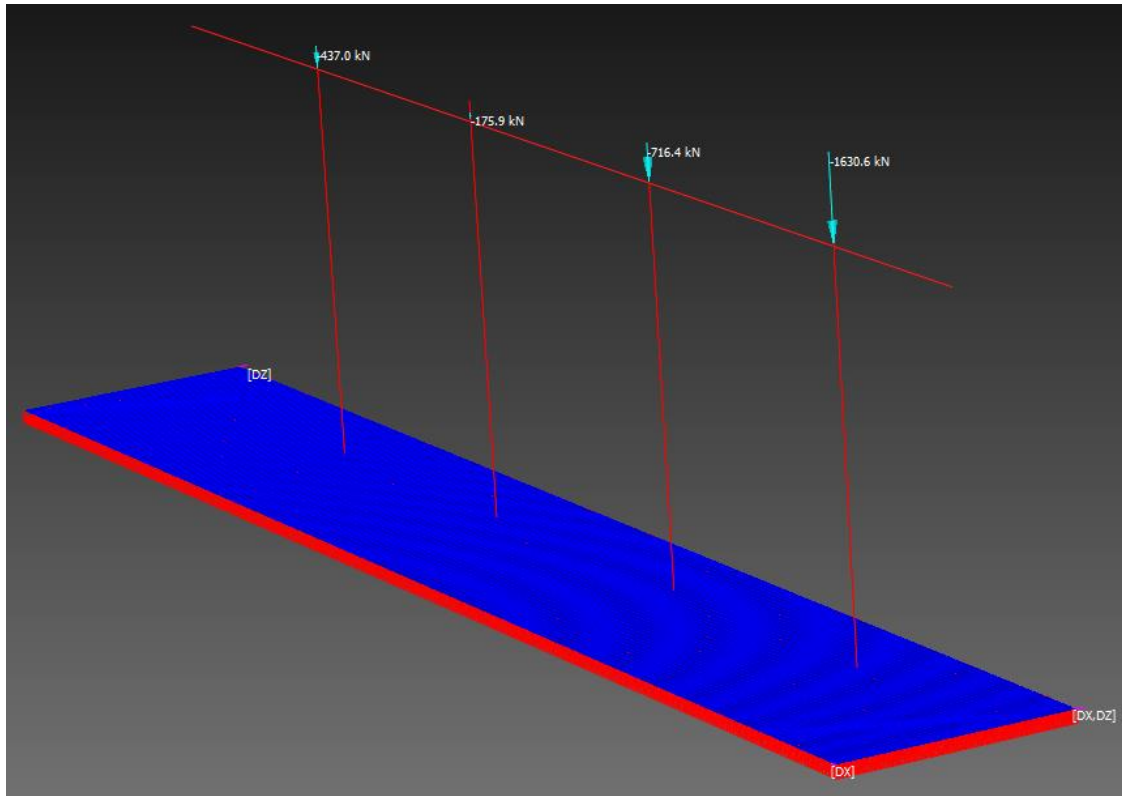


Figure C.13 Strand7 Model for Abutment 1 Pad Footing Structural Check

The structural check of Abutment 1 pad footing is shown in Table C.10 below.

Table C.10 Critical Pad Footing Structural Check for Abutment 1 (as per AS 5100.5:2017)

Abutment 1 Pad Footing Structural – ULS Transverse SM1600 + Wind	Symbol	PE+LL +0.7*Wind	PE +0.7*Wind	LL	Units
Maximum Moment	M^*	1058	542	-	kNm/m
Corresponding Shear	V_{Corr}	527	228	-	kN/m
Bottom Reinforcement Utilisation - MCFT		0.96	0.38	0.58 (equiv.)	
Load Rating	%LR	107%			%
Abutment 1 Pad Footing Structural – ULS Longitudinal EQ	Symbol	PE+EQ	PE	EQ	Units
Maximum Moment	M^*	444	186	-	kNm/m
Corresponding Shear	V_{Corr}	583	283	-	kN/m
Bottom Reinforcement Utilisation - MCFT		0.98	0.27	0.71 (equiv.)	
Load Rating	%LR	103%			%

Pier Columns

Hand calculations and a Strand7 model (shown in Figure C.14 below) were used to check worst case design actions on the pier columns. Bursting stresses at bearing locations were also checked in accordance with the BBR Multi-wire System prestressing (and bearings) manual (BBR Australia Pty Ltd, 1973).

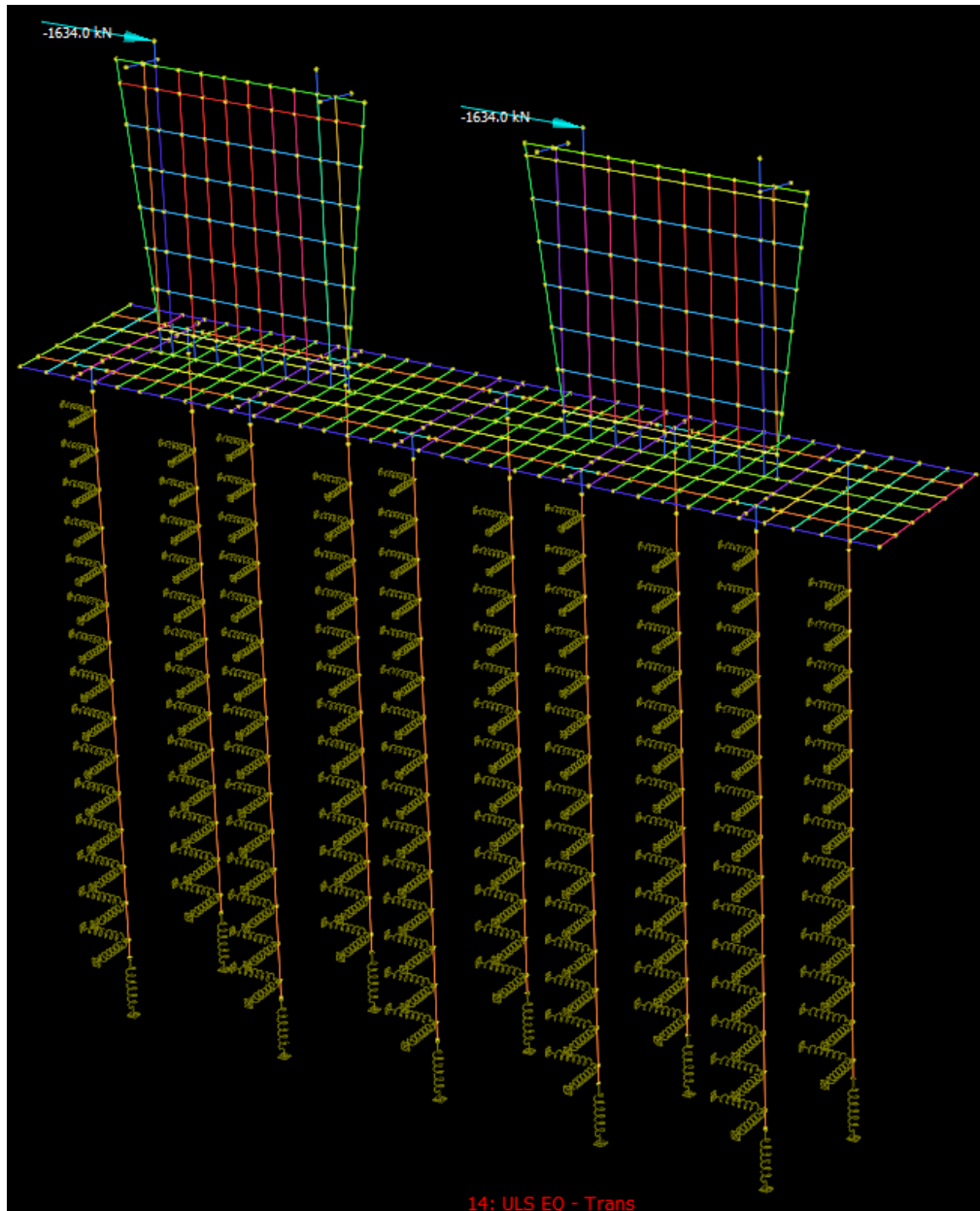


Figure C.14 Pier Strand7 Model (EQ Transverse Case)

ULS maximum PE + transverse EQ governed the pier column load ratings. The check conservatively ignored the shear keys at the abutments. The results are shown in Table C.11 below.

Table C.11 Pier Column Check (as per AS 5100.5:2017 and BBR Multi-wire System: Prestressing Manual 1973)

Pier Columns	Symbol	PE	EQ	Units
EQ Mass at Pier	m_P	-	1063.1	t
Horizontal Coefficient	$C_d(Tf)_P$	-	0.2153	
EQ Mass to Abutment 1	m_{A1}	-	600.0	t
Horizontal Coefficient $C_d(Tf)_{A1}$	$C_d(Tf)_{A1}$	-	0.1076	
EQ Mass to Abutment 2	m_{A2}	-	415.3	t
Horizontal Coefficient $C_d(Tf)_{A2}$	$C_d(Tf)_{A2}$	-	0.1076	
Stiffness Proportion to Pier Column	%	-	49.3%	%
Earthquake Force to Pier Column	F_{EQ}	-	1634	kN
Height of Mass	h_P	-	7.11	m
Transverse Bending Moment	$M_{x,EQ}$	355	11618	kNm
Transverse Pier Bending Capacity	ϕM_{ux}	135315		kNm
Load Rating	%LR	1162%		kNm
Pier Bursting				
Pier Bursting	Symbol	PE	LL	Units
ULS Bearing Load	N^*	1796	2684	kN
Bursting Force Resisted + Capacity of Ties Provided (Each Direction)	ϕT_b	1049		kN
Bursting Forces	T_b^*	244	365	kN
Load Rating	%LR	221%		
Pier Spalling				
Pier Spalling	Symbol	PE	LL	Units
ULS Bearing Loads (Average of Span 1 & Span 2)	N^*	2138	1389	kN
Spalling Force Resisted + Capacity of Top Longitudinal Bars Provided	ϕT_b	2015		
Spalling Forces	T_b^*	325	211	kN
Load Rating	%LR	799%		%

Pier Pilecap

A strut and tie model was used to assess the pilecap via transfer of loads from the pier columns to the piles. The model is shown in Figure C.15 below.

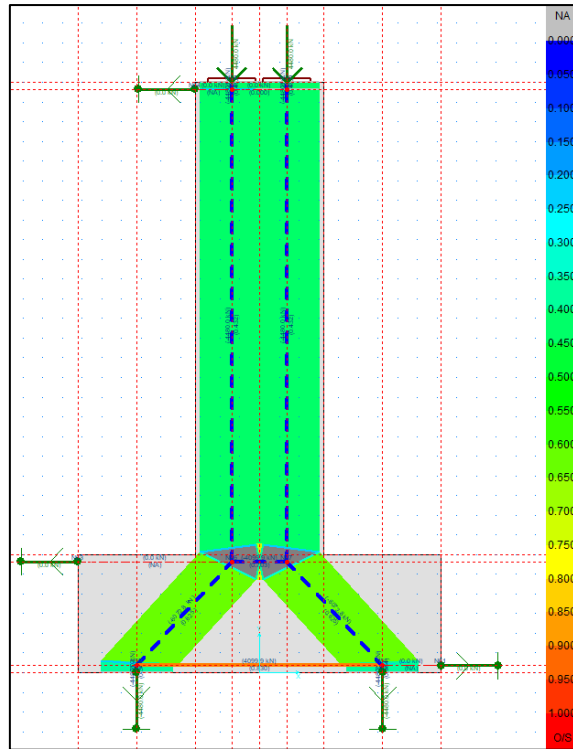


Figure C.15 CAST Strut & Tie Model – Pier Pilecap

Maximum PE and SM1600 loading governed the load rating of the bottom reinforcement. The load rating is shown in Table C.12 below.

Table C.12 Pier Pilecap Check (as per AS 5100.5:2017)

Pier Pilecap	Symbol	PE+LL	PE	LL	Units
ULS Bearing Load	N*	4480	1796	2684	kN
Bottom Reinforcement Utilisation		0.830	0.333	0.497	
Load Rating	%LR	134%			%

Pier Piles

Design actions were obtained from the Strand7 model shown in Figure C.14 above, with minimum PE and longitudinal impact (longitudinal to bridge) to the leading edge of Pier 1 governing. The load rating is shown in Table C.13 below.

Table C.13 Pier Piles Check (as per AS 5100.5:2017)

Pier Pile	Symbol	PE+LL	PE	LL	Units
ULS Maximum Moment	M*	1124	50	-	kNm
Corresponding Shear	V _{Corr}	196	31	-	kN
Corresponding Axial Force	N _{Corr}	-821	-1464	-	kN
Long. Reinforcement Utilisation		0.99	0.01	0.98	
Load Rating	%LR	101%			%

C.2.11 Conclusion and Recommendations

SM1600, T44, HLP, Group 1 and Group 2 vehicles were load rated for bending and shear using the MCFT approach in AS 5100.5:2017. The grillage properties were determined in line with Bridge Deck Behaviour (Hambly, 1991). The assessment covered 4No. bending checks and 5 No. shear checks for longitudinal design actions at 0.1 m increments, for 3 no. cases (a) maximum bending, corresponding shear and corresponding torsion; (b) maximum shear, corresponding bending and corresponding torsion; and (c) maximum torsion, corresponding bending and corresponding shear. The increments accounted for changes in section properties along the beams, as well as a worst-case combination of bending, shear and torsion. The design actions were assessed iteratively against bending and shear capacities. Compression fan regions, transverse bending, interface shear, substructure, foundations and bearings were also checked and found not to govern the load ratings.

Bridge No. 1694 is only 2 years old and there are no recommendations at this stage.

SECTION 5 – DESIGN VEHICLE LOADINGS

This information is Section 5 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Engineer Bridge Loading is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.



A LIM
SENIOR ENGINEER STRUCTURES

Date: 04/09/2023

Document No: 3912/02-5

Controlled Copies shall be marked accordingly

SECTION 5

CONTENTS

5	DESIGN VEHICLE LOADINGS.....	3
5.1	Introduction.....	3
5.2	Special Vehicle Loading	3
5.3	Oversize and Over-Mass Vehicles	3
5.4	Reduction of Standard Highway Loading	3

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
6	1	20/02/04	Road Train Vehicles diagram added to Appendix A
All	2	19/12/05	Complete review for introduction of AS 5100
3	3	10/01/07	Amendment of Document Number of High Wide Loads
3	4	11/01/12	Amendment of first paragraph in Section 5.2
All	5	06/07/22	Complete review for introduction of AS5100-2017
3	6	04/09/23	Amendment of Design Vehicle Loading Width and Service Vehicle

Custodian Endorsement

R Hossain
Engineer Bridge Loading
Date: 04/09/2023

5 DESIGN VEHICLE LOADINGS

5.1 Introduction

Generally vehicular (and pedestrian) loadings to be applied for the design of new structures shall be in accordance with AS 5100, Bridge Design (CODE). There are additional MRWA requirements, and these are described below. Where there is any conflict between the requirements of the CODE and the following, the latter shall take precedence.

Detailed guidelines applicable for vehicle loading and positioning are given in Branch Design Information Manual (BBDIM) Document No. 3912/02-04 “Load Rating Bridges”. Please note, the full width between barriers on the bridge shall be considered for design vehicle loadings to allow for any future changes ignoring internal kerbs, footpaths, traffic barriers, median barriers, and medians.

For load rating of bridges, the CODE, Document No. 3912/02-04 “Load Rating Bridges” and Document No. 6706-02-2227 “Load Rating and Refurbishment Design Manual for Existing Timber Bridges” are applicable.

5.2 Special Vehicle Loading

Structures located on highways, main roads and designated Heavy Haulage Routes shall be designed to Supervised Group 2 Vehicle 4, Group 2 Vehicle 5 and HLP 400 heavy load platform vehicles unless EBL specifies otherwise.

Structures that are part of a shared path where access by a maintenance, inspection or emergency vehicle is possible must be designed for a “Service Vehicle”. The configuration of the “Service Vehicle” is the same as an M10 truck (M-Truck), defined in Figure A8 of AS 5100.7-2004 with total mass of truck $M = 100$ kN. For performing load rating, the “Service Vehicle” shall be modelled and positioned similar as T44 vehicle (refer to Document 3912/02-04). The Load Factor and the Dynamic Load Allowance (DLA) shall in accordance with AS5100.2 defined for pedestrian, cyclist path and maintenance traffic loads. Structures protected by bollards are not exempt from this requirement, however shared path bridges containing loop ramps at each end are not required to comply.

5.3 Oversize and Over-Mass Vehicles

The design criteria for Oversize and Over-Mass load special vehicles shall be applied as additional specific load cases for all structures located on designated Oversize and Over-Mass Vehicle Corridors. Details of these special vehicles, designated routes and design guidelines are located online at www.mainroads.wa.gov.au, Guide to Design of Oversize and Over-Mass Vehicle Corridors.

The application of Oversize and Over-Mass vehicles for the design of new structures shall be confirmed with the Design Criteria Sheet and approved by SES.

5.4 Reduction of Standard Highway Loading

The use of less than full loading as outlined above on structures should only be considered in special cases as it is often a false economy and removes an important safety factor against overloading. Each instance must be approved individually by SES.

SECTION 6 – STRESS LIMITS IN STRUCTURAL CONCRETE

This information is Part 6 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 10/05/18

Document No: 3912/02-6

SECTION 6

CONTENTS

6	STRESS LIMITS IN STRUCTURAL CONCRETE	3
6.1	PRESTRESSED CONCRETE	3
6.2	REINFORCED CONCRETE	3

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	12/12/05	Complete review for introduction of AS 5100
All	2	04/04/18	Complete review for introduction of AS5100-2017

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 10/05/18

6 STRESS LIMITS IN STRUCTURAL CONCRETE

6.1 PRESTRESSED CONCRETE

When carrying out prestressed concrete design one of the Serviceability Limit State checks is for crack control in flexure. This is covered in AS 5100, Bridge Design (CODE), Part 5, Clauses 8.6.2 and 9.4.2 for the design of new bridges or load rating of bridges constructed using 500MPa steel reinforcement.

Additional requirements for prestressed concrete design limits on steel stress at the serviceability limit state are given in Table 6.1 for load rating of bridges constructed using different steel grades, and are applicable to both superstructure and substructure design. The values below are the limit on the increment in reinforcement bar stress between decompression and the applicable SLS load combination.

Table 6.1

Nominal Steel Grade (MPa)	Serviceability Stress Limits for Prestressed Concrete		
	T44/L44 & Road Trains	M1600	HLP & Special Vehicles
200	80	90	100
230	90	105	115
400	160	180	200

6.2 REINFORCED CONCRETE

Reinforced concrete requires different limitations on stress for serviceability compared to partially prestressed concrete due to the lower vulnerability of reinforcement to fatigue and corrosion.

When carrying out reinforced concrete design one of the Serviceability Limit State checks is for crack control in tension and flexure. This is covered in the CODE, Part 5, Clauses 8.6.1 and 9.4.1 for the design of new bridges or load rating of bridges constructed using 500MPa steel reinforcement.

Additional requirements for reinforced concrete design limits on steel stress at the serviceability limit state are given in Table 6.2 for load rating of bridges constructed using different steel grades, and are applicable to both superstructure and substructure design.

Table 6.2

Nominal Steel Grade (MPa)	Serviceability Stress Limits for Reinforced Concrete		
	T44/L44 & Road Trains	M1600	HLP & Special Vehicles
200	120	135	150
230	125	140	160
400	180	200	220

SECTION 7 – RAILINGS AND BARRIERS

This information is Part 7 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 11/01/19

Document No: 3912/02-7

SECTION 7

CONTENTS

7 RAILINGS AND BARRIERS 3

7.1 Traffic Barriers..... 3

7.1.1 General..... 3

7.1.2 Steel Barriers 3

7.1.3 Concrete Barriers..... 4

7.1.4 Transitions, Extents and Clear Zones 4

7.2 Balustrades 5

7.3 Standards and Approval 5

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	30/08/18	Complete review for introduction of AS 5100-2017

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 30/08/18

7 RAILINGS AND BARRIERS

7.1 Traffic Barriers

7.1.1 General

Traffic barriers are all barriers attached to a structure including bridges, underpasses, tunnels, culverts, retaining walls, traffic barrier footings and any associated approach slabs.

The same traffic barrier system should be used on both sides of the structure. Differing barriers may be used if required to simultaneously cater for pedestrian/cyclist access and passage of High Wide Loads.

Post holding down bolts must be designed such that they can be easily replaced if damaged during a crash.

The setback distance from the kerb face to the traffic barrier and height of rail above the road surface must be in accordance with Main Roads' standard drawings.

The CODE does not allow design of a barrier system by calculation, only design of prototypes for crash testing and design of modifications. It is important to note that crash testing or in-service performance evaluation to AS3845-2015 is required to confirm barrier performance. Since the 2015 update to AS3845 the barrier performance standard has been updated from NCHRP-350 to MASH. At the time of writing there are no barriers with steel sections available in Australia that have been tested to MASH requirements.

7.1.2 Steel Barriers

To prevent a variety of barrier proposals with unknown performance levels it is currently permitted to install AS5100-2004 compliant steel barrier systems and design the bridge to allow retrofit of an AS5100-2017 compliant barrier. Note:

1. Barrier design shall reference AS5100-2004 as the applicable standard on the design summary (typically located on the General Arrangement drawing)
2. The bridge (including anchorage) shall be designed for the increased loads from AS5100-2017
3. Post spacing can be assumed to be the same as existing standards
4. Line of sight implications for AS5100-2017 barrier geometry shall be checked with outcomes recorded in the design report & drawings
5. The above is only applicable whilst there is no approved AS5100-2017 regular performance steel barrier

Where sufficient rail height is required for cyclists and an AS5100-2004 low performance barrier is acceptable, heritage rail with toprail or low performance thriebeam (side-mounted PFC posts and PFC blockouts) with toprail should be considered. Note that toprail on a UC post is not a tested configuration and is therefore not accepted. Four rail should be considered where an AS5100-2004 regular performance system is required.

7.1.3 Concrete Barriers

For concrete barriers:

1. The preferred barrier shape of barriers on the edge of deck or edge of footpath is the F Type, due to the shape being less intrusive on shy lines
2. For F-Type barriers, geometrically extending an NCHRP-350 barrier or adding top rail to achieve the required effective height will be accepted as a medium performance barrier to MASH
3. Median barriers are preferred to be constant slope
4. For constant slope barriers, geometrically extending an NCHRP-350 barrier will be accepted as a medium performance barrier to MASH. Top rail is not acceptable
5. Other amendments to the shape of the barrier, eg: changing an edge to be vertical, is not preferred and is done at risk of the consultant. Eg: this has been a trend to meet footpath width requirements whilst minimising bridge width
6. Where the barrier system requires restraint, eg: by 75mm embedment into 3m of asphalt, this shall be increased accordingly for AS5100-2017 loads. This may require deeper embedment into asphalt to be effective

Concrete traffic barriers on bridges must not be considered as part of the deck and therefore must not contribute to its strength.

7.1.4 Transitions, Extents and Clear Zones

Start and end points of barriers must comply with 'length of need' requirements and extend adequately off the bridge to protect motorists from hazards in accordance with Austroads Guide to Road Design Part 6 and the associated Main Roads supplement. Examples of hazards include vertical drop, steep embankment, road or highway, railway, hazards in the median, or any combination of these.

Where access prevents installation of the required length of need or preferred barrier this is generally considered acceptable, but it must be demonstrated that vehicles accessing/leaving property are not subject to site specific safety concerns, increased risk due to crash histories, line of sight, etc. In some instances it will be required to liaise with the property owner to consider moving access to create a win-win outcome. Access for inspection and maintenance may also be justification for reducing the extent of guardrail, but can generally be worked around by providing one embankment behind the barriers that enables safe parking near the bridge.

Transitions from one barrier type to another must be done such that the performance of either barrier is not compromised, no unsafe ends are exposed and the appearance is neat. To avoid sudden changes in stiffness, short lengths of barrier joining onto a longer length of a different type of barrier must be avoided.

The ends of all approach and departure barriers must be terminated with a crashworthy end terminal in accordance with Austroads Guide to Road Design Part 6 and the associated Main Roads Supplement. It should be noted that the concept of clear zones is to allow 95% of sedan-class vehicles to recover. The statistical reliability of the research that clear zones is based on is low and no testing was done with regards to recovery of larger vehicles.

Due to the above, the shift to a safe systems approach within Main Roads and the changes in costs assigned to major incidents, providing the minimum Clear Zone as per Austroads does not generally negate the need for Guardrail. Any new structure or refurbishment omitting guardrail must justify the decision, considering factors such as whether existing guardrail is present, whether there is a local crash history, local road hazards and road geometry, the type of vehicles using/expected to use the crossing, AADT, etc.

7.2 Balustrades

Balustrades on road bridges, and on underpass headwalls and wingwalls where the wingwall is within 3m in plan of the edge of the path, must be standard Main Roads rectangular hollow section balustrade with solid balusters.

Balustrades on shared path bridges and associated ramps must comprise circular rails and circular balusters spaced in accordance with CODE requirements.

The standard Main Roads balustrade must extend no less than 3 complete panel lengths off the bridge from the abutment bearing centreline, and for bridges with abutment wingwalls adjacent to shared paths or footpaths the balustrade must extend at least 3m from the end of the wingwalls. A different type of barrier separating path users from hazards can be used beyond this point.

It should be noted that the standard Main Roads balustrade was not developed for crowd loading. The use of a flush mid-rail in place of a protruding grab-rail was via agreement with relevant internal and external stakeholders, note that acceptance was conditional on limiting use to paths of grade 1:50 and less.

The Memorandum of Understanding between Main Roads and the Public Transport Authority defines the ownership of Railway Protection Screens, refer D11#290707. In essence, Railway Protection Screens are owned by Main Roads if they are integral with balustrade or bridge barriers. All other Railway Protection Screens are owned by the PTA. Note that Railway Protection Screens should not be confused with screens used for privacy and other purposes.

The designer shall be considerate of detailing that allows ingress of water to tight spaces, eg: between edge-mounted steel plates and/or the deck. The retention of water may cause localised durability issues, such as rusting of anchor rods and consequently cracking & spalling of the deck well in advance of the design life. Note that silicon for water proofing is considered high maintenance and difficult to fund, therefore it should be avoided when possible. This is because the silicon perishes or hardens in a relatively short timeframe and if the bridge does not have other specific maintenance items then the silicon maintenance becomes a relatively low priority for maintenance funding. This is an especially common scenario for footbridges.

7.3 Standards and Approval

Refer to D11#307369 List of Approved Road Safety Barrier Systems for further information. Refer also to standard barrier and balustrade drawings in the Structures Engineering Standard Drawings Manual.

The omission of barriers or reduction in length of need will not be supported by Structures Engineering without detailed justification in the design report.

SECTION 8 – BEARINGS AND JOINTS

This information is Part 8 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As the head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.



A LIM
SENIOR ENGINEER STRUCTURES

Date: 04/09/2023

Document No: 3912/02-8

Controlled Copies shall be marked accordingly

SECTION 8

CONTENTS

8	BEARINGS AND JOINTS	3
8.1	Bearing Design	3
8.2	Expansion Joints	3
8.3	Approach Slabs.....	5

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	12/12/05	Complete review for introduction of AS 5100-2004
All	2	10/05/18	Complete review for introduction of AS 5100-2017
All	3	04/09/23	Complete review

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 04/09/2023

8 BEARINGS AND JOINTS

8.1 Bearing Design

The design of bearings is covered extensively in Part 4 of AS 5100, Bridge Design (CODE). Chapter 16 of the Bridge Branch Design Manual Document 3912/03 also contains useful information.

Elastomeric Bearings

Design Summary Notes, usually presented on the General Arrangement drawings, shall indicate the expected movement ranges at suitable timeframes (construction, 7 years, 15 years, 30 years) so that it can be easily determined whether measured deflections are within the design range. This ensures that bearings that are operating within specification are not mistaken as defective and flagged for maintenance. This has been an ongoing problem for long span bridges where creep and shrinkage are significant.

The ability to replace and re-set bearings is required as part of the bridge design. This will typically require structural design and geometric allowance for temporary jack locations and summarising pertinent information (eg: allowable jacking sequences and limitations on differential & total jacking).

Elastomeric bearings require keeper plates top and bottom (refer Section 2), regardless of whether minimum compression loads are met as per the Code. The designer is to allow for the reduced effective height of the bearing due to the keeper plates. Bolted plates are preferred over welded plates. Plates that are welded on a single side cannot provide a moment resisting couple and are therefore not allowed.

Other bearing types

There can be problems with overstressing pot bearings – particularly with a rotation movement under pressure. There is a ring underneath the elastomer that prevents egress down the piston when the elastomer is compressed. The ring can fail, which is particularly common for bearings that have the ends of the ring welded together. Consequently the elastomer can flow through the gap that is created and be permanently damaged.

8.2 Expansion Joints

Some form of expansion joint is required on most bridges to cater for longitudinal movements due to temperature change, concrete shrinkage and concrete creep. In fact one of the first decisions in a bridge design is what restraint system is to be adopted, i.e., where is the structure to be fixed and therefore where and in what direction is movement permitted.

The magnitude of anticipated movements due to temperature, creep and shrinkage can be calculated from figures given in the Code. Temperature movement can be +ve or -ve (expansion or contraction), whereas creep and shrinkage are only -ve (contraction). It is essential to ensure that there is adequate capacity for movement over the full temperature range, both early in the life of the bridge before much creep and shrinkage has occurred and ultimately after full creep and

shrinkage. Transverse movements need also be considered.

The concrete surrounding the expansion joint shall incorporate an upstand to suit the following seal types. The following table indicates typical values that should be confirmed with pavement design requirements for final design.

Seal Type	Required Concrete Upstand
2-coat seal (typical rural treatment)	20 mm
Asphalt / Hot-mix (rural)	40 mm
Asphalt / Hot mix (urban)	50 mm

The options available for expansion joints vary according to the anticipated range of movement and the type of structure, and reference to the Bridge Branch Design Manual Document 3912/03 should be made for details of the various types of joint and their applications. Chapter 16 of 3912/03 also gives a guide to the selection of an appropriate expansion joints for different bridge lengths.

Where finger plate joints are used, the fingers are to remain simply supported by extending across the joint. Cantilevered fingers have failed due to overstress or fatigue.

Modular joints must have a noise attenuation system if used in an urban area. The noise attenuation system must be supplied by the joint manufacturer and cannot be retrofitted with welded surface mounted plates. The top of the joint, including any noise attenuation system, must be at road surface level. Sufficient space must be provided under the Deck joint for access by maintenance personnel to safely remove and replace all joint components.

Advice on common types of expansion joints is provided below. Note that regional preferences may exist.

- Elastic polymer plug joints have been installed on Bridge 1009 Mill Point Road over Kwinana Freeway in 2016. At this time they are not considered suitable for high traffic volumes. This joint has also been installed on Bridges 87, 228, 270A, 572A, 1272, 5370.
- Poured flexible sealant has been used on multiple bridges, either between existing expansion joint angles or with new polymer nosing. The performance is extremely dependent on the quality of the installation. A good bond is often not achieved between existing expansion joint angles and the joint sealant. No comment is available on suitability when used with polymer nosings.
- Precompressed silicone and foam hybrid is currently being trialled, initial impressions of waterproofing are positive. These products are not suitable for installation between metal angles in any climate as the foam rapidly deteriorates. A construction drawback is that some products are supplied in 2m segment lengths, requiring numerous joints with joining silicone.

Where accessible by cyclists, anti-slip surfaces and gap widths between teeth (etc) must be suitable.

- For new bridges, cyclist requirements must be met without requiring modification of the proposed product.
- Where anti-slip plates have been welded to existing joints it has been found that the plates have dislodged and have the potential to become missiles.

Furthermore there is question as to whether the underlying joints have been damaged due to continued re-welding of the anti-slip plates. This and the ongoing maintenance needs to be considered versus the safety benefits.

8.3 Approach Slabs

Approach slabs are required for several reasons, including mitigation of settlement of approach embankment fill, provision of anchorage for expansion joints and approach transitions to reduce impact and sudden bumps.

Approach slabs shall be sufficiently thick to provide adequate support and anchorage for expansion joint angles and guardrail post anchor bolts, with consideration given to the ability of the slab to span over potential hollows or voids which may occur beneath the slab due to settlement or wash-out. Consideration must also be given to drainage and provision of kerbs etc.

If the road embankment is supported by solid rock and the abutment foundation is a spread footing on solid rock, then the approach slab shall be designed as a slab on elastic foundations. Controlled fill embankments with no possibility of scour or large settlements shall also be designed in this manner.

However, if underlying soils are soft and have the propensity for long term settlements then the approach slab shall be designed as simply supported, to span from the abutment support to the centreline of the trailing edge support of the approach slab.

Approach slabs designed in conjunction with timber bridge concrete overlays shall be in accordance with Document No. 6706-02-223, Structures Engineering Practice Notes.

At some sites it may be too disruptive to excavate deep enough to construct a corbel with an on-ground approach slab. In such cases an approach beam may be appropriate. In general an approach beam is only suitable for existing structures in the 20-30m length range where there will be limited settlement. It is not appropriate for situations where there may be scour.

SECTION 9 – CONSTRUCTION FORCES AND EFFECTS

This information is Part 9 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As the head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.



A LIM
SENIOR ENGINEER STRUCTURES

Date: 04/09/2023

Document No: 3912/02-9

Controlled Copies shall be marked accordingly

SECTION 9

CONTENTS

9 CONSTRUCTION FORCES AND EFFECTS 3

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	12/12/05	Complete review for introduction of AS 5100-2004
All	2	13/04/18	Complete review for introduction of AS5100-2017
All	3	04/09/23	No longer required. Marked for future removal

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 04/09/2023

9 CONSTRUCTION FORCES AND EFFECTS

This section is no longer used:

- For new bridges, the requirements have been transferred to Section 2.
- For maintenance and refurbishment, Section 3 requires the engineer to meet the same requirements as for new bridges.

Section 9 will be deleted in a future revision.

SECTION 10 – CONCRETE STRENGTHS AND FINISHES

This information is Part 10 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 16/04/18

Document No: 3912/02-10

SECTION 10

CONTENTS

10	CONCRETE STRENGTHS AND FINISHES	3
10.1	CONCRETE STRENGTHS.....	3
10.2	FINISHES	3
10.3	PROPRIETARY MORTAR AND REPAIR GROUTS.....	4
	TABLE 10.1 – FORMED SURFACE FINISHES FOR CONCRETE.....	5
	TABLE 10.2 – UNFORMED SURFACE FINISHES FOR CONCRETE.....	6

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	12/12/05	Complete review for introduction of AS 5100-2004
All	2	13/04/18	Complete review for introduction of AS 5100-2017

Custodian Endorsement

M RAJAKARUNA
Structures Design and Standards Engineer
Date: 13/04/18

10 CONCRETE STRENGTHS AND FINISHES

10.1 CONCRETE STRENGTHS

Unless otherwise approved by the SES, the following standard concrete strengths shall be used in the design of new bridges and the refurbishment design of existing bridges:

Concrete Strength	Class	Comments
20MPa	N20	Non-structural works only where durability is not an important factor, e.g., – blinding, post footings, mass concrete fill, paths etc
35MPa	S35/10	Standard reinforced concrete for precast parapet panels
40MPa	S40	Standard reinforced concrete and prestressed concrete, e.g., – foundations, piers, decks, concrete overlays, beams etc
50MPa	S50	Precast reinforced concrete, precast prestressed concrete, precast piles, beams, stress anchorages etc
	S50M	Reinforced concrete substructures in marine applications.
65MPa	S65	Precast prestressed beams

The 20 MPa is a standard AS 3600 mix and is designated N20. All others are specifically defined mixes as per MRWA Specification 820.

Although higher concrete strengths are included in the Bridge Code, parameters for higher strength mixes do not currently form part of Main Roads Specification 820. Higher strength mixes and/or special concretes can be used in special situations, e.g., prestressed concrete footbridges, precast work, high early strength, self-compacting concrete, sulphate resisting etc. The use of higher strength and/or special concretes is to be confirmed in the Design Criteria Sheet and approved by the SES.

10.2 FINISHES

All concrete surfaces should have the standard of finish indicated on the Drawings. There are two broad groups of concrete finishes – formed and unformed surfaces.

Formed Surface Finishes - shall comply with the requirements of Section 3 of AS 3610 - "Formwork for Concrete". Finishes Type 2, 3 and 4 cover most situations for bridge works and Table 10.1 gives guidance as to where they are to be used. Refer to the Standard for full details of allowable tolerances, colour variation, etc for each finish. Special formed finishes may also be used, e.g. ribbed, rope, board marked etc, but the above three cover the majority of cases.

Unformed Surface Finishes - four classes, U1 to U4 as per Table 10.2, cover all normal requirements. Note that the finishes and irregularities do not scale from best to worst as per formed finishes. The user is referred to the “typical location” in Table 10.2 to ensure appropriate unformed finishes are selected.

10.3 PROPRIETARY MORTAR AND REPAIR GROUTS

Proprietary mortars and grouts are often used for bearing pads, concrete repairs, infill concrete and other special applications. They shall be selected based on the appropriate requirements for strength, workability, performance or other special characteristics from well-known suppliers and/or manufacturers.

In general, such proprietary products should be readily available within Western Australia or Australia, and supported with detailed Technical and Safety Data Sheets.

Where a particular product has not been used previously on a MRWA project, it shall be approved by the SES prior to use in the Works. Consultants proposing the use of new products shall seek approval for its use prior to finalising the design or Works commencing.

TABLE 10.1 – FORMED SURFACE FINISHES FOR CONCRETE

Designated Finish	Typical Location	Type of Concrete Finish⁽¹⁾	Maximum Allowable Surface Irregularities
2	Exposed surfaces, general external and internal surfaces intended to be viewed in detail	Smooth, dense and dust free concrete finish uniform in colour and accurately formed to specified dimensions and tolerances. Joint marks to be unobtrusive and concrete surfaces to be free from air holes and effects of water migration. Panels to be arranged in an approved regular pattern conforming to the structural geometry.	3 mm abrupt or 6 mm in a 1.5m template
2X	As specified on the Drawings	Sandblasted concrete finish, or special architectural applications, otherwise as per Type 2 above.	As specified
3	General external or internal surfaces intended to be viewed as a whole, or unexposed surfaces hidden from view	Regular, dense and dust free concrete surface entirely free from honeycombing and effects of cement paste leakage.	5 mm abrupt or 7 mm in a 1.5m template
4	Footings and buried surfaces	Structurally sound and durable concrete with a dense surface free from honeycombing.	8 mm abrupt or 10 mm in a 1.5m template

Note: Table 10.1 provides a general description only. Refer to AS 3610 for detailed descriptions and classifications.

TABLE 10.2 – UNFORMED SURFACE FINISHES FOR CONCRETE

Designated Finish	Typical Location	Type of Concrete Finish	Maximum Allowable Surface Irregularities
U1	Unexposed surfaces	A wood floated finish to produce a uniform, dense concrete surface free of surface pitting or cavities.	5 mm abrupt or 15 mm in a 3m template
U2	Upper exposed surfaces	A high quality steel trowelled finish to produce a uniform, dense, smooth and impervious concrete surface finish free of surface pitting or cavities.	Nil abrupt or 5 mm in a 3m template
U3	Upper surfaces of bridge decks and approach slabs/spans	A high quality mechanical steel trowelled finish to produce a uniform, dense impervious concrete surface finish free of surface pitting or cavities.	2 mm abrupt or 5 mm in a 3m template
U4	Upper surfaces of bridge deck concrete overlays, footpaths and medians	A high quality wood floated finish to produce a uniform surface free of surface pitting or cavities followed by a broom finish to produce a uniformly roughened concrete surface free of excessive drag marks and overlaps.	2 mm abrupt or 5 mm in a 3m template

SECTION 11 – BRIDGE WIDTHS

This information is Part 11 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 27/07/2018

Document No: 3912/02-11

SECTION 11

CONTENTS

11	BRIDGE WIDTH APPROVAL PROCEDURE	3
11.1	Urban Bridges	3
11.2	Rural Bridges	3
11.3	Asset Owners Advice.....	3
11.4	Actions by Structures Engineering	3
11.5	Responsibilities for Consultants	4
11.6	Bridge Width Requirements	4

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	13/12/05	Complete review for introduction of AS 5100-2004
4	2	13/11/14	Updated Principal Design Engineer position in R&TE branch.
5	2	13/11/14	Table 11 - revised width requirements for roads other than National Highways
All	3	19/07/17	Complete review against AS5100.1-2017. No changes required.
3-4	3	19/07/17	Asset Owner, endorsements and approvals updated.
5	3	19/07/17	“Sealed Shoulder Width” amended to “Total Sealed Shoulder Width” and notes adjusted accordingly.
6	3	19/07/17	“Shoulder Width” amended to “Total Shoulder Width”. “Location” fields updated. Endorsements and approvals amended.
3	4	21/09/17	Endorsements and approvals amended
5	5	21/05/18	Table 11 AADT ranges updated. Rural Bridge Width Approval Form revision number amended.

Custodian Endorsement

M RAJAKARUNA

Structures Design & Standards Engineer

Date: 26/07/18

11 BRIDGE WIDTH APPROVAL PROCEDURE

This Section covers the procedure to be adopted for the determination and approval of bridge widths. It is split into two parts, Urban and Rural, as the criteria for assessing each are different. Rural bridge widths are standardised and determined based mainly on anticipated traffic flows. Urban bridge widths are subject to more variation.

The definition of 'urban' and 'rural' in this context is fairly subjective, being based more on the type of road/structure than its geographic location. The Structures Design & Standards Engineer shall be responsible for deciding which part of the procedure to follow.

In all cases, consideration should be given to the possible need for future widening.

11.1 URBAN BRIDGES

The Designer shall seek advice from the Principal Design Engineer, Road & Traffic Engineering Branch, on the required bridge width, including carriageway widths, shoulders, medians, dual use paths etc.

These requirements shall be incorporated into a schematic bridge cross-section, placed on the Bridge Design Part File and circulated for approval as per Paragraphs 11.3 and 11.4 below.

11.2 RURAL BRIDGES

For each rural bridge, the Designer shall place a Rural Bridge Width Approval Form 3912/02/11/01 and a copy of the best available map on file for the relevant Region. The map should show the location of the bridge site including details of the road and the Local Government area in which it is located.

Bridge width requirements are described in Section 11.6 below.

11.3 ASSET OWNERS ADVICE

The Designer shall obtain advice from the Asset Owner as to local requirements for bridge width. For MRWA owned bridges, the Asset Owner is the regional Asset Manager Structures.

11.4 ENDORSEMENTS AND APPROVALS

The schematic bridge cross-section (in the case of urban bridges) or the completed Rural Bridge Width Approval Form (in the case of rural bridges) shall be sent to:

- Asset Owner for advice
- Principal Design Engineer for advice (urban bridges only)
- regional Asset Manager Structures for endorsement

Following endorsement, forwarded to:

- Senior Engineer Structures for authorisation

Following authorisation, the regional Asset Manager Structures is responsible for placing the signed Rural Bridge Width Approval Form on the specific bridge design or maintenance file as appropriate.

11.5 RESPONSIBILITIES FOR CONSULTANTS

When the design is undertaken by Consultants, then unless otherwise specified in the consultants brief, the Consultant shall assume all the responsibilities of the Designer in the above procedure except that the MRWA Project Manager shall arrange for filing and returning a copy to the Consultant after actions by Structures Engineering as detailed above.

11.6 BRIDGE WIDTH REQUIREMENTS

The recommended minimum rural road and bridge width between kerbs for Roads other than Main Roads and Highways shall be in accordance with Table 11.

The minimum bridge width between kerbs on Main roads and Highways shall be :

- Width of Traffic Lanes + 2.4m unless the road is rarely trafficked by heavy vehicles and the AADT < 1000/lane in which case the width can be Width of Traffic Lanes + 1.2m.
- For bridges with less than 20 m in length, the width shall be full formation width.

For any curve widening width requirements, refer to Section 7.9 of Austroads Guide to Road Design: Part 3 the Geometric Design,

These width requirements do not apply to existing bridge refurbishment and widening work.

TABLE 11 RECOMMENDED MINIMUM RURAL ROAD AND BRIDGE WIDTHS
(Roads other than Main Roads and Highways)

	UNSEALED ROADS	SEALED ROADS				
		SINGLE LANE	TWO LANES			
DESIGN AADT (VPD)	<100	<150	150-500	500-1000	1000-2000	2000-8000
Sealed Trafficway Width	Not Applicable	3.5	6.0	7.0	7.0	7.0
Total Sealed Shoulder Width (1)	Not Applicable	1.5-2.5	1.0-1.5	1.5-2.0	2.0	2.0
Formation Width	As Appropriate	6.5-8.5	9.0	10.0	11.0	12.0
Bridge Width Between Kerbs (2)	4.2 (3, 4)	4.2 (3, 4)	7.2 (4)	8.2 (5)	8.2 (5)	8.2 (6)

Abbreviations: AADT – Annual Average Daily Traffic
VPD – Vehicles Per day

NOTES:

1. The Total Sealed Shoulder Width is the sum of both shoulders
2. Where there is a kerbed footway on the bridge, the kerb shall be set back a minimum of 600mm from the edge of the adjacent traffic lane
3. Where sight distance is inadequate or bridge length is less than 10m, the minimum width shall be 7.2m
4. For length of bridge 6m or less, the width shall be full formation width
5. For length of bridge 9m or less, the width shall be full formation width
6. For length of bridge 15m or less, the width shall be full formation width

References: AS 5100-2017, Bridge Design, Part 1
AUSTROADS Guide to Road Design, Part 3: Geometric Design

RURAL BRIDGE WIDTH APPROVAL FORM

3912/02/11/02

LOCATION

BRIDGE NUMBER	ROAD NUMBER	ROAD NAME
BRIDGE OVER	AT SLK	
ASSET OWNER	REGION	LOCAL GOV

PROPOSED STRUCTURE

TYPE OF BRIDGE
NUMBER OF SPANS TOTAL LENGTH

TRAFFIC DATA

ACTUAL AADT	(vpd)	(Year)	
DESIGN AADT	(vpd)	(Year)	DESIGN SPEED (km / hr)

	TRAFFICWAY WIDTH (m)	CURVE WIDENINGS (m) (IF REQUIRED)	TOTAL SHOULDER WIDTH (m)		FORMATION WIDTH (m)	BRIDGE WIDTH BETWEEN KERBS (m)
			SEALED	TOTAL		
Existing						
Minimum (1)						
Proposed						

(1) From Table 11

Comments:

Recommended By

Date / /

DESIGN ENGINEER

Endorsed By

Date / /

DESIGN SECTION LEADER

Asset Manager Structures Endorsement

Advice from Asset Owner at Folio:
 (May be N/A for MRWA Asset Owners)

Note: endorsement is required prior to submitting to SES for authorisation

SES Authorisation

SECTION 12 – CLEARANCES AND HIGH LOAD ROUTES

This information is Part 12 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Asset Policy Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 28/08/18

Document No: 3912/02-12

SECTION 12

CONTENTS

12	DESIGN VEHICLE LOADINGS	3
12.1	Introduction	3
12.2	Road Over Road Bridges and Footbridges.....	3
12.3	Road Over Rail Bridges	3
12.4	Bridges Over Water.....	4
12.5	Clearances During Construction	4
12.6	High Load Routes.....	4
12.7	High/Wide Load Routes.....	4

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
2	1	04/03/04	Clause 12.2 amended
5	1	04/03/04	Figure 12.1 amended
All	2	13/12/05	Complete review for introduction of AS 5100-2004
3,4	1	24/8/07	Figure Nos changed
6,7	1	24/8/07	Figure 12.2 drawing updated
8	1	24/8/07	Figure 12.4 drawing added
9 to 11	1	24/8/07	Figures 12.5 to 12.7 changed.
5	2	11/01/12	Figure 12.1 amended
All	3	20/08/18	Complete review for introduction of AS5100-2017

Custodian Endorsement

J PARVIN
Structures Asset Policy Engineer
Date: 24/08/18

12 DESIGN VEHICLE LOADINGS

12.1 Introduction

This Section sets out the minimum clearances, both horizontal and vertical, to be used in the design of bridges. It generally follows the requirements of Part 1, Clause 13 of AS 5100, Bridge Design (CODE), but where there is any conflict this document shall take precedence. Where none of the following considerations are applicable the minimum vertical clearance shall be set at 1.0m clear headroom to assist in safe future inspections and maintenance activities.

12.2 Road Over Road Bridges and Footbridges

Horizontal clearances shall be in accordance with Figure 12.1 attached. The minimum clearance shown on Figure 12.1 is derived for highway and main roads. Clearances below those specified may be used if suitable traffic barriers are installed.

Traffic barriers may be flexible (e.g. wire rope safety barriers or w-beam) or rigid (eg: concrete barriers). Refer further DIS 3912/02-2 “Design of New Structures”, Section 2.3 and Road and Traffic Engineering Branch’s Document No. D11#38472, *MRWA Supplement to Austroads Guide to Road Design – Part 6*.

For any situation not covered in this section, reference may be made to AUSTRROADS Guide to the Geometric Design of Major Urban Roads.

Vertical clearances shall be in accordance with Part 1, Clause 13.7 of the CODE, but shall be approved by the SD&SE.

12.3 Road Over Rail Bridges

Clearances shall be in accordance with the Public Transport Authority (PTA) clearance requirements. The clearance diagrams from PTA dated 28 Feb 2018 are shown at Figures 12.2 to 12.4. In all cases confirmation must be obtained from PTA.

On electrified routes, suitable protective screens must be installed on over-bridges to prevent people from touching the wires. Screens shall accommodate the minimum clearances as required by PTA. Screens must be provided on both sides of the bridge and must extend as per Public Transport Authority Specification “Protection Screens for Bridges over Electrified Railways”.

Because of the potentially catastrophic consequences of a train hitting a bridge pier, wherever possible railway lines should be crossed in a single span with solid abutments. Where a single span is not possible, piers shall be positioned and designed in accordance with the CODE and DIS 3912/02-2 “Design of New Structures”, Section 2.3.

12.4 Bridges Over Water

Navigation clearances are not usually a requirement for bridges in WA, but where they may be required, the relevant figures must be obtained from the Department for Planning and Infrastructure, Marine Information.

12.5 Clearances During Construction

During construction, it is often possible to reduce the above requirements. For road bridges, horizontal clearances may be reduced to the minimum required for safe working space with suitable protection works provided alternate routes are available for the transport of over-height vehicles. Vertical clearances may be reduced to 4.7 m or lower in specific circumstances. However, this may require special protective measures to be taken during construction and each case must be approved by SES. The preferred minimum clearance during construction is 4.90m.

For rail bridges, no reduction in horizontal clearance is permitted, however reduction in vertical clearance may be possible. Each case must be checked individually with PTA. In particular, construction over electrified lines will require special measures to be taken.

12.6 High Load Routes

There are a number of specific transport routes which are designated High Load Routes for the transport of large, indivisible loads. It is important that the vertical clearances on these routes are not encroached upon.

Details of existing and future preferred High Load Routes are shown in the attached Figures 12.5 and 12.6.

Designers shall ensure that all road bridges over these roads conform to these requirements. Clearances to footbridges should be an additional 300 mm greater than those shown.

The required vertical clearance shall be entered on the Design Criteria Sheet.

12.7 High/Wide Load Routes

High/Wide Load Routes incorporate the High Wide Load Corridor Project involving the development of suitable transport envelopes that will accommodate over-dimension loads up to 8m high, 8m wide and 24m long, and with a maximum 270 tonne net load along the designated routes that link key heavy industry centres in the Perth Metropolitan area. For other routes, clearance requirements need be obtained from Access Manager of Heavy Vehicle Services MRWA.

The designated routes and clearance requirements are located online at www.mainroads.wa.gov.au, Building Roads, Standards and Technical, Road and Traffic Engineering, Guide to Road Design, High Wide Loads.

The use of clearances for High/Wide Load vehicles for the design of new structures shall be confirmed with the Design Criteria Sheet and approved by the SES.

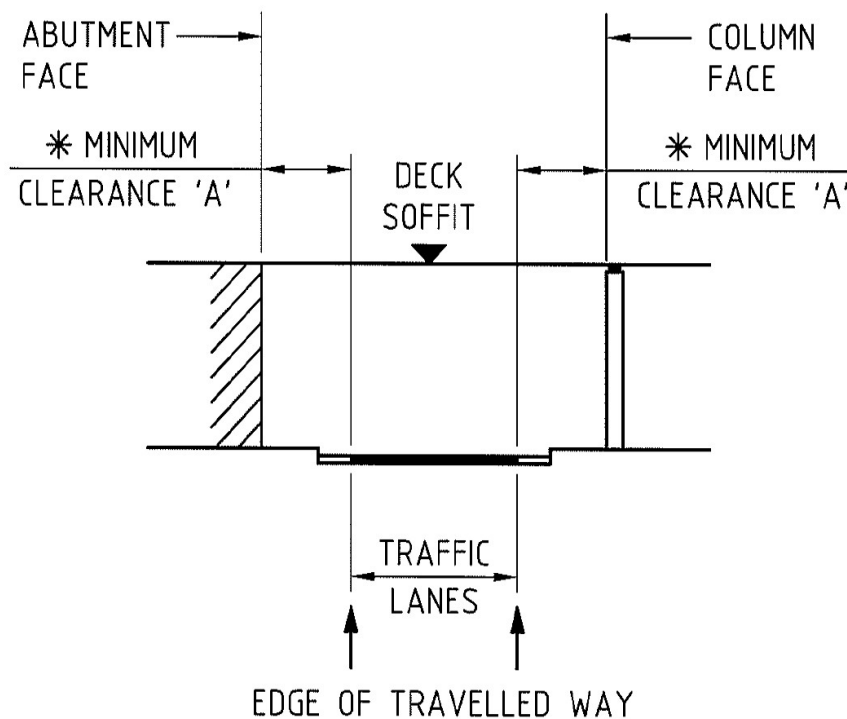
FIGURE 12.1

HORIZONTAL CLEARANCE TO SUBSTRUCTURE
COMPONENTS OF BRIDGES OVER ROADWAYS

MIN 'A' = 5m (DESIGN SPEEDS \leq 60 km/h)

MIN 'A' = 7m (60 km/h < DESIGN SPEEDS < 90 km/h)

MIN 'A' = 10m (90 km/h \leq DESIGN SPEEDS)



* MINIMUM CLEARANCE WIDTH 'A' IS MEASURED FROM THE EDGE OF TRAVELLED WAY. FILL BATTER SLOPE WITHIN 'A' SHALL BE 1 IN 5.5 OR FLATTER AND CUT BATTER SLOPE SHALL BE 1 IN 3 OR FLATTER.

FIGURES 12.2 TO 12.4
RAILWAY CLEARANCE REQUIREMENTS

NARROW GAUGE LINES (See Sheet 1)

1. NOTES ON TRACK CENTRES

- 1.1 Desirable minimum track centres for tangent track.
- 1.1.1 Adjacent tracks with marginal masts 4000mm.
- 1.1.2 Central overhead traction masts 5200mm.
- 1.2 Minimum track centres in mm for curved track:
- 1.2.1 $4000 \text{ or } 5200 + \frac{72250}{R} + 3(Ea1-Ea2)$ Where Ea1 is greater than Ea2
- 1.2.2 $4000 \text{ or } 5200 + \frac{72250}{R}$ Where Ea2 is greater than Ea1
- Ea1 = Cant in mm of Outer Track
Ea2 = Cant in mm of Inner Track
R = Radius in Metres

2. NOTES ON STRUCTURAL CLEARANCE OUTLINE

- 2.1 Minimum structural clearance of 2140mm to be increased by
- $$\frac{36125}{R} + 3Ea$$
- on the inside of a curve
- Where R = Radius in metres Ea = Cant in mm
(no increase to outside of curve)
- 2.2 All new overhead structures are to be constructed with a minimum overhead clearance in accordance with "The Design Supply Construction and Commissioning of 25 kvAC Traction Overhead Catenary Equipment" Doc. No. 8190-800-001.

- 2.3 Heights to be measured from high rail on curves.
- 2.4 Clearance outline to be increased to 4500mm from track centreline for fences and long structures without refuges. Faces of masts carrying catenary systems to be in accordance with "The Design Supply Construction and Commissioning of 25 kvAC Traction Overhead Catenary Equipment" Doc. No. 8190-800-001. For bridges and retaining walls within the railway reserve refer to Drg 00-C-04-0079

3. NOTES ON ROLLINGSTOCK & LOADING OUTLINES

- 3.1 All new passenger rollingstock shall be built to the Urban Passenger Railcar Static Outline.
- 3.2 The maximum longitudinal dimensions for rollingstock and railcar outlines are:
- I) Length over body 24 metres
II) Bogle Centres 17 metres
III) Bogle Centre to body end 3.5 metres
- The values in Notes 1.2 and 2.1 are based upon these dimensions.

4. NOTES ON PLATFORMS AND STATION STRUCTURES

- 4.1 Platform Clearances
- 4.1.1 Platforms are a permanent infringement of the base operating standard.
- 4.1.2 Platforms on curves must be approved in advance by the Manager Track and Structures or their approved delegate, as a minimum prior to Project Definition Plan stage.
- 4.1.3 On curves platform distance in mm from centre of track to be increased by:
- 4.1.3.1 Convex Platform Faces $\frac{36125}{R} + Ea$ R = Radius in metres
Ea = Cant in mm
- 4.1.3.2 Concave Platform Faces $\frac{36125}{R} - Ea$
- Note that concessions to these dimensions may be required for conformance to disability standard at door steps.

- 4.2 Platform heights on curves to be measured perpendicular to the plane of the designed cant. i.e. top of rails.
- 4.3 For structures on platforms, see Drgs 00-C-04-1398 and 00-C-04-1399

STANDARD AND DUAL GAUGE LINES (See Sheet 2)

5. NOTES ON TRACK CENTRES

- 5.1 Minimum track centres for tangent track
- 5.1.1 Adjacent tracks 4000mm. NG to NG, SG to SG and NG to SG.
- 5.1.2 Central overhead traction masts:
Centres to provide for masts to be outside minimum structural clearance
- 5.2 Minimum track centres in mm for curved track
- 5.2.1 Passenger Rollingstock and Loading Outline
- 5.2.1.1 Tangent Centres $+ \frac{83600}{R} + 3(Ea1-Ea2)$ Where Ea1 is greater than Ea2
- 5.2.1.2 Tangent Centres $+ \frac{83600}{R}$ Where Ea2 is greater than Ea1
- Ea1 = Cant in mm of Outer Track Ea2 = Cant in mm of Inner Track
R = Radius in Metres
- 5.2.2 Freight Rollingstock and Loading Outline
- 5.2.2.1 Tangent Centres $+ \frac{83600}{R} + 4.5(Ea1-Ea2)$ Where Ea1 is greater than Ea2
- 5.2.2.2 Tangent Centres $+ \frac{83600}{R}$ Where Ea2 is greater than Ea1

6. NOTES ON STRUCTURAL CLEARANCE OUTLINE

- 6.1 Minimum structural clearance of 2140mm, 2325mm or 2500mm to be increased by
- $$\frac{41800}{R} + 3Ea \text{ or } \frac{41800}{R} + 4.5 Ea$$
- on the inside of a curve
- Where R = Radius in metres
Ea = Cant in mm
(no increase to outside of curve)
- 6.2 All new overhead structures are to be constructed with a minimum overhead clearance in accordance with "The Design Supply Construction and Commissioning of 25 kvAC Traction Overhead Catenary Equipment" Doc. No. 8190-800-001.

- 6.3 Heights to be measured from high rail on curves.
- 6.4 Clearance outline to be increased to 4500mm from track centreline for fences and long structures without refuges. Faces of masts carrying catenary systems to be in accordance with "The Design Supply Construction and Commissioning of 25 kvAC Traction Overhead Catenary Equipment" Doc. No. 8190-800-001. For bridges and retaining walls within the railway reserve refer to Drg 00-C-04-0079
- 6.5 On the common rail side the co-incident NG clearance outline governs.

7. NOTES ON ROLLINGSTOCK & LOADING OUTLINES

- 7.1 Current minimum wire height of 6200 on the North Fremantle to Fremantle Section precludes operation of double stack container vehicles. For vehicle outline refer to AS7507 RISSB Reference vehicle 33.
- 7.2 The maximum longitudinal dimensions for rollingstock and loading outlines are:
- I) Length over body 25.9 metres
II) Bogle Centres 18.3 metres
III) Bogle Centre to body end 3.8 metres
- The values in Notes 5.2 and 6.1 are based upon these dimensions.

8. NOTES ON PLATFORMS AND STATION STRUCTURES

- 8.1 Platform Clearances
- 8.1.1 Platforms are a permanent infringement of the base operating standard.
- 8.1.2 The platform clearance and platform height shown are for standard gauge track only. For dual gauge track, narrow gauge clearances govern. See Sheet 1 for narrow gauge clearances.

- 8.1.3 On curves platform distance in mm from centre of track to be increased by:
- 8.1.3.1 Convex Platform Faces $\frac{41800}{R} + Ea$ R = Radius in metres
Ea = Cant in mm
- 8.1.3.2 Concave Platform Faces $\frac{41800}{R} - Ea$
- Note that concessions to these dimensions may be required for conformance to disability standard at door steps.
- 8.2 Platform heights on curves to be measured perpendicular to the plane of the designed cant. i.e. top of rails.
- 8.3 For structures on platforms, see Drgs 00-C-04-1398 and 00-C-04-1399

GENERAL NOTES (Sheets 1 and 2)

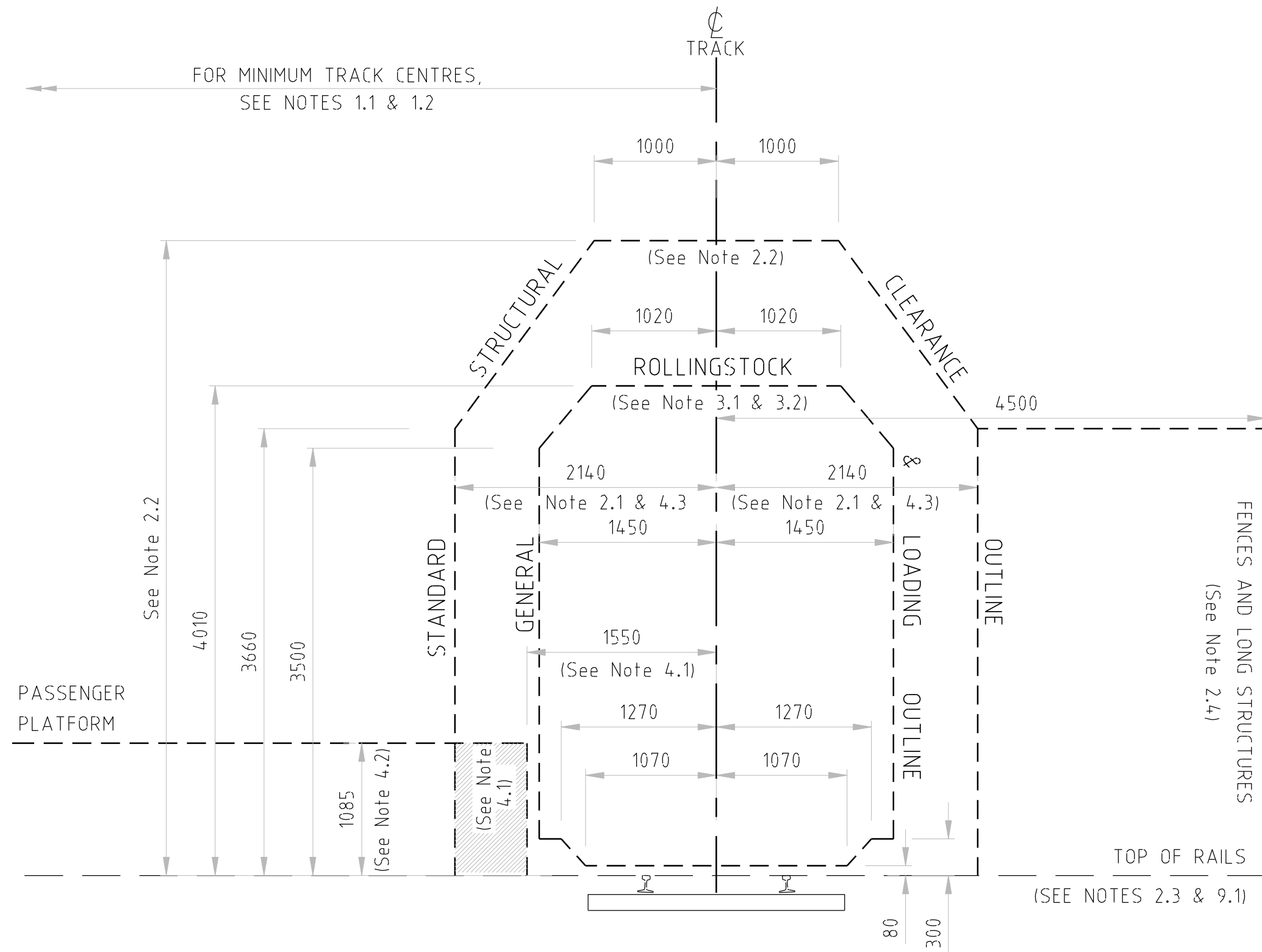
9. GENERAL NOTES

- 9.1 For special circumstances, concessional structural clearances may be considered by the Manager Track and Structures (or their approved delegate) with a supporting safety argument and associated risk assessment. These shall comply with the general design procedures of the NG & SG Codes of Practice. Approved concessions shall be entered into the clearance register. Use standard form 8830-400-007 - Request for Concessional Structural Clearance
- 9.2 Third Party access. Procedures must be in accordance with the Railways (Access) Act 1998 and Railways (Access) Code 2000.
- 9.3 For Clearance and Rollingstock Outlines on Narrow Gauge Lines, refer 00-C-04-0076
- 9.4 For Clearance and Rollingstock Outlines on Standard and Dual Lines, refer 00-C-04-0077

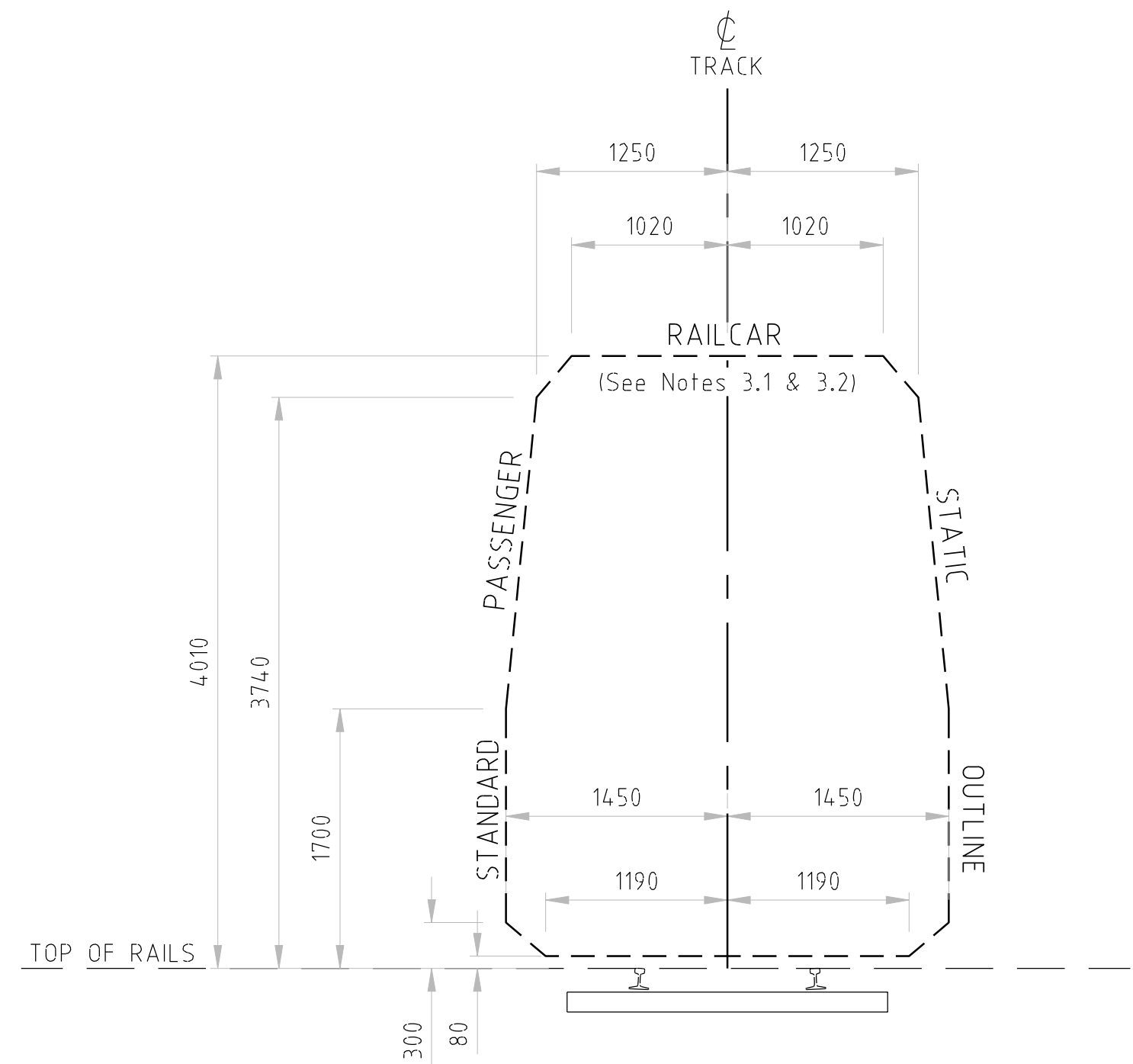
1	28.02.2018	ISSUED AS STANDARD	ZS	ZS	MK	RD
5	19.05.06	ISSUED FOR CONSTRUCTION	WPL	AWP	WPL	PM
REV	DATE	AMENDMENT	DSN	DRN	CHKD	APP
ORIG SIZE	A1					
<small>This document must not be copied without PTA's written permission, and the contents thereof must not be imparted to a third party nor be used for any unauthorised purpose.</small>						

CAD DRAWING PATHNAME \\p\pwp\j\02\rend\fontemp\mp-905090573431031224\00-C-04-0078

REFERENCES	SCALE :	DESIGNED		CLEARANCES STANDARDS FOR URBAN NETWORK STRUCTURAL CLEARANCE AND ROLLINGSTOCK OUTLINES NOTES RELATING TO CLEARANCES
	DATUM :	DRAWN		
	HORIZONTAL :	CHECKED		
	VERTICAL :	APPROVED FOR ISSUE		
PTA ACCEPTANCE STAMP	A3335619	MANAGER TRACK & STRUCTURES Network & Infrastructure	DATE	PTA Drawing No: 00-C-04-0078 REV : 1



STANDARD OUTLINES FOR STRUCTURAL CLEARANCE, ROLLINGSTOCK AND LOADING



STATIC OUTLINE FOR STANDARD PASSENGER RAILCARS

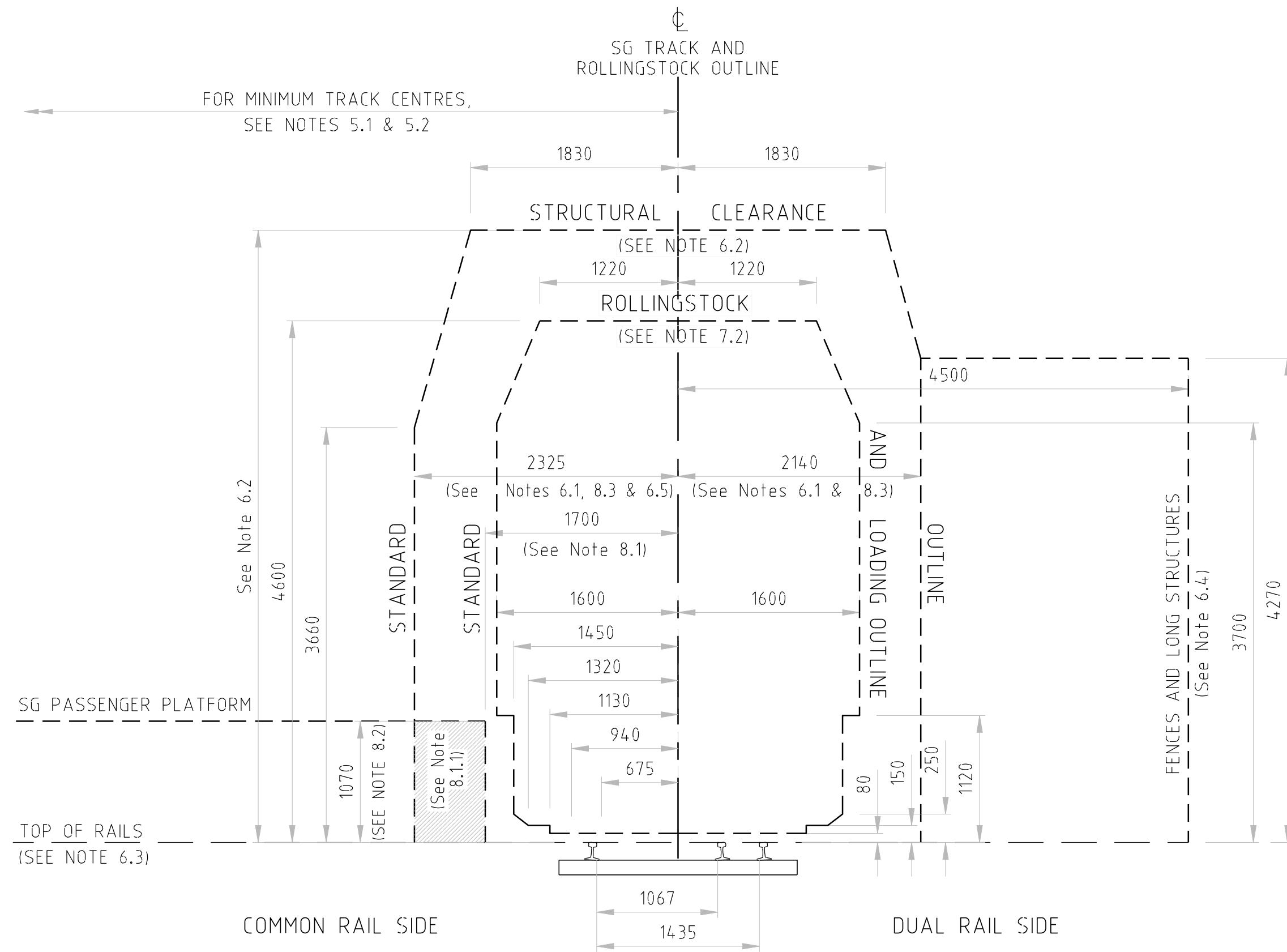
NOTES

1. All dimensions shown on this drawing are in mm.
2. For referenced notes refer drawing 00-C-04-0078
3. For Clearance and Rollingstock Outlines on Standard and Dual Gauge Lines refer drawing 00-C-04-0077
4. Refer to AS 7507, RISSB reference vehicle 13, 14 and 31 for Narrow Gauge vehicles

1	28.02.2018	ISSUED AS STANDARD	ZS	ZS	MK	RD
5	19.05.06	ISSUED FOR CONSTRUCTION	WPL	AWP	WPL	PM
REV	DATE	AMENDMENT	DSN	DRN	CHKD	APP
ORIG SIZE	A1					
<small>This document must not be copied without PTA's written permission, and the contents thereof must not be reported to a third party nor be used for any unauthorised purpose.</small>						

CAD DRAWING PATHNAME \\ptevwpob\je02\rend\lontemp\mp-4174-09614-9789927026\00-C-04-0076

REFERENCES	SCALE :	DESIGNED		CLEARANCES
	DATUM :	DRAWN		STANDARDS FOR URBAN NETWORK
PTA ACCEPTANCE STAMP A3335619	HORIZONTAL:	CHECKED	STRUCTURAL CLEARANCE AND ROLLINGSTOCK OUTLINES	
	VERTICAL:	APPROVED FOR ISSUE	NARROW GAUGE LINES	
DATE		MANAGER TRACK & STRUCTURES Network & Infrastructure	PTA Drawing No: 00-C-04-0076 REV : 1	



**EAST PERTH - MIDLAND RAILWAY
DUAL GAUGE STRUCTURAL & STANDARD GAUGE ROLLINGSTOCK OUTLINES**

NOTES

1. All dimensions shown on this drawing are in mm.
2. For referenced notes refer drawing 00-C-04-0078
3. For Clearance and Rollingstock Outlines on Narrow Gauge Lines refer drawing 00-C-04-0076
4. North Fremantle to Robb Jetty Railway - see note 7.1
5. Refer to AS 7507, RISSB reference vehicle 15 for Dual Gauge vehicles

						REFERENCES		SCALE : 1:25 (@ A1)	DESIGNED	<p align="center">CLEARANCES</p> <p align="center">STANDARDS FOR URBAN NETWORK STRUCTURAL CLEARANCE AND ROLLINGSTOCK OUTLINES STANDARD AND DUAL GAUGE LINES</p> <p>PTA Drawing No: 00-C-04-0077 REV : 1</p>
								DATUM :	DRAWN	
								HORIZONTAL:	CHECKED	
								VERTICAL:	APPROVED FOR ISSUE	
								PTA ACCEPTANCE STAMP A3335619	MANAGER TRACK & STRUCTURES Network & Infrastructure	
1	28.02.2018	ISSUED AS STANDARD	ZS	ZS	MK	RD				
5	19.05.06	ISSUED FOR CONSTRUCTION	WPL	AWP	WPL	PM				
REV	DATE	AMENDMENT	DSN	DRN	CHKD	APP				
ORIG SIZE A1				<small>This document must not be copied without PTA's written permission, and the contents thereof must not be reported to a third party nor be used for any unauthorised purpose.</small>						

FIGURE 12.5
METROPOLITAN BRIDGE HEIGHTS - EXISTING & PROPOSED



Route Description

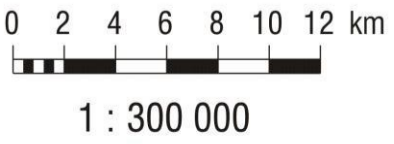
1. Railway Parade
2. Collier Rd
3. Iolanthe St
4. Walter Rd
5. Northmoor Rd
6. Morley Drive East
7. Lord St
8. Benara Rd
9. West Swan Rd
10. Great Northern Hwy

Route Description

1. Welshpool Rd
2. Hale Rd
3. Hawin Rd
4. Kalamunda Rd
5. Midland Rd
6. Bushmead Rd
7. Military Rd
8. Clayton St
9. Lloyd St
10. Elgee Rd
11. Ferguson St
12. Great Eastern Hwy

2018/19 UPDATE IN PROGRESS

BRIDGE HEIGHTS METROPOLITAN AREA
Existing Routes
Date: 30/4/2001



LEGEND

ROUTE

- Current
- 6.0 m
- 4.6 m
- 8.0 m

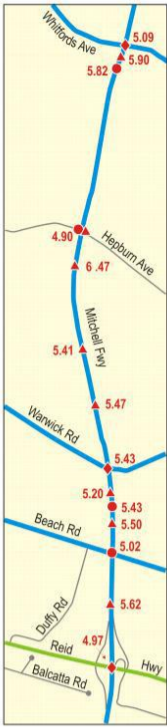
BRIDGES

- DIAMOND INTERCHANGE
- FOOT-BRIDGE

OTHER

- INDUSTRIAL AREAS
- FUTURE ROAD

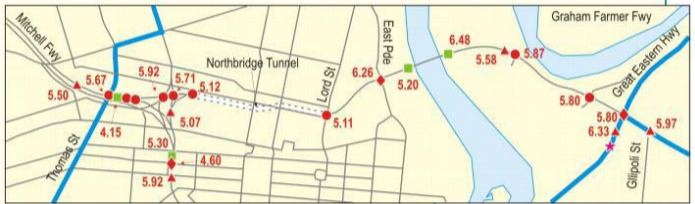
BRIDGE HEIGHTS METROPOLITAN AREA Future - Preferred Routes



DETAIL C
ENLARGEMENT NOT TO SCALE



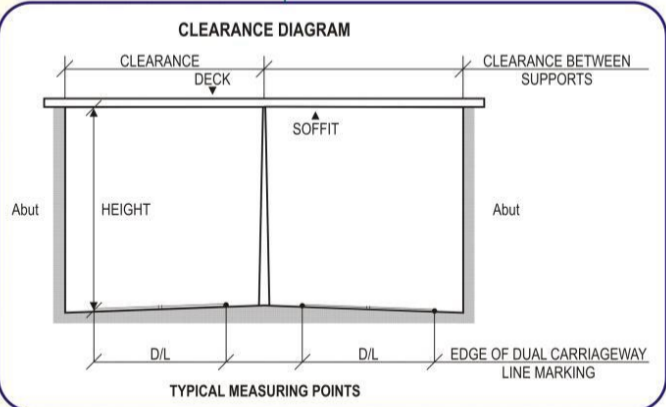
DETAIL B
ENLARGEMENT NOT TO SCALE



DETAIL A
ENLARGEMENT NOT TO SCALE



NOTES:
 * HIGH WIDE CORRIDOR TO Accommodate A TARGET LOAD OF 9.0m WIDE, 9.0m HIGH, 24.0m LONG AND A MASS OF 200 TONNES. EFFECTIVE HEIGHT CLEARANCE REQUIRED IS 10.0m.
 * MINIMUM HEIGHT CLEARANCE REQUIRED ON OTHER ROADS IS 5.3m.
 * INTERSECTIONS REQUIREMENT THAT CROSSING IS WHICH EVER WAY IS POSSIBLE.
 * PROJECT OWNER: BOB PETERS, CUSTODIAN: TONY KASPER (ph. 9311 8413).

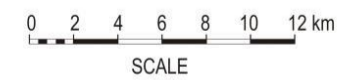


NOTES:
 1 Clearances are from maps and/or plans and have not been physically checked.
 2 Quoted clearances do not include any tolerance. Loaded vehicles should be at least 0.3 metres lower than normal bridges and 0.5 metres lower than footbridges.
 3 Under special conditions vehicles may be allowed a lesser tolerance when going under bridge.
 4 The major road is the one first listed in the far left list of roads.
 5 The current map shows existing routes and clearances.
 6 The proposed map shows what is needed, so that choke points can be identified and 'fixed'.

2018/19 UPDATE IN PROGRESS

LOOP ROAD	SUFFIX	COMMENTS
1 Tonkin	Hwy	
1 Roe	Hwy	
1 Reid	Hwy	
1 Brearley	Ave	
1 Great Eastern	Hwy	
1 Great Eastern Hwy Bypass	Hwy	
1 Great Northern	Hwy	
1 Welshpool	Rd	
1 Toodyay	Rd	
1 Wanneroo	Rd	
2 Leach	Hwy	
2 Port Beach	Rd	
2 Queen Victoria	St	
2 Tydemans	Rd	
3 Stirling	Hwy	
3 Cockburn	Rd	
3 West Coast	Hwy	
3 Marmion	Ave	
4 Perth-Bunbury	Hwy	
4 Albany	Hwy	
4 Thomas	Rd	
4 Anketell	Rd	
4 South Western	Hwy	
4 Armadale	Rd	
4 Brookton	Hwy	
5 Guildford	Rd	
6 Kwinana	Fwy	
6 Mitchell	Fwy	
6 City Northern Bypass	Hwy	
7 Karrinyup-Morley	Hwy	
8 Canning	Hwy	

Local names include Rockingham Rd, Paterson Rd, Ennis Ave, Mandurah Rd and Fremantle Rd
 Partly Local Government

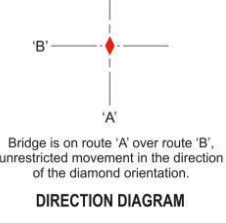


DRAFT:
 Internal Use Only
 Date: 8/8/2003

ROUTE	Clearance
Existing	
Proposed	10.0 m
Alternative	10.0 m (Alternative)
Future considerations	10.0 m (Future considerations)
	8.0 m
	6.0 m
	4.6 m

BRIDGES	Restricted movement	Unrestricted movement in the direction of diamond orientation (See Direction Diagram)	Footbridge
Existing	●	◆	▲
Proposed	●	◆	▲

BRIDGES	OTHER
Existing	■
Proposed	■
Sign gantry	★
Railway bridge over road	★
Industrial area	■



MAIN ROADS
 Western Australia

ASSET AND NETWORK INFORMATION

Perth & Pinjarra District
 Project: Asset & Network Information 2003
 Date: 8/8/2003
 Drawn by: [Name]
 Date of Print: Aug 2003

SECTION 13 – BRIDGE WATERWAYS INVESTIGATION AND FLOOD ESTIMATION

This information is Part 13 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Senior Waterways Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 15/08/18

Document No: 3912/02-13

SECTION 13

CONTENTS

13	BRIDGE WATERWAYS INVESTIGATION AND FLOOD ESTIMATION	3
13.1	Bridge Waterways Design Computer Programs	3
13.1.1	Introduction	3
13.1.2	HEC-RAS (River Analysis System).....	3
13.1.3	HEC-HMS (Hydrologic Modeling System)	3
13.1.4	HEC-SSP (Statistical Software Package)	4
13.1.5	RORB (Runoff Routing 'B')	4
13.1.6	TUFLOW.....	4
13.1.7	TUFLOW FLIKE	4
13.1.8	MIKEFLOOD.....	5
13.1.9	XP-STORM.....	5
13.1.10	XP-RAFTS.....	5
13.1.11	AFFLUX.....	5
13.1.12	CRC-FORGE FOR WESTERN AUSTRALIA.....	6
13.1.13	RFFE (Regional Flood Frequency Estimation Model).....	6

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	09/01/06	Complete review
All	2	15/08/18	Complete review for introduction of AS5100-2017

Custodian Endorsement

E. CHEUNG

A/Senior Waterways Engineer

Date: 15/08/18

13 BRIDGE WATERWAYS INVESTIGATION AND FLOOD ESTIMATION

13.1 Bridge Waterways Design Computer Programs

13.1.1 Introduction

This section contains a brief outline of some of the suitable and common waterways programs used for hydrological and hydraulic analyses to design bridges for Main Roads. A detailed manual is available for most of the programs giving full information on theoretical background, inputs and outputs.

The programs mentioned in this section are not exclusive. There are other waterways programs that are also suitable and acceptable for hydrological and hydraulic analyses to design bridges for Main Roads.

It is recommended that this section be read in conjunction with Austroads Guide to Bridge Technology Part 8 – Hydraulic Design of Waterway Structures – Section 3.6: Computer Modelling. Other sections in the Austroads Guide which are recommended for reading include Section 2.2: Estimation of Design Floods, Section 4.3: Analysis Methods, Section 4.4: 1D Bridge Hydraulic Analysis and Section 4.5: 2D Bridge Hydraulic Analysis.

13.1.2 HEC-RAS (River Analysis System)

This program can calculate water surface profiles for steady gradually varied flow in channels in a one dimensional (1D) model. Profiles may be calculated for both sub critical and super critical flow. The program can model obstructions such as bridges, culverts, weirs and levees. The computational procedure is based on the solution of the one dimensional energy equation with energy loss due to friction evaluated with Manning's Equation.

This program can also calculate water surface and velocity profiles for unsteady flow in channels and wider floodplains in a 1D, two dimensional (2D) and combined 1D/2D model. Full Shallow Water or Diffusion Wave equations may be selected for the computational procedure, where full Shallow Water is applicable to a wider range of problems and Diffusion Wave allows the program to run faster and have greater stability properties. Flows can be generated in the 2D model through hydrograph and direct rainfall inputs.

13.1.3 HEC-HMS (Hydrologic Modeling System)

This program simulates the hydrologic processes of watershed systems utilising traditional hydrologic analysis procedures including event infiltration, unit hydrographs, and hydrologic routing to generate hydrographs which can be input into hydraulic models. Advanced capabilities are available for gridded runoff simulation using the linear quasi-distributed runoff transform method (ModClark). Supplemental analysis tools are also available for model optimisation, forecasting streamflow, depth-area reduction, assessing model uncertainty, erosion and sediment transport, and water quality.

13.1.4 HEC-SSP (Statistical Software Package)

This program performs statistical analyses of hydrologic data and can calculate the expected probability curve and confidence limits of flood flow. The program can perform flood frequency analysis based on Bulletin 17B (Interagency Advisory Committee on Water Data, 1982), Bulletin 17C (England, et al., 2015) and also a generalised frequency analysis on not only flow data but other hydrologic data as well. Both Bulletin's recommend log-Pearson Type III distribution however Bulletin 17C advances in several areas including adopting the Expected Moments Algorithm and Multiple Grubbs Beck Test to address low outliers, and correcting confidence intervals for the flood frequency curve. It is recommended that the practitioner check that the results output from this program are in accordance with Australian guidelines.

13.1.5 RORB (Runoff Routing 'B')

This program is based on runoff routing concepts and is used for hydrological analysis of catchment areas to produce design hydrographs. The model is arially distributed, nonlinear, and applicable to both urban and rural catchments. The program has the capability of simulating storage and allows 'DESIGN' runs using design rainfall and temporal patterns to estimate design flows, or 'FIT' runs where actual rainfall events may be fitted to known flows in order to estimate catchment parameters. The program also has capability to vary parameters over sub-catchments and carry out batch runs and Monte Carlo simulations.

13.1.6 TUFLOW

This program can calculate water surface and velocity profiles in channels and wider floodplains in a 1D, 2D and combined 1D/2D model. It is ideally suited to modelling flooding of rivers and creeks with complex flow patterns, overland and piped flows through urban areas and coastal scenarios. The program can model obstructions such as bridges and culverts in 1D models, and also in 2D models provided that the flow width of the structure is of similar or larger size than the 2D cell size. The 1D Solver utilises the Saint-Venant equations and the 2D implicit solver is based on Stelling (1984) and Syme (1991) and solves the full two-dimensional, depth averaged, momentum and continuity equations for free-surface flow. The models can be run using several engines including Classic, HPC (Heavily Parallelised Compute) and FV (Finite Volume) to optimise run times and obtain results as appropriate.

13.1.7 TUFLOW FLIKE

This program calculates the probability of flood events based on historical records to calculate the expected probability curve and confidence limits of flood flow. The primary purpose of the program is to carry out flood frequency analysis however it can be applied to extreme value analysis. A range of probability models distributions can be applied to the analysis. The program uses the Bayesian inference methodology which allows the ability to use historic data outside of the gauged record, incorporate the multiple Grubbs-Beck test for low outliers and incorporate regional information as prior knowledge.

13.1.8 MIKEFLOOD

The MIKEFLOOD package contains several 1D and 2D simulation engines which can model rivers, open channels, sewer and drainage networks, and overland flow. These engines can be coupled with one another to create an integrated model to calculate water surface and velocity profiles in channels and wider floodplains. The program can model obstructions such as bridges, culverts and weirs. The package can also be used to design and assess coastal structures, offshore structures, dams and environmental flood impacts. The 2D component of MIKEFLOOD, MIKE 21 HD, is a general numerical modelling system that utilises the conservation of mass and momentum integrated over the vertical equations to describe flow and water level variations. Run times can be optimised by enabling parallel 2D engines.

13.1.9 XP-STORM

This program can simulate stormwater and river flows using models comprising of 1D channels and pipes coupled to a 2D surface grid. All hydrologic processes including snowmelt, evaporation, infiltration, surface ponding and ground-surface water exchanges can be included in the model. Rainfall can be selected through design storms or actual recorded rainfall events, and the program provides numerous methods for computing runoff from the rainfall. This program utilises the Saint-Venant equation as the hydraulic computational procedure in 1D models to calculate backwater effects, flow reversal and surcharging. The program can model obstructions and control structures such as bridges, culverts, and detention basins in the 1D model. The 2D modelling package incorporates the TUFLOW engine into the XP graphical interface.

13.1.10 XP-RAFTS

This program may be used to simulate runoff hydrographs at defined points throughout a watershed for a set of catchment conditions and rainfall events and is suitable for application on both rural and urbanised catchments of all sizes. The watershed can be divided into a number of sub-catchments and storage both small and large in volume may be assigned to nodes. Rainfall events can be generated from Intensity-Frequency-Duration data together with storm temporal patterns or standard pre-set storm data. The program uses the Laurenson non-linear runoff routing procedure to develop hydrographs and a number of loss models can be selected to calculate rainfall excess.

13.1.11 AFFLUX

This program carries out surface water analysis in channels based on Manning's Equation and also computes backwater as a result of obstructions. The program models the natural stream properties and superimposes a bridge template over this natural stream. The bridge template includes information such as deck level, abutment chainages, abutment type, number of piers and skew. Scour and floodways may also be added to the model. Outputs from this program consists of discharge, velocities and backwater height for each specified stage height. It is recommended that this program only be considered for simple scenarios of bridges operating with or without floodways.

13.1.12 CRC-FORGE FOR WESTERN AUSTRALIA

This tool is a regional frequency analysis method used for estimating large to rare rainfalls in Western Australia. This method is based on the concept that additional information can be gained by pooling standardised data from a number of rainfall sites at a regional scale and standardised. Growth curves of design rainfalls are generated by plotting at-site data and pooling additional data from rainfall sites within areas of increasing size to estimate rainfalls with decreasing Annual Exceedance Probabilities (AEP). A seasonal approach to extreme flood estimation has specifically been adopted for Western Australia due to rainfall characteristics evident in this state.

13.1.13 RFFE (Regional Flood Frequency Estimation Model)

This model calculates discharge and provides confidence limits based on catchment location and characteristics using data from relevant gauged catchments. The application of this model is most relevant in ungauged catchment scenarios. This model provides an approach which is consistent nationally and smooths discrepancies at state boundaries which previously existed. The Region of Influence approach is adopted to iteratively determine the lowest prediction error and maximise the regression model predictive skill. The reliability of results is highly dependent on data availability and quality. This model is recommended in the Australian Rainfall and Runoff 2016 guidelines for ungauged catchments and the practitioner must recognise and understand the limitations of this model prior to using it.

There is no specific program to calculate discharge using the regional methods in the Australian Rainfall and Runoff 1987 guidelines, however it is noted that Main Roads currently still recommends practitioners carry out these calculations in conjunction with the RFFE model.

SECTION 14 – STRUCTURAL DESIGN AND ANALYSIS SOFTWARE

This information is Part 14 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 16/04/18

Document No: 3912/02-14

SECTION 14

CONTENTS

14	BRIDGE STRUCTURAL DESIGN COMPUTER PROGRAMS	3
14.1	INTRODUCTION	3
14.2	ACES	3
14.3	COLDES.....	3
14.4	CONKS.....	4
14.5	CSI BRIDGE	4
14.6	GRLWEAP.....	4
14.7	HLR	4
14.8	LIMSTEEL	4
14.9	LOADIST	4
14.10	MULTBEAM	4
14.11	PARTIAL.....	5
14.12	PCBEAMAN	5
14.13	PIGLET.....	5
14.14	RETWALL	6
14.15	SPACEGASS	6
14.16	STLBEAM.....	6
14.17	STRUCTURAL BRIDGE DESIGN	6
14.18	TIMBAR.....	6

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	13/12/05	Complete review for introduction of AS 5100-2004
All	2	13/04/18	Complete review for introduction of AS 5100-2017

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 13/04/18

14 BRIDGE STRUCTURAL DESIGN COMPUTER PROGRAMS

14.1 INTRODUCTION

This Section contains a brief outline of structural design and analysis software programs normally used within Main Roads.

Structures Engineering prefers to receive computer models prepared using the below programs so that the models can be used internally if required.

For full information on input, output and theoretical background, refer to program user guides and manuals.

14.2 ACES

This is a general structural analysis software package performing linear elastic static analysis. Applications include 2 and 3 dimensional frames, grillage and finite element analysis of plane, plate and shell structures.

ACES-BEAM provides a continuous bridge beam module for linear elastic analysis with any span configuration.

ACES Incremental Launching module calculates and displays effects of an incrementally launched girder, using an iterative linear-elastic analysis.

ACES Section Properties module allows properties to be calculated of an arbitrary shaped section, including hollow sections, and sections with a number of voids.

The basic input is composed of the following:

- Geometry of the structure - defined by a series of nodes, connected by members or elements.
- Physical properties of all members and/or elements.
- Location and types of support (rigid or elastic).
- Load data, including self-weight, temperature, differential settlement and traffic load. The program has several in-built AS 5100, Bridge Design (CODE) traffic vehicles and facility to set-up standard vehicles for load application.

Output consists of all nodal, member and/or element displacements and forces (moments, shear and reactions). The program has graphical facilities for mesh generation, vehicle loadings, to validate input data and to plot output information.

14.3 COLDES

This program performs section analysis and assists with the design of 'short' reinforced concrete columns. It calculates the ultimate strength, ultimate balanced strength and minimum reinforcement to take the applied axial and/or bending moment, and plots the axial-bending moment interaction diagram. Torsion and shear are not considered.

It also provides a screen plot of the section to enable checking of input data and axial-bending moment interaction diagram to enable selection of a suitable column.

14.4 CONKS

This program carries out a cracked section analysis of reinforced and prestressed concrete under serviceability and ultimate moments.

Output gives the ultimate moment capacity of the section plus concrete and steel stresses under serviceability moments.

14.5 CSI BRIDGE

This is an advanced software package produced by Computers & Structures Inc. for use in more complex projects. Useful for analysis, design, load rating and reporting.

14.6 GRLWEAP

A program for analysing dynamic pile driving response. Inputs consist of soil profile (shear modulus), pile details (weight, length material etc), hammer (rated energy, weight of ram, type etc). Outputs are pile driving response, set, pile stresses etc.

The program is useful in selecting the appropriate pile driving hammer, helmet, packing material etc to achieve the nominated pile capacity, and to design the pile for driving conditions.

14.7 HLR

HLR is a computer program to enable indicative assessment of load-carrying capacity of bridge structures and to monitor passage of heavy vehicles on a defined road network.

14.8 LIMSTEEL

Interactive design of steel members to AS 4100.

14.9 LOADIST

This program interactively performs Guyon-Massonet analysis of an orthotropic simply supported bridge superstructure. The analysis is linear elastic. It is used for determining the distribution of longitudinal moments due to traffic load in a multi-beam bridge structures. MRWA only recommends its use for distribution factor comparative analysis.

14.10 MULTBEAM

Transverse distribution of longitudinal movements in linked plank bridges. Cannot input specific vehicles but good as a check for distribution factors from ACES.

14.11 PARTIAL

This program analyses partially prestressed continuous beams. It will allow for non-linear effects due to differential temperature gradient and shrinkage with cracking, plasticity and creep of both concrete and steel. Because of the general nature of the analysis it will also handle reinforced and fully prestressed beams and columns and analyse effects due to constructing staging.

Input consists of:

- Definition of structure - the beam must be subdivided into a number of sections longitudinally and the cross-section modelled as a number of layers with specified width and thickness.
- Definition of steel.
- Applied external loads, prestress forces, sequence of construction/staging, etc.

Output gives a prestress friction analysis, the deflected shape of the beam, moments and shears. The stresses and strains in each layer of steel and concrete can also be obtained at selected sections.

The program uses an iterative method of analysis aimed at achieving equilibrium throughout the structure under the given loading conditions and material's stress-strain relationship.

14.12 PCBEAMAN

This program performs linear elastic analysis of a continuous beam with any span configuration. It allows for varying moment of inertia, construction staging of a multi-stage bridge and composite section (beam and slab acting together).

Input is composed of the span configuration, section properties (moment of inertia, area, etc), details of construction staging if necessary and the applied external loads. The program has several in-built live loads including NAASRA traffic vehicles, and facility to enable setting-up of a user defined vehicle for load application. The program also has an in-built differential settlement facility.

Output gives the bending moments, shear forces, deflections and normal and shear stresses at the specified or result points and reactions of supports. The result can be presented in table format and/or graphically. The graphical viewing enables determination of position of a live load for maximum moment, shear or deflection and enables assessment of the variation of bending moments, shears and deflections caused by a moving live load.

14.13 PIGLET

This program analyses the load/deformation response of a pile group under general loading conditions.

Input consists of data on the pile group, soil parameters and loading. The pile cap is assumed to be rigid, with the piles pinned or fixed to the pile cap. The group may contain up to 85 piles, which can be vertical or raked in any direction. Coordinates and structural data are required. The only soil parameters necessary are Poisson's

ratio and a shear modulus profile with depth. Only linear profiles are permissible. Loading may be general 3-D loads to the pile cap or individual piles or imposed deformations to the pile cap or individual piles.

Both a full and a summarised output are available. The "slimline" output gives the forces and moments in each pile and deformations of the pile cap. Full output gives the response of the group to unit deformations of the pile cap and overall stiffness and flexibility matrices for the group.

Analysis is based on a number of approximate, compact solutions for the response of single piles, with due allowance for interaction effects. The soil is assumed to behave as a linear elastic medium.

14.14 RETWALL

Interactive design of concrete retaining walls.

14.15 SPACEGASS

General purpose frame analysis program.

14.16 STLBEAM

STLBEAM performs static elastic analysis of a prismatic continuous bridge using a Fourier Transform of loading and support conditions. The analysis is based on harmonic folded plate theory. Applications include analysis of steel, concrete or composite bridge superstructures, particularly box girders.

The structure must be square at the abutments and prismatic. The structure is modelled as a collection of folded plates which may be isotropic or orthotropic. Longitudinal beam members can also be included in the assembly. Internal supports can be rigid or elastic, but only knife-edge supports are allowed at the abutment.

Advantages of STLBEAM over finite element programs are in the speed of modelling (using the graphic user interface and vehicle load generation) and the accuracy and speed of the analysis for transverse effects of vehicle loadings.

Results can be selected interactively for viewing and plotting. The output includes moments, forces plate stresses, displacements, etc.

14.17 STRUCTURAL BRIDGE DESIGN

This is an advanced software package produced by Autodesk for use in more complex projects. Useful for analysis, design, load rating and reporting.

14.18 TIMBAR

An interactive program using an ACES analysis engine for the rating and refurbishment design of timber bridges.

SECTION 15 – INVENTORY INFORMATION

This information is Part 15 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Bridge Condition Manager is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 16/04/18

Document No: 3912/02-15

SECTION 15

CONTENTS

15 INVENTORY INFORMATION	3
15.1 Purpose	3
15.2 Scope	3
15.3 References	3
15.4 Definitions	3
15.5 Procedure	4
15.6 Inventory Form Guidance.....	4

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
1 to 10	1	25/10/04	Section 15 revised including the incorporation of the revised Section 16.
3, 5, 6, 11 & 12	2	28/10/05	Attachment 5 - General Bridge Inventory Information Amended. Attachment 4 - Tunnel Inventory Information form added.
All	3	14/12/05	Complete review for introduction of AS 5100
5-8, 11 & 12	4	22/06/06	Amended General Bridge, Culvert and Tunnel Inventory forms
5-12	5	13/01/12	Amended General Bridge, Culvert and Tunnel Inventory and Construction Information Forms
All	6	12/04/18	Complete Review

Custodian Endorsement

G. Johnston
Bridge Condition Manager
Date: 12/04/18

15 INVENTORY INFORMATION

15.1 Purpose

This Section defines the extent of information to be supplied for the Main Roads Bridge Inventory System to allow for efficient management of the State's infrastructure.

15.2 Scope

This Section shall be followed as part of the completion of the design of any bridge, tunnel, or culvert replacing an existing bridge, within or over a public road within WA.

15.3 References

This Section is provided for reference by the following Procedures of the Structures Engineering Management System Document 3912/01:

- Procedure for the Management of Bridge Data & Information 3912/01/04
- Procedure for the Design of Structures 3912/01/05
- Procedure for Design Review 3912/01/11
- Procedure for Updating Bridge Inventory and Construction Information 3912/01/12

15.4 Definitions

IRIS - Integrated Road Information System, which contains a database of inventory for each bridge from information supplied in accordance with this Section.

Designer - The person with sufficient knowledge of the design of the bridge to be able to provide the required information accurately.

Project Manager - Generic title referring to the person responsible for the delivery of the structural project.

Ownership – The Owner in IRIS is defined as the party responsible for maintenance, not the party that owns the asset.

Tunnel - A structure is defined as a Tunnel where its principal function provides access for road or rail and is generally buried within and surrounded by soil. Pedestrian and fauna under/overpasses are not recorded as tunnels in IRIS.

Rail Carriage – A superstructure formed using the undercarriage of a rail car.

Other Composite Steel Beams & Concrete Deck – This is for structures that are not composite I-beams, box girders, cable stayed or rail carriage. The only occurrence at time of writing is Third Avenue Bridge 905A, which embeds fabricated steel boxes into structural concrete band-beams.

Inverted U-beam – This refers to all U-beams that are not Rocla M-Lock Precast Bridge U-beams.

Solid Slab Reinforced with Steel Beams – this is a concrete slab with cast-in beams, typically spare or re-purposed rail beams, not designed for composite action.

Pavement Type – Refer to Appendix A of the Detailed Visual Bridge Inspection Guidelines for Timber Bridges (Level 2 Inspections).

Surface Type – Refer to Appendix A of the Detailed Visual Bridge Inspection Guidelines for Timber Bridges (Level 2 Inspections).

Delineation post – typically a plastic post with reflective marker.

Visibility Barrier – A continuous barrier that does not offer appropriate performance under vehicle impact.

15.5 Procedure

The process for collecting and providing inventory information to Structures Engineering is managed through:

- 1) Complete the appropriate inventory form at a time when the design, including drafting, may be reasonably deemed to be complete and final. Inventory forms are available on the public Main Roads Western Australian website via Building Roads, Standard and Technical, Structures Engineering, Asset Management, [Inventory Forms \(link\)](#).
- 2) The Regional Asset Manager Structures shall ensure that these Attachments are promptly sent to StructEngReviews@mainroads.wa.gov.au.

15.6 Inventory Form Guidance

- General Bridge Inventory

The General Bridge Inventory form shall be completed for all new structures, replacement structures and bridge refurbishments wherein either the bridge geometry or bridge type is changed.

- Sign Gantry Inventory

The Sign Gantry Inventory Form shall be completed for any overhead structure spanning, or partially spanning (if cantilevered), a road carriageway for the specific purpose of carrying regulatory, advisory, warning, variable message (VMS) or directional sign.

- Culvert Inventory Information

The Culvert Inventory Information form shall be completed for any culvert that replaces a numbered bridge.

- Tunnel Inventory Information

The Section 15.4 definition of a tunnel should be used to confirm whether the Tunnel Inventory Information form or General Bridge Inventory form is applicable.

SECTION 16 – HISTORICAL DESIGN AND LOAD RATING VEHICLES

This information is Part 16 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

Structures Asset Policy Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.



Adam Lim
SENIOR ENGINEER STRUCTURES

Date: 18/08/2021

Document No: 3912/02-16

SECTION 16

CONTENTS

16	HISTORICAL DESIGN AND LOAD RATING VEHICLES.....	3
16.1	INTRODUCTION	3
16.2	HISTORICAL DESIGN VEHICLES.....	3
16.2.1	1965 Highway Bridge Design Specification (NAASRA).....	3
16.2.2	1970 Highway Bridge Design Specification (NAASRA).....	7
16.2.3	1973 Highway Bridge Design Specification (NAASRA) Metric Version	7
16.2.4	1973 MRWA Road Train and Abnormal Vehicle	10
16.2.5	1976 NAASRA Bridge Design Specification.....	11
16.2.6	1989 MRWA Bridge Design Manual Road Train	14
16.2.7	1992 Austroads Bridge Design Code.....	15
16.2.8	1998 MRWA Bridge Branch Design Information Manual Standard Road Trains	18
16.2.9	1999 MRWA NRTC Vehicles.....	19
16.2.10	1999 MRWA Interim Bridge Design Loads	20
16.2.11	2004 Australia Standard Bridge Design AS5100	22
16.3	HISTORICAL LOAD RATING VEHICLES	23
16.3.1	1993 MRWA Bridge Branch Design Information Manual	23
16.3.2	1993 MRWA Load Rating Vehicles	25
16.3.3	1995 MRWA Bridge Branch Design Information Manual	27

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	18/08/2021	Review and update against AS5100 2017, Include historical vehicles cited by AS5100.7 2004, which are not included in AS5100 2017

Custodian Endorsement

Jewely Parvin
Structures Asset Policy Engineer
Date: 18/08/2021

16 HISTORICAL DESIGN AND LOAD RATING VEHICLES

16.1 INTRODUCTION

This Section of the Manual shall be used to determine the load capacity of existing steel and concrete bridges in Western Australia (WA) from historical design vehicles and load rating vehicles.

The aim of load rating analysis is to determine the theoretical capacity of a bridge by calculating what proportion of different vehicles it can carry. These values are used for the assessment of heavy haulage movements throughout the State.

Section 16 has been prepared to provide details of historical vehicles that bridges may have been designed or load rated for that are no longer in current CODES or in Section 4 of this Manual. Comparisons can then be made between these vehicles and current rating vehicles to assist in the assessment of heavy vehicles. For more details, user needs to look at old codes.

16.2 HISTORICAL DESIGN VEHICLES

16.2.1 1965 Highway Bridge Design Specification (NAASRA)

- Type of Code – Working stress

Truck and Lane Loads

- Live Loads – Standard trucks or lane loads corresponding to truck trains. H loadings and H-S loadings (as below)
- Design Traffic Lane Width – 10-ft
- Number of design lanes

Width between kerbs (feet) Excludes median widening and road curvature widening	Number of Design Traffic Lanes
over 20-30 incl.	2
over 30-42 incl.	3
over 42-54 incl.	4
over 54-66 incl.	5
over 66-78 incl.	6
over 78-90 incl.	7
over 90-102 incl.	8
over 102-114 incl.	9
over 114-126 incl.	10

- Location – One vehicle per design lane applied anywhere on the structure
- Lane Reduction Factors –

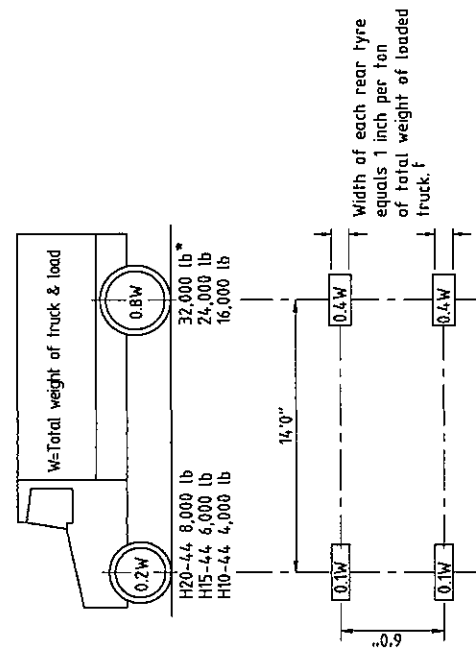
1 or 2 lanes	100%
3 lanes	90%
≥4 lanes	75%
- Overload provision – Provision for overload shall be made by applying in any

single lane an H or HS truck as specified, increased 100 per cent, and without concurrent loading of any other lanes. Combined dead, live and impact stresses resulting from such loading shall not be greater than 150 per cent of the allowable stresses allowed herein. The overload shall apply to all parts of the structure affected, including stringers, but excluding portions of the structure affected by individual wheel loads only.

- Dynamic Load Allowance - $DLA = \frac{5000}{L+125} \%$ where L = span length in feet
(more details are available in code for L)

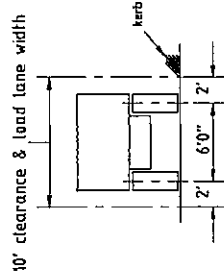
Max. 30% and Min. 10%

Note: Not applicable to foundations, piles not rigidly connected to the superstructure, retaining walls, footways, timber structures and structures carrying more than 3ft of fill



Width of each rear tyre equals 1 inch per ton of total weight of loaded truck.†

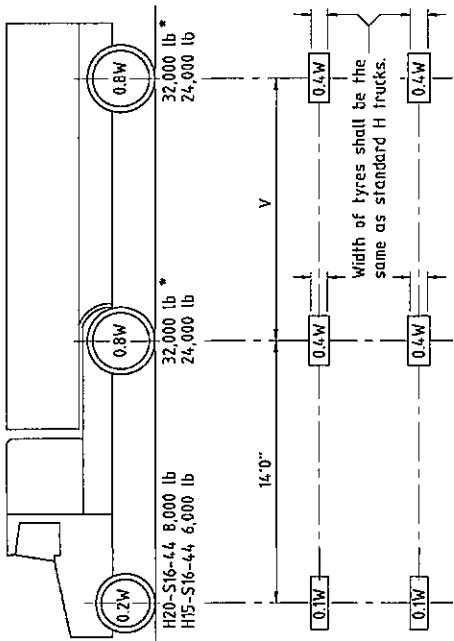
Length of contact of tyre with deck = 4" for front wheel.
8" for rear wheel.



STANDARD H TRUCKS

* In the design of steel grid & timber decks only, for H20 loading, one axle load of 24,000 lb. or axle loads of 16,000 lb each spaced 4 ft. apart shall be used, whichever produces the greater stress, instead of the 32,000 lb. axle shown. Concrete slabs shall be designed for the 32,000 lb. axle.

† Ton here means a weight of 2,000 lb.

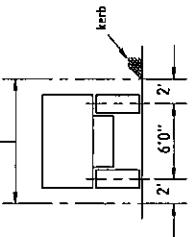


W= Combined weight on the first two axles which is the same as for the corresponding H truck.
V= Variable spacing - 14ft to 30ft, inclusive, spacing to be used is that which produces maximum stresses.

Length of contact of tyre with deck = 4" for front wheel.
8" for rear wheel.

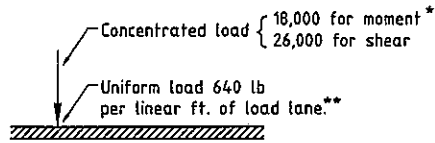
Width of tyres shall be the same as standard H trucks.

10' clearance & load lane width

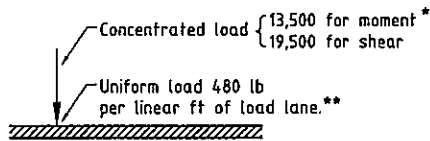


STANDARD HS TRUCKS

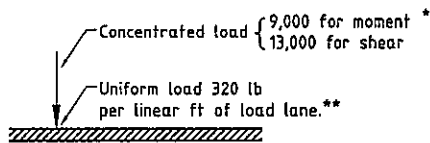
* In the design of steel grid & timber decks only, for H20-S16 loading, one axle load of 24,000 lb. or two axle loads of 16,000 lb each spaced 4 ft. apart shall be used, whichever produces the greater stress, instead of the 32,000 lb. axle shown. Concrete slabs shall be designed for the 32,000 lb. axle.



H20-44 Loading
H20-S16-44 Loading



H15-44 Loading
H15-S12-44 Loading



H10-44 Loading

H LANE & HS LANE LOADINGS

** To follow or precede, or be on both sides of the concentrated loads to produce the maximum stress.

* NOTE: For the loading of continuous spans involving lane loading, an additional concentrated load shall be placed in or other span in such a position as to produce maximum negative moment.

16.2.2 1970 Highway Bridge Design Specification (NAASRA)

No changes from 1965 Highway Bridge Design Specification (NAASRA)

16.2.3 1973 Highway Bridge Design Specification (NAASRA) Metric Version

- The content of the 1973 NAASRA Code is the same as the 1965 and 1970 versions except with minor numerical differences introduced during the conversion from imperial to metric. Note also that H and HS were renamed to M and MS.
- Type of Code – Working stress

Truck and Lane Loads

- Live Loads – Standard trucks or lane loads corresponding to truck trains. M loadings and MS loadings (as below)
- Design Traffic Lane Width – 3.0m
- Number of design lanes

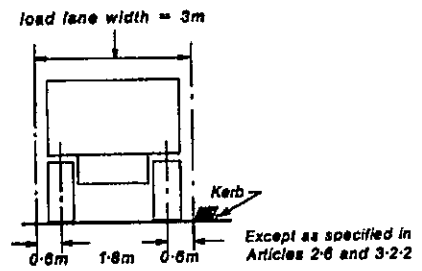
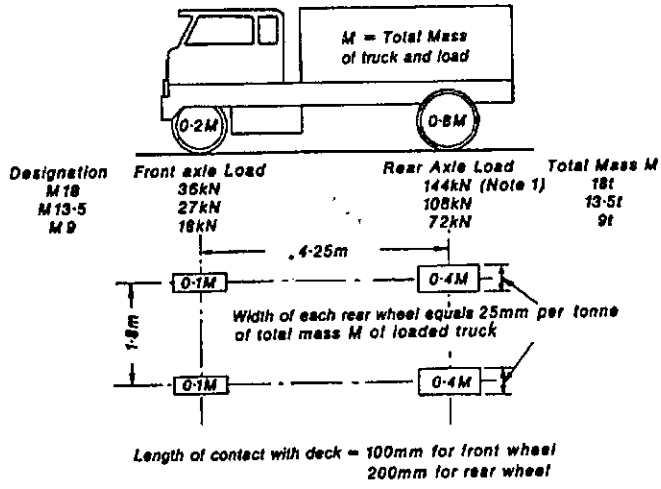
Width between kerbs (metres) Excludes median widening and road curvature widening	Number of Design Traffic Lanes
over 6 to 9 incl.	2
over 9 to 12.7 incl.	3
over 12.7 to 16.4 incl.	4
over 16.4 to 20.1 incl.	5
over 20.1 to 23.8 incl.	6
over 23.8 to 27.5 incl.	7
over 27.5 to 31.2 incl.	8
over 31.2 to 34.9 incl.	9
over 34.9 to 38.6 incl.	10

- Location – One vehicle per design lane applied anywhere on the structure
- Lane Reduction Factors –

1 or 2 lanes	100%
3 lanes	90%
≥4 lanes	75%
- Overload provision – Provision for overload shall be made by applying in any single lane an H or HS truck as specified, increased 100 per cent, and without concurrent loading of any other lanes. Combined dead, live and impact stresses resulting from such loading shall not be greater than 150 per cent of the allowable stresses allowed herein. The overload shall apply to all parts of the structure affected, including stringers, but excluding portions of the structure affected by individual wheel loads only.
- Dynamic Load Allowance – $DLA = \frac{1600}{L+40} \%$ where L = span length in metre
(More details are available in code for L)

Max. 30% and Min. 10%

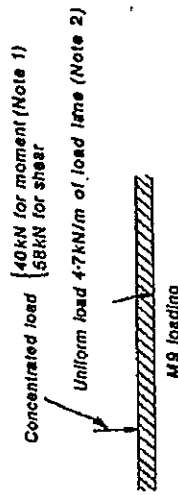
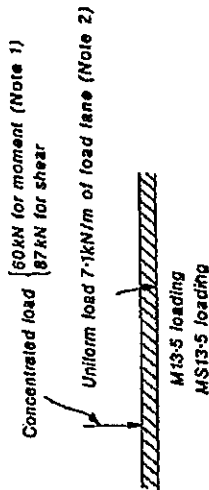
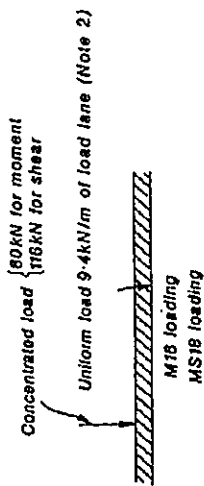
Note: Not applicable to foundations, piles not rigidly connected to the superstructure, retaining walls, footways, timber structures and structures carrying more than 3ft of fill



NOTES

1. In the design of steel grid and timber decks only, for M 18 loading, one axle load of 108 kN or two axle loads of 72 kN each spaced 1.2 m apart shall be used, whichever produces the greater stress, instead of the 144 kN axle shown. All other deck systems shall be designed for the 144 kN axle. (The reason for the use of reduced loading on timber and steel grid decks is the ease and relative economy with which they can be replaced.)

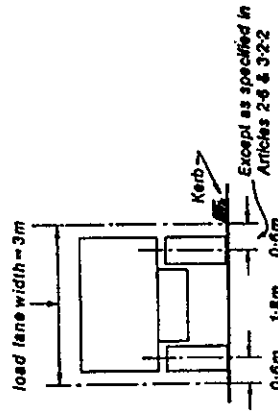
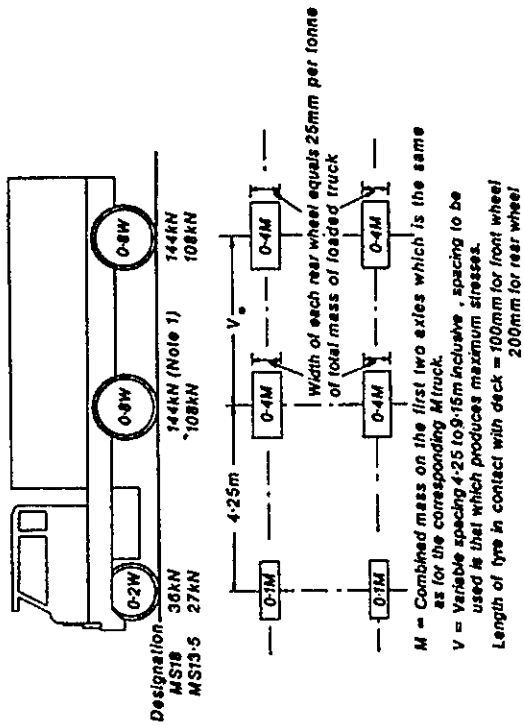
STANDARD M TRUCKS



NOTES

1. For the loading of continuous spans involving lane loading an additional concentrated load of equal weight shall be placed in one other span in such a position as to produce maximum negative moment.
2. To follow or precede, or be on both sides of the concentrated loads to produce the maximum stress.

M LANE & MS LANE LOADINGS



NOTES

1. In the design of steel grid and timber decks only, for MS18 loading, one axle load of 108 kN or two axle loads of 72 kN each spaced 1.2 m apart shall be used, whichever produces the greater stress, instead of the 144 kN axle shown.
- All other deck systems shall be designed for the 144 kN axle. (The reason for the use of reduced loading on timber and steel grid decks is the ease and relative economy with which they can be replaced)

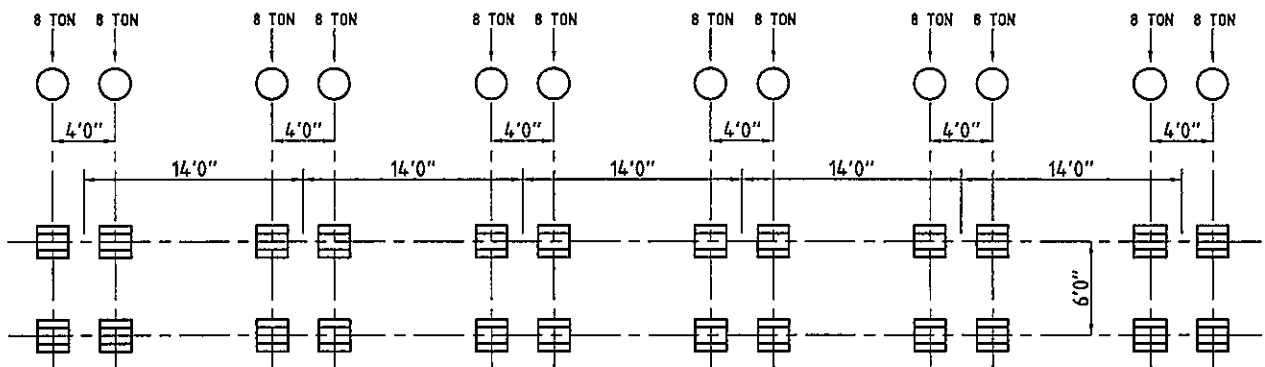
STANDARD MS TRUCKS

16.2.4 1973 MRWA Road Train and Abnormal Vehicle

- Type of Code – Working stress

Road Train

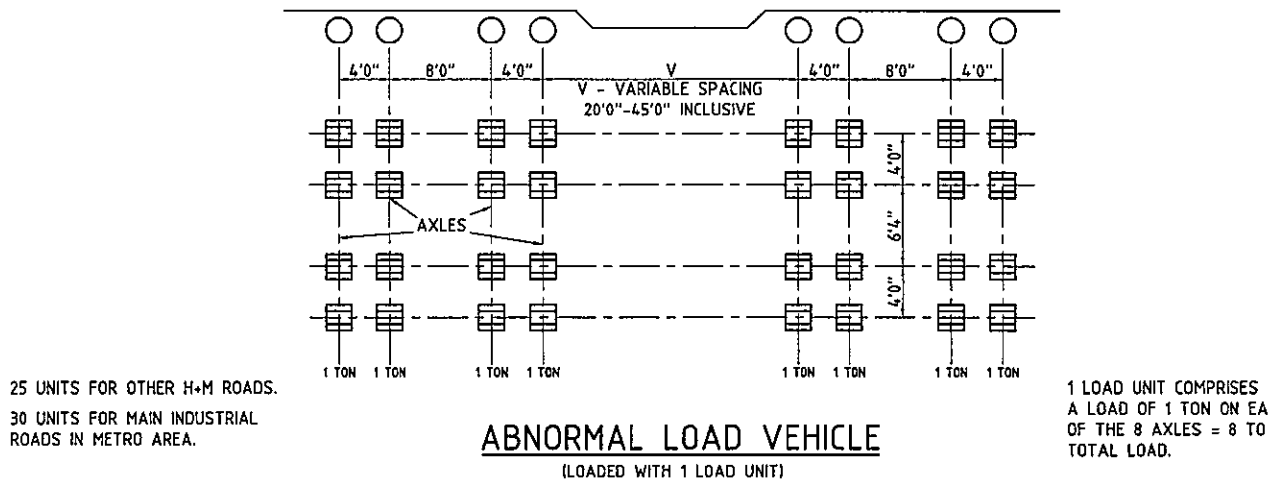
- Live Load – Road Train (as below)
- Design Lane Width – N/A
- Location – One vehicle per bridge applied anywhere on the structure without concurrent loading
- Lane Reduction Factors – N/A
- Dynamic Load Allowance – $DLA = \frac{5000}{L+125} \%$ where L = span length in feet
Max. 30% and Min. 10%



ROAD TRAIN

Abnormal Vehicle

- Live Load – Abnormal Load Vehicle (as below)
- Design Lane Width – N/A
- Location – One vehicle per bridge applied centrally without concurrent loading
- Lane Reduction Factors – N/A
- Dynamic Load Allowance – DLA = 10%



16.2.5 1976 NAASRA Bridge Design Specification

- Type of Code – Working stress

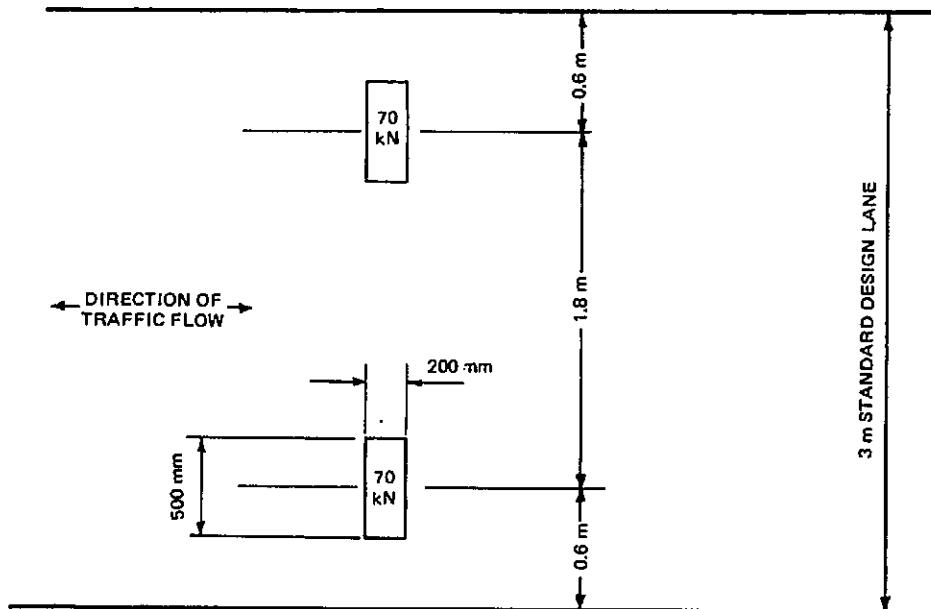
Vehicle Load for Spans Less than or Equal to 4m

- Live Load - A14 Standard Vehicle Loading (as below)
- Design Traffic Lane Width – 3.0m
- Number of design lanes, $n = \text{width between kerbs} / 3.1$
- Location – One axle per design lane applied anywhere on the structure.
- Lane Reduction Factors –

1 or 2 lanes	100%
3 lanes	90%
≥ 4 lanes	75%
- Dynamic Load Allowance – $DLA = \frac{1600}{L+40} \%$ where $L = \text{span length in metre}$
(more details are available in code for L)

Max. 30% and Min. 10%

Notes: DLA = 30% for culverts with cover $\leq 300\text{mm}$ and for cantilevers
 = 20% for culverts with cover $> 300\text{mm}$ and $\leq 600\text{mm}$
 = 10% for culverts with cover $> 600\text{mm}$ and $\leq 1.0\text{m}$
 = 10% for Abnormal vehicles



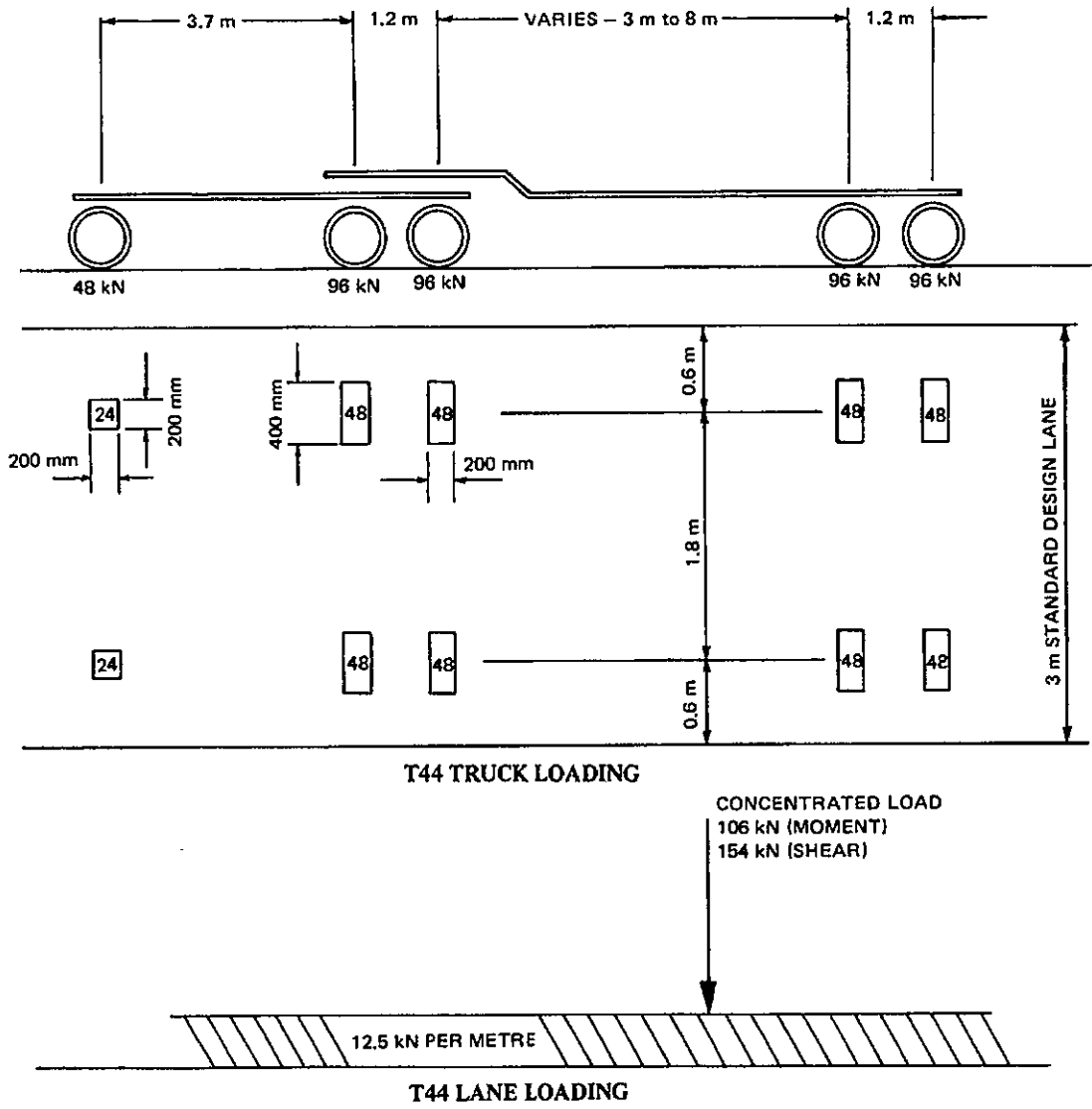
NOTES

1. Total mass on axle is 14.3 tonnes (figure shows loads).
2. In designing the deck system for local effects, the wheel nearest the kerb may be placed with its centre 0.3 m from the kerb face.
3. In continuous spans, for the calculation of maximum negative bending moment, an additional axle of similar weight and configuration shall be placed in the design lane so that the axle spacing is 4.25m

A14 STANDARD VEHICLE LOADING

Vehicle Load for Spans Equal to or Greater than 5m

- Live Load - T44 truck or lane loading (as below)
- Note: Lane loading applies to spans of 10m or greater only.
- Design Lane Width – As A14 above
- Location – One truck load or lane load per design lane applied anywhere on the structure. The lane loading shall be continuous or discontinuous.
- Lane Reduction Factors – As A14 above
- Dynamic Load Allowance – As A14 above



NOTES

1. Total mass of vehicle is s 44 tonnes (figure shows loads).
2. For continuous spans the lane loading shall be continuous or discontinuous as may be necessary to produce maximum effects, and an additional concentrated load shall be placed in one other span in such a position as to produce maximum negative moment.
3. The T44 lane loading shall be considered as uniformly distributed over the width of the standard design lane.

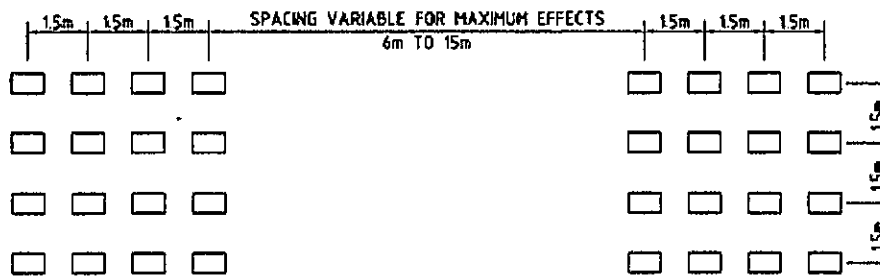
T44 STANDARD VEHICLE LOADING

Vehicle Load for Spans Between 4 & 5m

- Live Load – Interpolate A14 & T44. Design effect = $A14 + (T44 - A14)(span - 4)$

Abnormal Load

- Live Load – Standard Abnormal Vehicle and MRWA 205 & 245 tonne variants (as below)
- Design Lane Width – N/A (loads not applicable for width between kerbs less than 6m)
- Location – One vehicle per bridge applied centrally without concurrent loading
- Lane Reduction Factors – N/A
- Dynamic Load Allowance – DLA = 10%



STANDARD ABNORMAL VEHICLE

Plan of Wheel Positions

NOTES

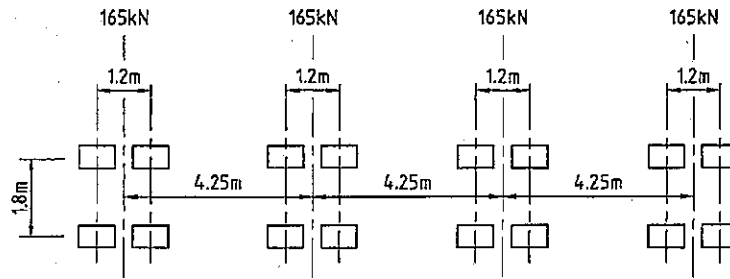
1. Load Per wheel = 60kN
2. Load Per axle = 240kN
3. Total mass of vehicle 196 Tonne (approx)

MRWA own increase to axle loads

205 Tonne = 251kN Per Axle
245 Tonne = 300kN Per Axle

16.2.6 1989 MRWA Bridge Design Manual Road Train

- Type of Code – Limit state
- Live Load – 4 or 6 x 16.5t Tandem Axles (as below)
- Design Lane Width – 3.0m
- Ultimate Limit State Factor – 2.0
- Location – One vehicle per bridge applied anywhere on the structure without concurrent loading
- Lane Reduction Factors – N/A
- Dynamic Load Allowance – As per T44 of 1992 Austroads Bridge Design Code



4 x 16.5t TANDEM AXLES

16.2.7 1992 Austroads Bridge Design Code

- Type of Code – Limit state

W7 Wheel Load

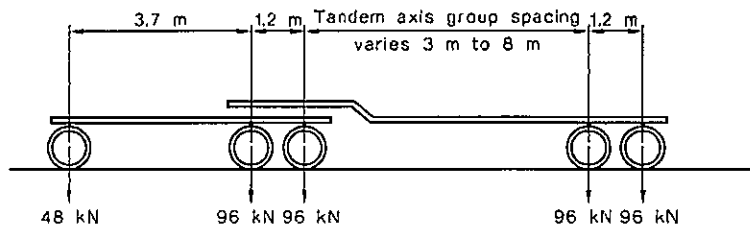
- Live Load - 70kN over a contact area of 500mm x 200mm
- Design Lane Width – N/A
- Ultimate Limit State Factor – 2.0
- Location – Anywhere on the bridge to produce the maximum local effect for the structural element under consideration for which the critical load is a single wheel load
- Lane Reduction Factors – N/A
- Dynamic Load Allowance – DLA = 0.25 as minimum

T44 Truck Load and L44 Lane Load

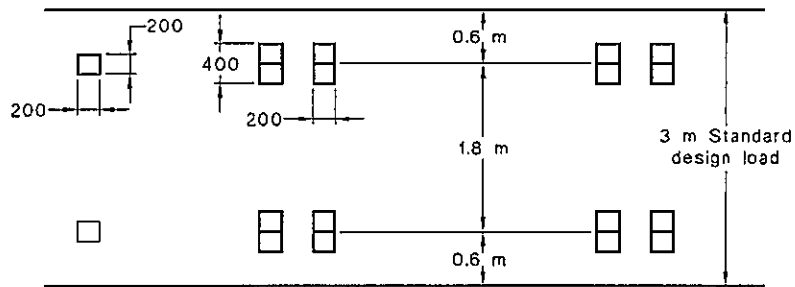
- Live Load - T44 truck or lane loading (as below)
- Design Lane Width – 3.0m
- Ultimate Limit State Factor – 2.0
- Location – One truck load or lane load per design lane applied anywhere on the structure. The lane loading shall be continuous or discontinuous.
- Lane Reduction Factors –

1 lane	1.0
2 lanes	0.9
3 lanes	0.8
4 lanes	0.7
5 lanes	0.6
≥6 lanes	0.55

- Dynamic Load Allowance (as below)

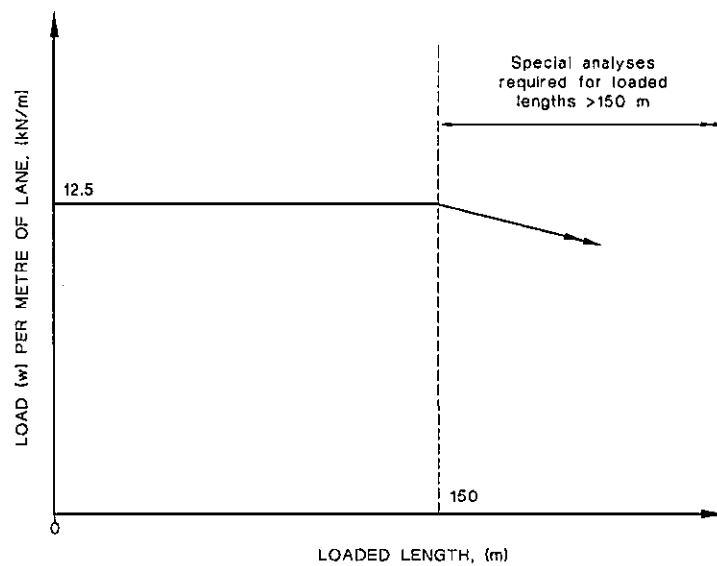


ELEVATION VIEW



PLAN VIEW

T44 TRUCK LOAD

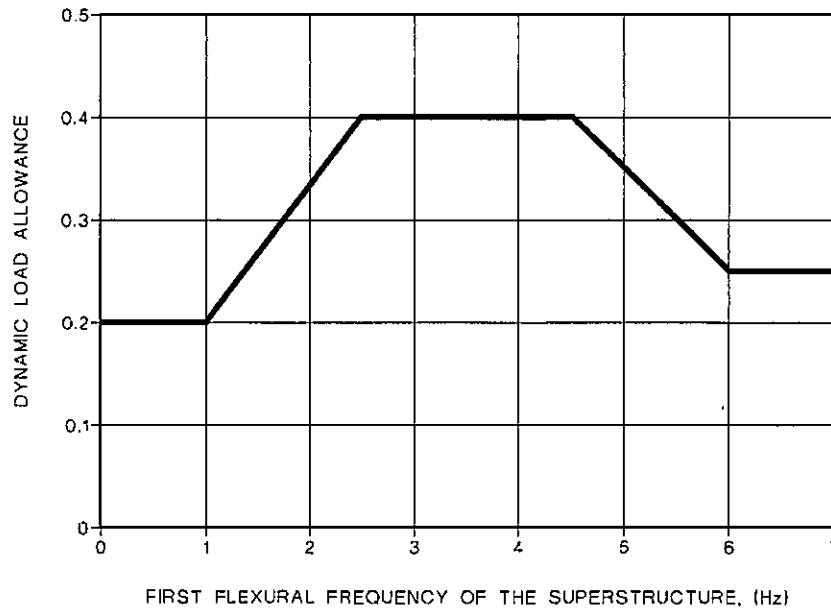


NOTES

1. L44 Lane loading shall consist of a uniformly distributed load as shown above together with a concentrated load of 150kN
2. For continuous spans the lane loading shall be continuous or discontinuous as may be necessary to produce maximum effects, and an additional concentrated load shall be placed in one other span in such a position as to produce maximum negative moment.
3. The L44 lane load does not apply to spans less than 10m.

L44 LANE LOAD

(Uniformly distributed part only)



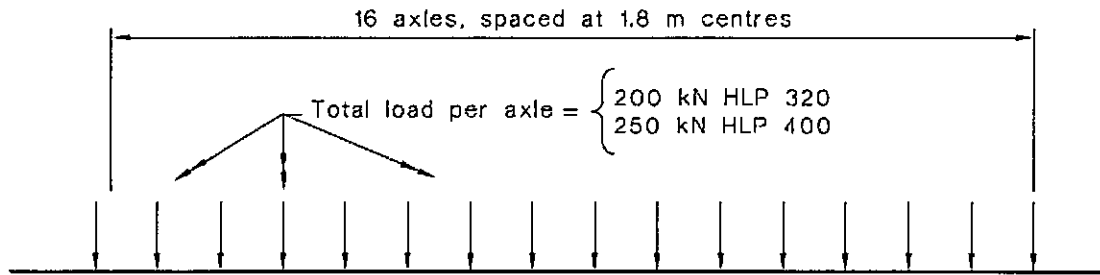
NOTE: A range of first flexural frequencies from 0.9 to 1.1 times the calculated superstructure frequency should be considered. The dynamic load allowance adopted should be the maximum value obtained from Figure A4 for this frequency range.

DYNAMIC LOAD ALLOWANCE FOR T44 TRUCK AND L44 LANE LOADS (ONE LANE LOADED)

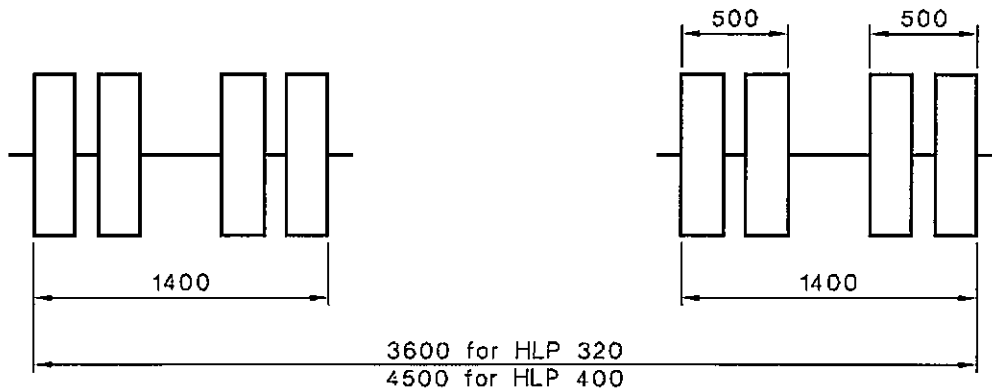
Note: DLA to be taken as full at ground line, reducing linearly to zero at depth 2m. For buried structures this is 0.4 reducing to 0.1.

HLP320 and HLP400 Platform Loads

- Live Load – HLP320 or HLP 400 platform loading (as below)
- Design Lane Width – N/A
- Ultimate Limit State Factor – 1.5
- Location – One platform per bridge along the centreline ± 1 m of the bridge without concurrent loading (undivided) or along the centreline ± 1 m of the carriageway in the travel direction with 50% T44 truck loading or L44 lane loading on the other carriageway.
- Lane Reduction Factors – N/A
- Dynamic Load Allowance - DLA = 0.1



ELEVATION VIEW



END VIEW OF AN HLP AXLE

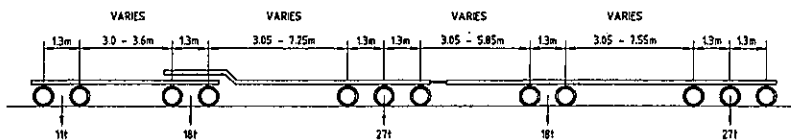
FOR HLP LOADS LATERAL SPACING OF DUAL WHEELS ALONG AN AXLE

Note: For continuous bridges the loading may be separated into two groups with a central gap of between 6 m and 15 m, the gap being chosen to give the most adverse effect.

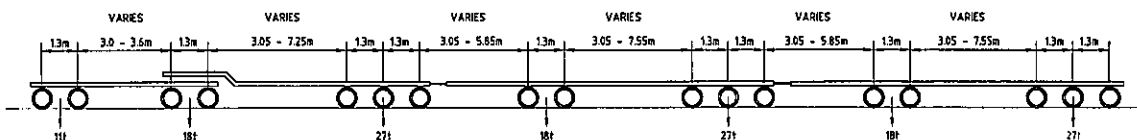
16.2.8 1998 MRWA Bridge Branch Design Information Manual Standard Road Trains

- Type of Code – Limit state
- Live Loads – 101t Double Bottom Road Train and 146t Triple Bottom Road Train (as below)
- Design Lane Width – 3.0m
- Ultimate Limit State Factor – 2.0
- Location – As per T44 of 1992 Austroads Bridge Design Code
- Lane Reduction Factors – As per T44 of 1992 Austroads Bridge Design Code
- Dynamic Load Allowance – As per T44 of 1992 Austroads Bridge Design Code

DOUBLE BOTTOMED DESIGN VEHICLE
(G.C.M = 101 tonnes)

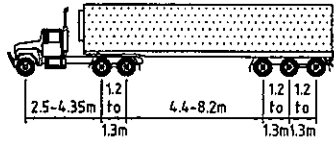


TRIPLE BOTTOMED DESIGN VEHICLE
(G.C.M = 146 tonnes)



16.2.9 1999 MRWA NRTC Vehicles

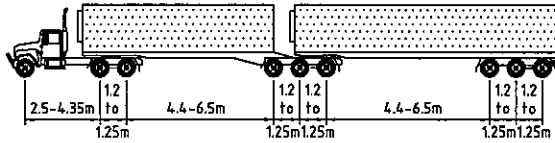
- Type of Code – Limit state
- Live Loads – Semi Trailer, Tri-Tri B-Double, Double Bottom Road Train and Triple Bottom Road Train at road friendly suspension weights (as below)
- Design Lane Width – 3.0m
- Ultimate Limit State Factor – 2.0
- Location – As per T44 of 1992 Austroads Bridge Design Code
- Lane Reduction Factors – As per T44 of 1992 Austroads Bridge Design Code
- Dynamic Load Allowance – As per T44 of 1992 Austroads Bridge Design Code



6.0T	17.0T	22.5T
+0.5T	+0.5T	+0.5T
+0.13T	+0.35T	+0.46T
<u>6.63T</u>	<u>17.85T</u>	<u>23.46T</u>

MASS LIMITS
EXTRA LOAD ALLOWANCE
2% TOLERANCE
DESIGN LOAD (UNFACTORED FOR LIMIT STATES)

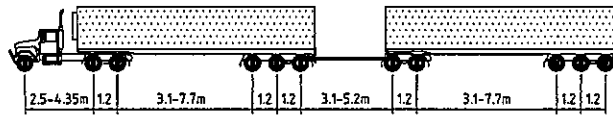
SEMI - TRAILER
GROSS COMBINED MASS 45.5T



6.0T	17.0T	22.5T	22.5T
+0.5T	+0.5T	+0.5T	+0.5T
+0.13T	+0.35T	+0.46T	+0.46T
<u>6.63T</u>	<u>17.85T</u>	<u>23.46T</u>	<u>23.46T</u>

MASS LIMITS
EXTRA LOAD ALLOWANCE
2% TOLERANCE
DESIGN LOAD (UNFACTORED FOR LIMIT STATES)

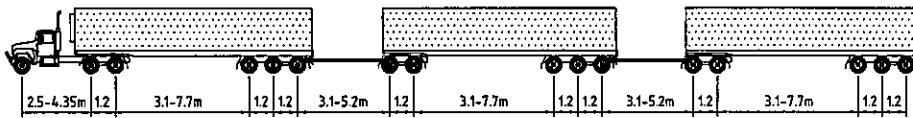
TRI - TRI, B - DOUBLE
GROSS COMBINED MASS 68T



6.0T	17.0T	22.5T	17.0T	22.5T
+0.5T	+0.5T	+0.5T	+0.5T	+0.5T
+0.13T	+0.35T	+0.46T	+0.35T	+0.46T
<u>6.63T</u>	<u>17.85T</u>	<u>23.46T</u>	<u>17.85T</u>	<u>23.46T</u>

MASS LIMITS
EXTRA LOAD ALLOWANCE
2% TOLERANCE
DESIGN LOAD (UNFACTORED FOR LIMIT STATES)

DOUBLE BOTTOM ROAD TRAIN
GROSS COMBINED MASS 85T



6.0T	17.0T	22.5T	17.0T	22.5T	17.0T	22.5T
+0.5T	+0.5T	+0.5T	+0.5T	+0.5T	+0.5T	+0.5T
+0.13T	+0.35T	+0.46T	+0.35T	+0.46T	+0.35T	+0.46T
<u>6.63T</u>	<u>17.85T</u>	<u>23.46T</u>	<u>17.85T</u>	<u>23.46T</u>	<u>17.85T</u>	<u>23.46T</u>

MASS LIMITS
EXTRA LOAD ALLOWANCE
2% TOLERANCE
DESIGN LOAD (UNFACTORED FOR LIMIT STATES)

TRIPLE BOTTOM ROAD TRAIN
GROSS COMBINED MASS 124.5T

16.2.10 1999 MRWA Interim Bridge Design Loads

- Type of Code – Limit state

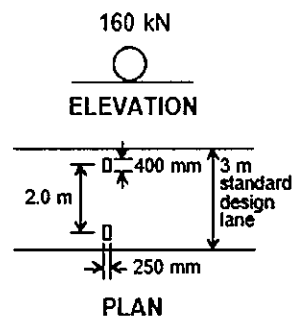
Wheel Load

- Live Load – W80 as per AS5100.2 Clause 7.2.2
- Design Lane Width – N/A
- Ultimate Limit State Factor – As per AS5100.2 Clause 7.10
- Location – As per AS5100.2 Clause 7.2.2
- Lane Reduction Factors – N/A
- Dynamic Load Allowance - DLA = 30%

Note: DLA to be taken as full at ground line, reducing linearly to zero at depth 2m. For buried structures this is full at ground line reducing to 0.1.

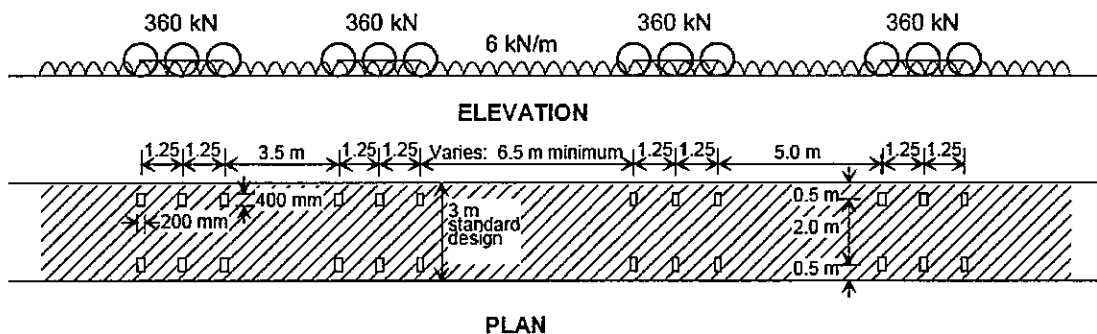
Axle Load

- Live Load – A160 axle load (as below)
- Design Lane Width – 3.0m
- Number of design lanes, $n = \text{width between barriers} / 3.1$
- Ultimate Limit State Factor – As per AS5100.2 Clause 7.10
- Location – One axle load per design lane (as below) anywhere on the structure
- Lane Reduction Factors – As per AS5100 Clause 7.6
- Dynamic Load Allowance - DLA = 30% (note: AS5100-2004 & 2017 are 40%)
Note: DLA to be taken as full at ground line, reducing linearly to zero at depth 2m. For buried structures this is full at ground line reducing to 0.1.



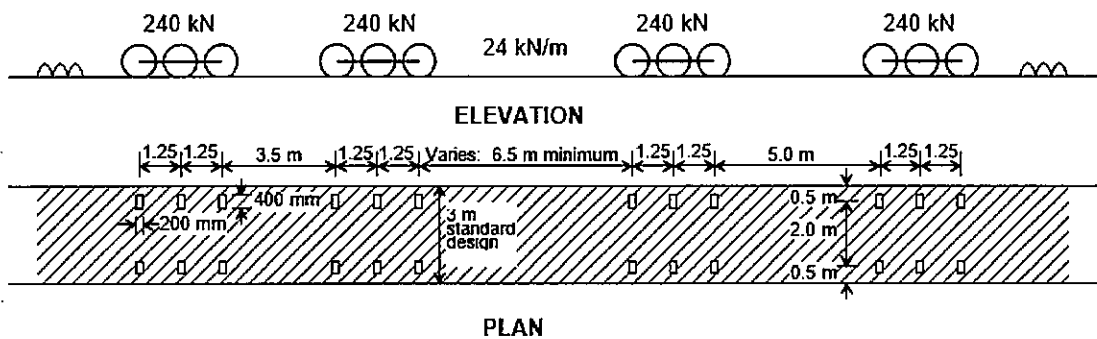
Moving Traffic Load

- Live Load – M1600 moving traffic load (as below. Note this is different to AS5100)
- Design Lane Width – 3.0m
- Number of design lanes, $n = \text{width between barriers} / 3.1$
- Ultimate Limit State Factor – AS5100.2 Clause 7.10
- Location – As per AS5100.2 Clause 7.2.4
- Lane Reduction Factors – As per AS5100.2 Clause 7.6
- Dynamic Load Allowance – As per T44 of 1992 Austroads Bridge Design Code
Note: DLA to be taken as full at ground line, reducing linearly to zero at depth 2m. For buried structures this is full at ground line reducing to 0.1.



Stationary Traffic Load

- Live Load – S1600 stationary traffic load (as below. Note this is different to AS5100)
- Design Lane Width – 3.0m
- Ultimate Limit State Factor – As per AS5100.2 Clause 7.10
- Location – As per AS5100.2 Clause 7.2.5
- Lane Reduction Factors – As per AS5100.2 Clause 7.6
- Dynamic Load Allowance – DLA = 0%



16.2.11 2004 Australia Standard Bridge Design AS5100

- Type of Code – Limit state
- W80, A160, M1600, S1600, HLP320 and HLP400 as per AS5100.2 2017

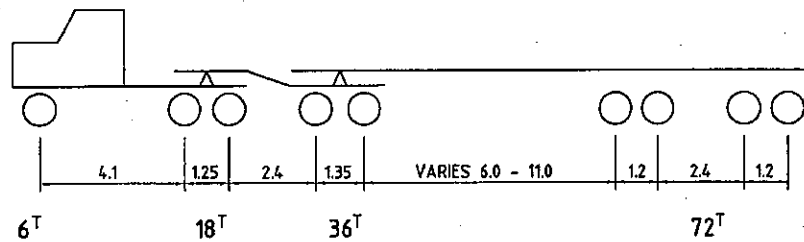
16.3 HISTORICAL LOAD RATING VEHICLES

16.3.1 1993 MRWA Bridge Branch Design Information Manual

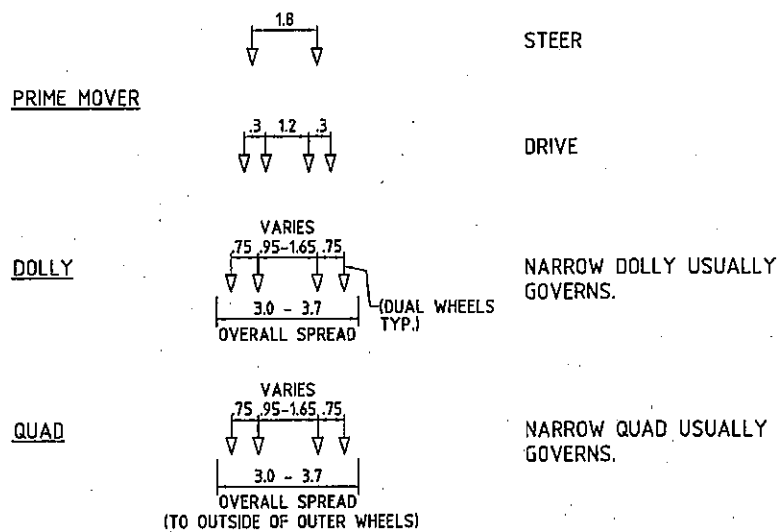
- Type of Code – Limit state
- Live Loads – Rating Vehicles 1-4 (as below)
- Design Lane Width – N/A
- Ultimate Limit State Factor – 1.5
- Location – One vehicle for single carriageway bridges $\pm 1\text{m}$ of the bridge centreline without concurrent loading
 One Vehicle 1-2 for dual carriageway bridges $\pm 1\text{m}$ of the carriageway centreline with 50% T44/L44 on the other carriageway
 One Vehicle 3-4 for dual carriageway bridges $\pm 1\text{m}$ of the carriageway centreline without concurrent loading
- Lane Reduction Factors – N/A
- Dynamic Load Allowance – DLA = 10%

VEHICLE 1

PRIME MOVER + DOLLY + QUAD = 132 TONNES ALL-UP.

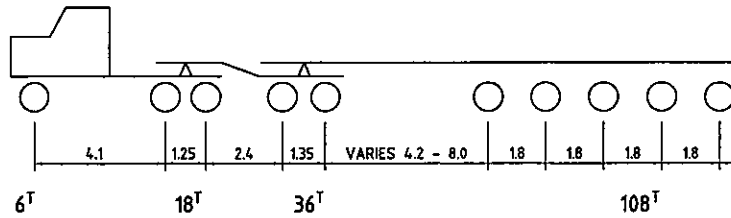


TRANSVERSELY

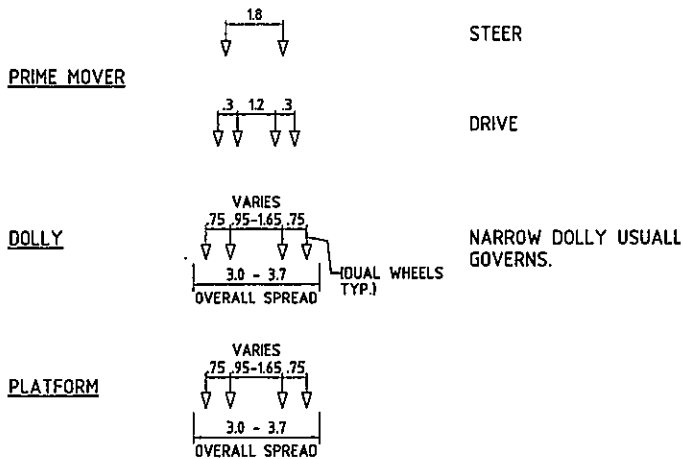


VEHICLE 2

PRIME MOVER + DOLLY + 6 LINE PLATFORM = 168 TONNES ALL-UP.

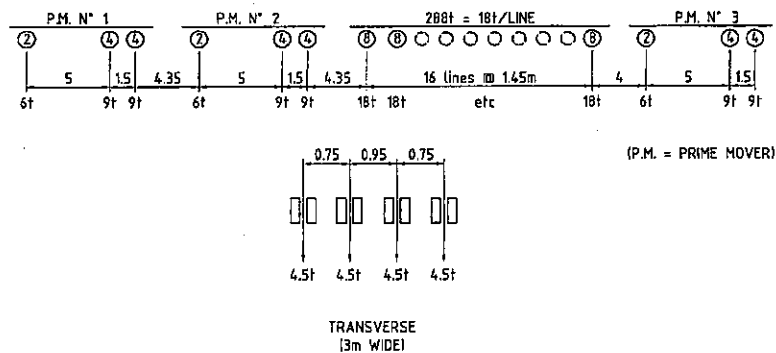


TRANSVERSELY



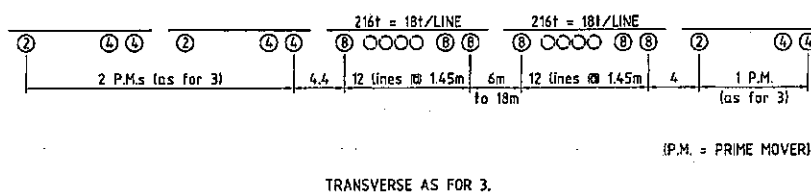
VEHICLE 3

16 LINE 3m WIDE PLATFORM WITH LINE SPACING AT 1.45m. (288 TONNES GROSS) PLUS 3 PRIME MOVERS. (2 AT FRONT AND 1 AT REAR)



VEHICLE 4

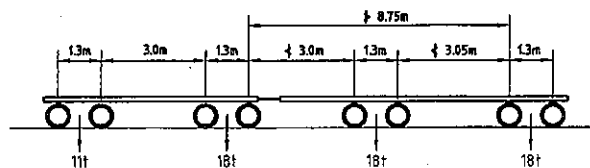
2/12 LINE PLATFORMS AT 1.45m. (192 WHEELS)
PLUS 3 PRIME MOVERS



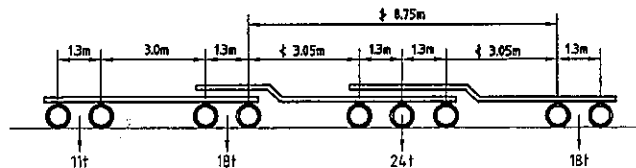
16.3.2 1993 MRWA Load Rating Vehicles

- Type of Code – Limit state
- Live Loads – Vehicles 1-8 representing various semi trailers, B-doubles and road trains (as below)
- Design Lane Width – 3.0m
- Ultimate Limit State Factor – 2.0
- Location – As per T44 of 1992 Austroads Bridge Design Code
- Lane Reduction Factors – As per T44 of 1992 Austroads Bridge Design Code
- Dynamic Load Allowance – As per T44 of 1992 Austroads Bridge Design Code

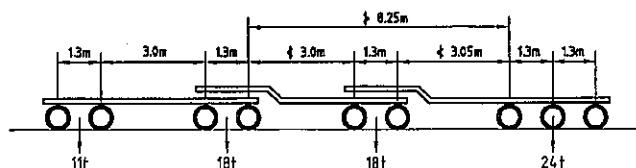
VEHICLE 1: TRUCK PLUS 4 AXLE DOG TRAILER
(G.C.M = 65 tonnes)



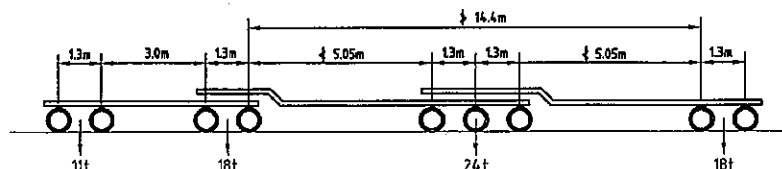
VEHICLE 2: SHORT "B" DOUBLE TRI-TANDEM
(G.C.M = 71 tonnes)



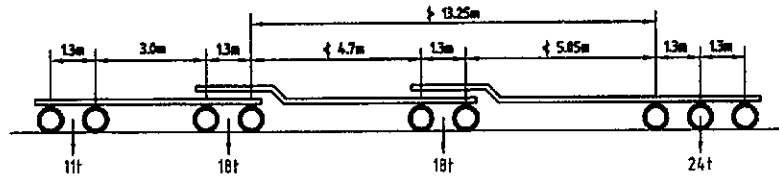
VEHICLE 3: SHORT "B" DOUBLE TANDEM-TRI
(G.C.M = 71 tonnes)



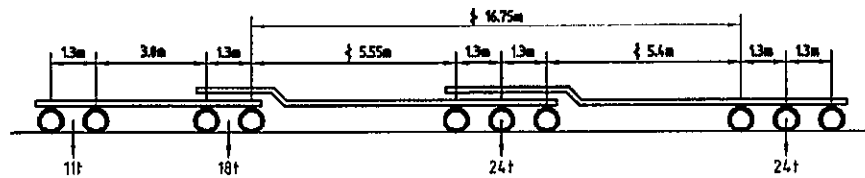
VEHICLE 4: LONG "B" DOUBLE TRI-TANDEM
(G.C.M = 71 tonnes)



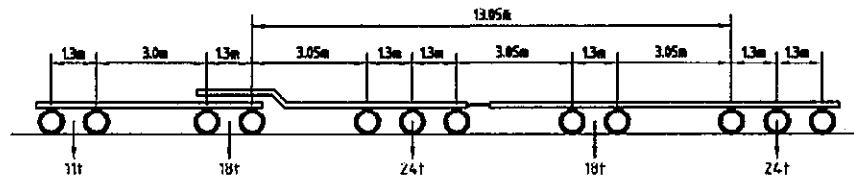
VEHICLE 5: LONG "B" DOUBLE TANDEM-TRI
(G.C.M = 71 tonnes)



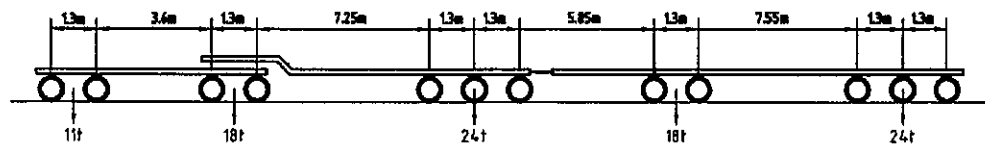
VEHICLE 6: TRI-TRI "B" DOUBLE
(G.C.M = 77 tonnes)



VEHICLE 7: SHORT DOUBLE BOTTOM ROAD TRAIN
(G.C.M = 95 tonnes)



VEHICLE 8: LONG DOUBLE BOTTOM ROAD TRAIN
(G.C.M = 95 tonnes)



16.3.3 1995 MRWA Bridge Branch Design Information Manual

- Type of Code –Limit state

Group 1 Vehicles

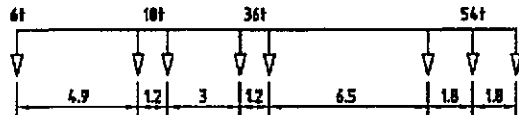
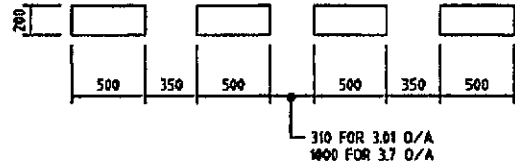
- Live Load – Group 1 Vehicles 1-3 as per the same vehicles in Section 4 of this Manual
- Design Lane Width – 3.0m
- Ultimate Limit State Factor – 2.0
- Location – As per T44 of 1992 Austroads Bridge Design Code , but only one rating vehicle to be on the bridge with T44/L44 in the other lane(s) positioned to give the worst effects
- Lane Reduction Factors – As per T44 of 1992 Austroads Bridge Design Code
- Dynamic Load Allowance – As per T44 of 1992 Austroads Bridge Design Code , refer AS5100.7 Clause A2.2.10

Group 2 Vehicles

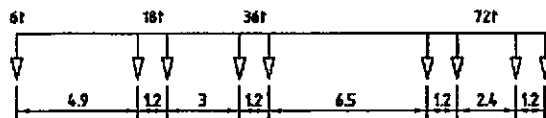
- Live Loads – Group 2 Vehicles 1-6 (as below)
Note: Group 2 Vehicles 1-2 and 5 are identical to the same vehicles in Section 4 of this Manual and Group 2 Vehicle 4 is identical in configuration to the same vehicle in Section 4 of this Manual but was considered at both vehicle platform spreads
- Design Lane Width – N/A
- Ultimate Limit State Factor – 1.5
- Location – One vehicle for single carriageway bridges ± 1 m of the bridge centreline without concurrent loading
One vehicle for dual carriageway bridges ± 1 m of the carriageway centreline with T44/L44 on the other carriageway
- Lane Reduction Factors – N/A
- Dynamic Load Allowance – DLA = 10%

NOTE

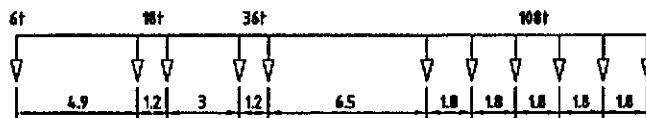
VEHICLES 1-4 CAN HAVE
AN O/A WIDTH OF EITHER
3.01m OR 3.7m.
VEHICLE 5 IS 3.01m O/A
VEHICLE 6 IS 3.7m O/A



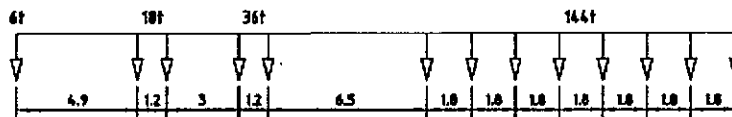
1. PRIME MOVER + 36 TONNE DOLLY + 54 TONNE TRIAXLE
(G.C.M. = 114 TONNES)



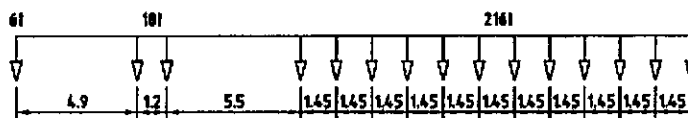
2. PRIME MOVER + 36 TONNE DOLLY + 72 TONNE SPREAD QUAD
(G.C.M. = 132 TONNES)



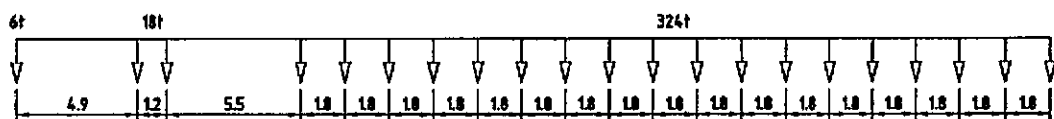
3. PRIME MOVER + 36 TONNE DOLLY + 108 TONNE 6-LINE PLATFORM
(G.C.M. = 168 TONNES)



4. PRIME MOVER + 36 TONNE DOLLY + 144 TONNE 8-LINE PLATFORM
(G.C.M. = 204 TONNES)



5. PRIME MOVER + 216 TONNE 12-LINE PLATFORM
(G.C.M. = 240 TONNES)



6. PRIME MOVER + 324 TONNE 18-LINE PLATFORM
(G.C.M. = 348 TONNES)

GROUP 2 RATING VEHICLES

SECTION 17 – EXTERNAL AUTHORITIES

This information is Part 17 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

The Structures Design & Standards Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia, I authorise this issue and the use of this Information.

A LIM
SENIOR ENGINEER STRUCTURES

Date: 16/04/18

Document No: 3912/02-17

SECTION 17

CONTENTS

17	LIST OF EXTERNAL AUTHORITIES	3
----	------------------------------------	---

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description
All	1	15/12/05	Complete review
All	2	13/04/18	Complete review

Custodian Endorsement

M RAJAKARUNA
Structures Design & Standards Engineer
Date: 13/04/18

17 LIST OF EXTERNAL AUTHORITIES

Before the commencement of a design project it is necessary to contact ALL known appropriate external authorities that may be affected. This applies mostly to proposed works but is nevertheless appropriate to maintenance works, particularly where pile driving or temporary works are likely to cause disruption to the immediate environment, community or traffic.

This list records various known authorities with comments on area of authority, responsibility or interest. It should be noted that this list does not include Main Roads Regions, Mining Companies, Landowners, etc.

Different authorities will need to be contacted for different jobs. It is the responsibility of the Designer to check that all authorities likely to be affected by a project are contacted.

It should not be assumed that this list is comprehensive or final.

AUTHORITIES	AREA OF RESPONSIBILITY OR INTEREST
Department of Agriculture and Water Resources	Matters likely to impact land in an agricultural sense, e.g. backwater, salinity, waterway diversion or realignment.
Department of Primary Industries and Regional Development	Initial contact via Main Roads.
Department of Planning, Lands and Heritage	<p>Manages the location of Aboriginal sites of significance and matters concerning social and economic equity for Indigenous people, respect for the land or unique heritage and culture. See also Local Aboriginal Groups.</p> <p>Includes listed structures of historical significance. See also Australian Heritage Council.</p>
Australian Heritage Council	Matters concerning significant historical sites where Federal funding is involved.
Local Aboriginal Groups	Matters concerning social and economic equity for Indigenous people, respect for the land or unique heritage and culture.
<p>Independent Regional Development, eg:</p> <ul style="list-style-type: none"> • Regional Development Council • Western Australian Regional Development Trust • Gascoyne Development Commission (DC) • Goldfields DC • Great Southern DC • Kimberley DC • Mid West DC • Peel DC • Pilbara DC • South West DC • Wheatbelt DC 	Independent Partners to the Department of Primary Industries and Regional Development.
Department of Transport – Cycling	Cycle path requirements.
WestCycle	Peak cycling body for WA
Department of the Environment and Energy	Designs and implements Australian Government policy and programs to protect and conserve the environment, water and heritage, promote climate action, and provide adequate, reliable and affordable energy.
Conservation Council of WA	Matters relating to environmentally sensitive areas. Matters relating to Wetlands Conservation Society will be identified by Conservation Council.

Department of Biodiversity, Conservation and Attractions	Matters relating to works likely to have an environmental impact re-National Parks, State Forests, Marine Parks, Conservation Parks, dieback control, flora and fauna etc, the Swan and Canning Rivers / tributaries and adjoining land.
Department of Fire & Emergency Services <ul style="list-style-type: none"> • Fire and Rescue Service • St. John Ambulance • Police Service WA 	All emergency services to be advised of intent to close bridge/road. To be done at design stage in case of access or staging problems.
Department of Water and Environmental Regulation	The DWER conducts environmental impact assessments and develops policies to protect the environment. The DWER also monitors compliance with the conditions of Ministerial Statements. Responsible for the waters and associated land within declared management areas. Must approve any alteration to the bed or banks of waterways within declared management areas of the State.
Landgate	Responsible for land tenure throughout WA. For mining tenements see Department of Industry, Innovation and Science.
Local Government Authority	Road or bridge closures, scheme approval, drainage methods, footpath requirements, services etc.
Department of Transport	Preparation of land use strategies and development. Responsible to ensure planned development is in accordance with sound planning principles. Initial contact via Main Roads.
Department of Transport (Marine)	Responsible to ensure that any navigable body of water is not modified in any way likely to create a navigation hazard. Jurisdiction includes recreational waters set aside for water skiing, sailing etc.
Department of Mines, Industry Regulation and Safety	Geological and hydrological advice such as site investigation, water bores, quarries, road cuttings etc.
National Trust (WA)	Details of National Estates. Copy of National Estates Register held in Main Roads Library. No statutory requirement for contact, however where historical sites are involved, contact is advised as a courtesy.

<p>Service providers, eg:</p> <ul style="list-style-type: none"> • Alinta Energy • Atco Gas • BP (Oil pipeline) • Natural Gas Pipelines • Telecommunication Groups (Telstra, Optus, etc) • Water (Water Corporation of WA, Harvey Water, Aqwest (Bunbury), Busselton Water Board) • Western Power/Horizon Power 	<p>Mandatory contact required for possible relocation of existing service or requirement for new service.</p>
<p>Public Transport Authority (PTA) [bus; passenger rail]</p>	<p>Bus servicing considerations for engineering design, scheduling and/or disruptions to services. Mandatory contact for all passenger rail impacts and interfaces.</p>
<p>Arc Infrastructure/Aurizon [freight rail]</p>	<p>Mandatory contact for all freight rail impacts and interfaces.</p>
<p>Private Rail Operators, eg:</p> <ul style="list-style-type: none"> • Rio Tinto • BHP 	<p>Mandatory contact for all private rail impacts and interfaces.</p>
<p>WA Farmers Federation</p>	<p>Mandatory contact required for all proposed new bridge construction in the rural areas of the State.</p>
<p>Other Environmental and Resource Groups, eg:</p> <ul style="list-style-type: none"> • Landcare District Committees • Pastoralists and Graziers Association • Environs Kimberley • North Metro Conservation Group • Northern Agricultural Catchment Council • Perth Region NRM • Rangelands Natural Resource Management WA • South Coast National Resource Management Inc. • South West Catchment Council • Urban Bushland Council 	<p>Various non-government groups.</p> <p>Landcare District Committees - found throughout the State, refer Department of Agriculture and Water Resources.</p> <p>Pastoralists & Graziers Association - mostly Northern Areas of the State.</p>

SECTION 18 – PREPARATION OF DESIGN REPORT (OCCUPATIONAL SAFETY AND HEALTH)

This information is Part 18 of the Bridge Branch Design Information Manual and is owned and controlled by the Senior Engineer Structures.

Senior Design Engineer is the delegated custodian. All comments and requests for changes should be submitted to the delegated custodian.

Authorisation

As head of Structures Engineering of Main Roads Western Australia,
I authorise this issue and the use of this Information.



R SCANLON
SENIOR ENGINEER STRUCTURES

Date: 16 June 2009

Document No.: 3912/02-18

Controlled Copies shall be marked accordingly

TABLE OF CONTENTS

18	PREPARATION OF DESIGN REPORT (OS&H).....	3
18.1	INTRODUCTION.....	3
18.2	BACKGROUND	3
18.3	DESIGNER'S REQUIREMENTS.....	3
18.4	DESIGN REPORT.....	3
Appendix A	Procedure for Development of the Report.....	5
Appendix B	Examples of Design Risks.....	6
Appendix C	Design Report Pro-forma.....	7
Appendix D	Main Roads Risk Reference Tables	8

REVISION STATUS

Page No.	Rev. No.	Rev. Date	Revision Description

Revision Authorisation

R SCANLON
 Senior Engineer Structures
 Date:

18 PREPARATION OF DESIGN REPORT (OCCUPATIONAL SAFETY AND HEALTH)

18.1 Introduction

This Section of the Manual describes the mandatory requirements for Designers to provide clients with a written report on the occupational safety and health (OSH) aspects of their designs. In addition it provides guidance to Designers on a basis for identifying the types and extent of hazards and risks to be addressed.

18.2 Background

Regulations relating to the National Standard for Construction Work came into operation for the civil/commercial construction sector on 3rd January 2008.

These regulations introduce requirements relating to the provision of information, consultation, planning, documentation and other measures to ensure occupational safety and health in the building and construction industry.

These regulations are contained in Division 12 of Part 3 of the Occupational Safety and Health Regulations 1996.

The regulations apply to main contractors and people with control of construction work, clients commissioning design and construction work and designers doing design work for construction projects. This manual covers design requirements only.

18.3 Designer's Requirements

Designers must provide their clients with a written report on the occupational safety and health aspects of their designs. The client must ensure that this information is passed on to the main contractor and to anyone who obtains the end product of the construction work from the client.

18.4 Design Report

18.4.1 Requirements under the Regulations

In accordance with Regulation 3.140 of Division 12 of Part 3 of the Occupational Safety and Health Regulations 1996, the Designer's OSH report must identify the following aspects of the design for the constructor to consider:

- The hazards associated with the construction work required to build the design, (for example, hazardous structural features, hazardous construction materials or hazardous procedures or practices);
- The designer's assessment of the risk of injury or harm resulting from those hazards;
- The action the designer has taken to reduce those risks, (for example, changes to the design or changes to construction methods or construction materials); and
- Any parts of the design where the hazards have been identified but not resolved.

18.4.2 Preparation of the Report

The extent and type of hazards are only broadly defined within the Regulations. Given that a construction site is potentially a hazardous environment due to the nature of the work, the Designers might elect to include all hazards associated with the work site and prepare mitigation actions accordingly.

Structures Engineering considers that in most cases this would result in a report that had a level of detail that would be a duplication of other processes whilst not adding value in achieving the objectives of the regulations. One reason for this is that MRWA has a pre-qualification system for contractors that ensures the constructor is qualified and experienced to undertake the construction works. In addition, the contractor is required within the contract to prepare a range of management plans that include for site safety.

Therefore in preparing the Report the Designer may assume that the constructor is an experienced builder, unless it is known to the contrary, and identify only those hazards that may be of a non-standard nature, unusual, specific to the design or otherwise noteworthy. Some examples are given in Appendix B to illustrate the types of design specific hazards that should be included in the Report. Other hazards that are typically found on construction sites such as traffic, working at heights or with machinery and tools may be considered to be of a standard nature, familiar to the Contractor and within its responsibility.

APPENDIX A - PROCEDURE FOR DEVELOPMENT OF THE REPORT

1. The Designer during the design stage must assess the following:
 - Is the design complex with potential hazards associated with the complexity of the design impacting on the level of construction hazard?
 - Are there any designer identified construction hazards associated with the site conditions, features, topography, site constraints etc.?
 - Is the design innovative or unusual, requiring construction methodology, techniques and equipment which may not be familiar to an appropriately pre-qualified constructor?
 - Is the design straightforward, but with certain hazards associated with the construction?
 - Are there any specific or unusual interfaces with other agencies that might constitute an unusual hazard during construction?
2. Based on the above assessments, the Designer must identify and document construction activities and materials that are potentially hazardous. It is considered that designs of standard type structures which are regularly constructed would require minimum input into a Report prepared by the Designer, compared to more complex or innovative designs.
3. The next step is to assess and rate the risk associated with the identified potential hazard. Refer to the 'Corporate Risk Management Policy and Procedure'. A suitable pro-forma for recording the identified hazard and assessment is shown in Appendix C.
4. It is the preferred approach that the Designer develops strategies to mitigate those activities with high risk and include them in the Report. The residual risk must then be rated in accordance with MRWA Risk-Web matrix in the 'Corporate Risk Management Policy and Procedure'. Refer to the extract in Appendix D.
5. The residual risk must then be compared to what is considered acceptable by MRWA that is, Low or Medium.
6. The Designer must then document the risk in the Report. The Design Report must be signed by the Designer and endorsed by a Senior Designer before issue.

APPENDIX B – EXAMPLES OF DESIGN RISKS

(Note that these are illustrative examples only and in every instance the hazard, likelihood and consequence must be assessed on its merits). Assessment of risk rating before and after Design may vary depending on specific site circumstances.

Construction Activity	Designer Identified Hazard	Likelihood Level	Consequence Level	Risk Rating	Action Designer has taken to Reduce Risk	Residual Risk Rating	Residual Risk Acceptable?
Bridge Launching	<ul style="list-style-type: none"> Uncontrolled movement of bridge during launching Locations of high load and stress 	1	4	Medium	Designer ensures details of all design assumptions are included on the Drawings and Specification.	Low	Yes
Working over or near a Railway	Conflict between site staff/plant with <ul style="list-style-type: none"> trains and overhead electrified cables 	1	4	Medium	Designer liaises with the Rail Authority at the design stage and identifies a process enabling the successful completion of works. Specifications require Rail Authority personnel to be present on site during critical stages of construction.	Low	Yes
Structural Alterations requiring Temporary Supports	Instability and possible collapse	2	4	High	Designer to provide the loads required for propping/temporary works	Medium	Yes
Lifting of large precast concrete members	<ul style="list-style-type: none"> Instability during lifting Inadequate capacity in lifting points Access for cranes, capacity for lift Safe landing and location and fixing of precast member 	2	4	High	Designer to provide lifting loads, position of lifting points, anchorage requirements for lifters. Also, seek advice from specialists if necessary.	Medium	Yes

APPENDIX C - DESIGN REPORT PRO-FORMA

Construction Activity	Designer Identified Hazard	Likelihood Level	Consequence Level	Assessment of Risk	Action Designer has taken to Reduce Risk	Residual Risk Rating	Residual Risk Acceptable? <i>Sign off</i>

APPENDIX D - MAIN ROADS RISK REFERENCE TABLES

QUALITATIVE MEASURES OF LIKELIHOOD

LEVEL	DESCRIPTOR	FREQUENCY
1	Rare	Less than once in 10 years
2	Unlikely	At least once in 10 years
3	Moderate	At least once in 3 years
4	Likely	At least once per 1 year
5	Almost certain	More than once per year

QUALITATIVE MEASURES OF CONSEQUENCE

LEVEL	RANK	INJURIES	FINANCIAL LOSS	INTERRUPTION TO SERVICES	REPUTATION & IMAGE	PERFORMANCE	ENVIRONMENTAL
1	Insignificant	No injuries.	Less than \$25,000	Less than 1 hour	Unsubstantiated, low impact, low profile or no news item.	Up to 5% Variation in KPI or objective.	No lasting effect of significance. Very short term impact (< 6 months).
2	Minor	First aid treatment.	\$25,000 to \$100,000	1 hour to 4 hours	Substantiated, low impact, low news profile.	5% to 10% Variation in KPI or objective.	Minor localised impacts. Short term impact (6 months - 2 years).
3	Moderate	Medical treatment required.	\$100,000 to \$500,000	4 hours to 24 hours	Substantiated, public embarrassment, moderate impact, moderate news profile.	10% to 25% Variation in KPI or objective.	Localised - local significance. Medium term impact (2 - 5 years).
4	Major	Death or extensive injuries.	\$500,000 to \$ 5 million	24 hours to 1 week	Substantiated, public embarrassment, high impact, high news profile, Third Party actions.	25% to 50% Variation in KPI or objective.	Severe and of moderate size. Long term impact (5 - 20 years).
5	Catastrophic	Multiple deaths or severe permanent disablements.	More than \$5 million	More than 1 week	Substantiated, public embarrassment, very high multiple impacts, high widespread multiple news profile, Third Party actions.	More than 50% Variation in KPI or objective.	Severe and extensive. Permanent or very long term (> 20 years). * Evaluate in terms of the scale and/or degree of impact.

RISK-WEB RISK RATING CHART

